January 4, 2023

Revised:

February 28, 2023 May 26, 2023 June 29, 2023 **September 13, 2023**

222 Church Road

Cheltenham Township, Montgomery Co., PA

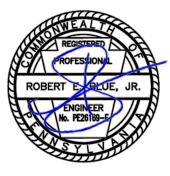
POST CONSTRUCTION STORMWATER MANAGEMENT REPORT

REB No.: 2154-10

Prepared for:

222 Church Road, LLC

509 Cedarhill Road Far Rockaway, NY 11691





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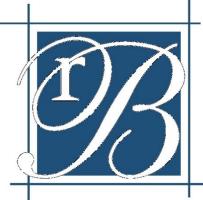


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1.0 INTRODUCTION

This report has been prepared for the 222 Church Road project, a residential subdivision development located in Cheltenham Township, Montgomery County, PA. This report summarizes the stormwater management design and calculations for the approval of the municipal land development application and procurement of the Pennsylvania Department of Environmental Protection's (PADEP) National Pollutant Discharge Elimination System (NPDES) Permit. This report shall accompany the PCSM Plans (Plans) for the project ("PCSM Plan" sheets contained within the "Final Subdivision & Land Development Plan for 222 Church Road". The plans and this report shall be considered the overall stormwater management plan for the project.

The plans and report were prepared by the staff of Robert E. Blue Consulting Engineers, P.C. under the direction of Robert E. Blue Jr., P.E. The measures shown have been designed in accordance with the guidelines of PADEP, the County Conservation District, and municipal regulations.

Formal Education

Associates Degree in Architectural Design from Temple University, 1970

Bachelors of Science: Civil Engineering from Temple University, 1972

Pennsylvania Licensed Professional Engineer since 1977 Lic.No.: PE26169-E

Pennsylvania Licensed Land Surveyor since 1982 Lic.No.: SU1323A

Most recently approved plans include:

- The Shoppes at South Abington (South Abington Township, Lackawanna County, PA 2020)
- 1950 Skippack Pike Blue Bell Storage (Whitpain Township, Montgomery County, PA 2020)
- Royal Farms #195 (Marple Township, Delaware County, PA 2019)
- Royal Farms #234 (Collegeville Borough, Montgomery County, PA 2019)
- Kidz Konnect Daycare (Whitpain Township, Montgomery County, PA 2018)
- Royal Farm #132 (Towamencin Township, Montgomery County, PA 2017)
- Dooley Residence (Whitemarsh Township, Montgomery County, PA, 2017)

2.0 PROJECT/SITE BACKGROUND INFORMATION

The site consists of land identified as 222 Church Road located in Cheltenham Township, Montgomery County, PA. The project proposes to subdivide the existing property into ten (10) separate parcels and includes an extension of Harrison Avenue to create a cul-de-sac. Lots 1 thru 4 and 6 thru 8 will be developed into proposed single-family dwellings that front the new extension of Harrison Avenue. Lot 5 will be developed into a proposed single-family dwelling that fronts Church Road (Sr 2023). Lot 9 will remain as an existing dwelling and include a proposed trail extension to connect to the existing Tookany Creek Trail. Lot 10 will remain as open space and be dedicated to Cheltenham Township. Each proposed dwelling includes a driveway for access to the attached garage, a lead walk from the driveway to the front door of the dwelling, and a patio at the rear of the dwelling. An above ground infiltration basin is proposed at the southern end of the development that spans across the rear of Lots 6 thru 8. The NPDES project site boundary and limits of earth disturbance for the project have been defined on the accompanying "PCSM Plan" sheets contained within the "Final Subdivision & Land Development Plan for 222 Church Road".

The development site is within the Tacony Creek-Frankford Creed watershed (A.K.A. Tookany Creek), which is a tributary of the Delaware River. A portion of the development site drains overland directly to Tookany Creek which is located within the adjacent Township-owned property to the south of the subject development. The remainder of the development site drains overland to on-site wetlands which drain overland into the Tookany Creek. The receiving waters have a stream classification, pursuant to PA Chapter 93, of WWF (Warm Water Fishery) and MF (Migratory Fish). FEMA Flood Insurance Rate Maps indicate that the 100-year Floodplain of Tookany Creek extends into the southern portion of the property designated as Lot 10 and is fully outside of the development area with the exception of the proposed trail connection and sanitary sewer replacement.

<u>Natural Resources</u> – A site evaluation has been performed by a wetland scientist and determined that regulated waters, including wetlands, are present within the subject property. These surface waters have been depicted on the accompanying Land Development Plans and are located outside of any development and earth disturbance activities.

A Pennsylvania Natural Diversity Inventory (PNDI) report was prepared on June 27, 2023 and indicates that there are no known impacts.

Drainage Conditions – In general, the site drains in a southerly direction towards the Tookany Creek. The project has been determined to contain two (2) distinct study points, defined as Point of Discharge (POD) #1 and POD #2. POD #1 has been defined as the portion of the site that drains to Tookany Creek upstream of the recently constructed Township trail crossing of Tookany Creek and coincides with the discharge location of the proposed above ground infiltration basin (BMP ID 001) located along the rear of Lots 6 thru 8. POD #2 has been defined as the portion of the site that drains to the on-site wetland (Wetland A) and ultimately Tookany Creek downstream of the recently constructed Township trail crossing of Tookany Creek. In the existing conditions, both POD's receive primarily sheet flow and shallow concentrated flow from the upland residential properties. There are no distinct stormwater facilities or outfalls that drain to these POD's in the existing conditions.

In the proposed conditions, the same general drainage patterns are maintained to the greatest extent possible and the locations of POD #1 and POD #2 remain the same. Some of the area

that was tributary to POD #2 in the existing conditions will be directed towards the BMP ID 001 in the proposed conditions and subsequently POD #1. POD #2 will continue to receive primarily sheet flow and shallow concentrated flow from upland residential properties in the proposed conditions. The proposed stormwater management program provides an overall reduction in peak rate and volume of runoff to the receiving waters.

Infiltration and Geological Studies – Infiltration testing at the site was performed by Penn's Trail Environmental, LLC detailed in a report issued on February 2, 2022 which has been included as an appendix within this report. As part of the investigation, 6 test pits were dug across the site which yielded favorable conditions for infiltration. Test Pits (TP) #5 and #6, specifically, are located within the footprint of the proposed above ground infiltration basin (BMP ID 001) and yielded rates of 0.43 and 4.11 inches per hour, respectively. A factor of safety of 2 was applied to these raw test rates and the geomean was utilized in accordance with the PADEP BMP Manual which resulted in a design infiltration rate of 0.66 inches per hour. The infiltration tests performed in TP#5 and TP#6 were within 1 foot of the proposed infiltration elevation of BMP ID 001.

3.0 DISCUSSION OF BEST MANAGEMENT PRACTICES

The project proposes the use of various BMPs to meet the design requirements both during and post construction. Items of implementation include:

Erosion and Sediment Control BMPs:

- **Rock Construction Entrance:** Two rock construction entrances will be installed to provide a stabilized site access from both Church Road and Harrison Avenue.
- **Pumped Water Filter Bags:** Filter bags will be utilized as needed to pump water out of low areas during construction.
- **Concrete Washout:** All excess concrete products and mixed concrete will be contained within the washout area to prevent pollution during rain events.
- Compost Filter Socks: In areas where minimal runoff is expected, compost filter socks are proposed to intercept construction runoff and filter before discharge from the site. The perimeter of the disturbance areas will be installed with Compost Socks which are an ABACT device for use to control siltation concerns of the watersheds TMDL requirements.
- Erosion Control Blanket: All slopes at a grade of 3:1 or steeper will be installed with slope protection matting to prevent unnecessary erosion of graded areas. Matting will also be installed within the permanent emergency spillway of Sediment Trap #1/BMP ID 001 to prevent erosion should the spillway be activated.
- Sediment Trap/Compost Filter Sock Sediment Trap: A sediment trap is proposed to detain sediment laden runoff prior to discharging from the site. Detaining the runoff allows for sediment and other pollutants to settle out within the trap prior to the stormwater discharging from the site.
- **Riprap Aprons:** Riprap aprons will be installed at all pipe discharge locations to prevent accelerated erosion that would otherwise result from the concentrated runoff.

• **Temporary Topsoil Stockpile:** A topsoil stockpile has been provided on site to provide a location to store topsoil.

Post-Construction Stormwater Management

• Raingarden/Bioretention Basin (BMP ID 001): The proposed installation a bioretention basin will provide storage of runoff allowing for evapotranspiration and infiltration of runoff in accordance with volume, peak rate, and water quality requirements. This facility has been designed to infiltrate a specified volume of runoff while still dewatering sooner than 72 hours after the end of the design storm.

<u>Design Methodologies</u> – The project was designed in accordance with the local ordinance regulations for Cheltenham Township including, but not limited to, the Subdivision and Land Development Ordinance, the Zoning Ordinance and the Stormwater Management Ordinance; and the requirements of the Pennsylvania Department of Environmental Protection to procure the NPDES permit.

<u>Erosion & Sediment Pollution Control</u> – The following reference materials and manuals were used in the design of the erosion control measures.

• Erosion and Sediment Pollution Control Program Manual, Department of Environmental Protection, dated March 2012.

<u>Stormwater Management</u> – The following reference materials and manuals were used in the design of the stormwater management system.

- Cheltenham Township Stormwater Management Ordinance and SALDO
- Urban Hydrology for Small Watersheds TR55, U.S. Sept of Agriculture, Natural Resources Conservation Service, Conservation Engineering Division, dated June 1986 (TR55)
- Erosion and Sediment Pollution Control Program Manual, Department of Environmental Protection Bureau of Watershed Management, dated March 2012 (E&S Manual)
- Pennsylvania Stormwater Best Management Practices, Department of Environmental Protection Bureau of Watershed Management, dated December 30, 2006 (BMP Manual)

<u>Programs, Applications, and References</u> – To perform the necessary calculations the following programs were utilized to generate the variables and outputs.

- Hydraflow Hydrographs Extension for Autodesk Civil 3D by Autodesk, Inc. v2023
- Stormwater Studio 2022 v3.0.0.29
- AutoCAD Civil3D 2023

Precipitation intensity and depth for the design storms used in the supporting calculations was obtained from NOAA Atlas 14, Volume 2, Version 3 for the area in question.

4.0 POST CONSTRUCTION STORMWATER MANAGEMENT DESIGN

The following shall illustrate that the design of this site meets or exceeds the requirements of the appropriate agencies necessary for the approval of the stormwater management systems and issuance of related permits.

4.1 Pre-Development Runoff Rate Analysis

In general, the site drains in a southerly direction towards the Tookany Creek. The project has been determined to contain two (2) distinct study points, defined as Point of Discharge (POD) #1 and POD #2. POD #1 has been defined as the portion of the site that drains to Tookany Creek upstream of the recently constructed Township trail crossing of Tookany Creek and coincides with the discharge location of the proposed above ground infiltration basin (BMP ID 001) located along the rear of Lots 6 thru 8. POD #2 has been defined as the portion of the site that drains to the on-site wetland (Wetland A) and ultimately Tookany Creek downstream of the recently constructed Township trail crossing of Tookany Creek. In the existing conditions, both POD's receive primarily sheet flow and shallow concentrated flow from the upland residential properties. There are no distinct stormwater facilities or outfalls that drain to these POD's in the existing conditions.

The overall drainage area to each POD was delineated and separated into "On-Site" and "Off-Site" areas, with "On-Site" being the portion of the drainage area within the Limit of Disturbance (LOD) and "Off-Site" being areas outside of the LOD that are tributary to the development site. Time of Concentration (Tc) flow paths were delineated and a Tc was calculated for the drainage area to each POD based on TR-55 methodology.

The pre-development rate of runoff was determined for each drainage area in accordance with the Dekalb Rational Method as defined by Hydraflow Hydrographs 2023. The cover conditions identified for the pre-development conditions are as follows:

- **Meadow/Pervious** C-Value = 0.25
- Impervious Areas C-Value = 0.95

A weighted 'C' value was determined for each drainage area and used in conjunction with the calculated Tc to determine the pre-development peak rate of runoff to the POD.

4.2 Post-Development Runoff Rate Analysis

The post-development conditions were evaluated utilizing the same procedures defined for the pre-development condition. On-Site and Off-Site drainage areas were delineated for the proposed stormwater BMP as well as bypass areas that drain to each POD. Similar to the pre-development condition, a post-development Tc path was delineated for each drainage area and a Tc was calculated based on TR-55 methodology. The cover conditions identified for the pre-development conditions are as follows:

- Off-Site/Undisturbed Pervious C-Value = 0.25
- **On-Site Lawns/Pervious** C-Value = 0.35
- Impervious Areas C-Value = 0.95

In the post-development conditions, additional impervious was accounted for on each proposed lot (Lots 1 thru 8) to account for future variations in the amount of impervious cover proposed compared to what is currently shown on the accompanying Land Development Plans. Each lot (Lots 1 thru 8) were allotted an additional 500 square feet beyond what is currently shown on the Land Development Plans, a total of 0.09 Acres of additional impervious. The stormwater management system and all runoff, volume, and water quality calculations were prepared accounting for this additional 0.09 Acres of impervious coverage.

A weighted 'C' value was determined for each drainage area and used in conjunction with the calculated Tc for each area in order to determine the post-development peak rates. The areas draining to the proposed basins were routed using the Hydraflow Hydrographs software, and the resultant flow was added to the Bypass area peak rate in order to determine the total resultant flow to each POD.

Per the Cheltenham Township Stormwater Management Ordinance, Section 290-23, project site is located in Stormwater District 'B' of the Tookany Creek Watershed. Stormwater District 'B' has the following peak rate reduction criteria:

Table 1: Required Peak Rate Reductions per the Cheltenham Township Stormwater Management Ordinance, Section 290-23, for Stormwater District 'B'.

Pre-Development Design Storm	Reduce To	Post-Development Design Storm
1-Year Peak	4	2-Year Peak
2-Year Peak		5-Year Peak
5- Year Peak		10- Year Peak
10-Year Peak		25-Year Peak
25-Year Peak		50-Year Peak
100-Year Peak	_	100-Year Peak

The stormwater management system for the site has been designed to reduce the peak rate of runoff from each post-development design storm to be less than the peak rate of runoff from the designated pre-development design storm. A worksheet summarizing the runoff peak rates in the pre-development and post-development conditions and compliance with the criteria listed above are included Appendix A of this report.

4.3 Runoff Volume and Water Quality Analysis

To procure the NPDES permit pursuant to Chapters 93 and 102 of the PA Code, the regulations require that the development manage the difference in runoff volume generated during the 2-yr/24-hr design storm while considering 20% of the pre-development impervious cover as meadow in good condition. To demonstrate compliance, the PADEP PCSM Spreadsheet (included with the supporting calculations) was utilized. Note that 20% of all impervious cover within the limit of disturbance were considered meadow in the pre-development condition. Based on existing and proposed cover conditions and accounting for 20% of the existing impervious as meadow, there is a resultant increase in runoff volume in the 2-yr/24-hr design storm that is managed by the stormwater management system proposed with this development.

To manage the net increase in runoff volume from the 2-yr/24-hr design storm ("Delta-2 Volume") one infiltration BMP is proposed. BMP ID 001 consists of an above ground bioretention basin designed to manage the entire Delta-2 Volume via infiltration and provide water

quality benefits. Compliance with the NPDES volume and water quality criteria are demonstrated via the PADEP PCSM Spreadsheet.

Alternatively, the Cheltenham Township Stormwater Management Ordinance, Sections 290-20 and 290-21, provide separate criteria for Groundwater Recharge and Water Quality Requirements. The ordinance dictates that the Recharge Volume (Rev) and Water Quality Volume (WQv) are both equal to one (1) inch of runoff over all impervious surfaces within the LOD. Based on the provided drainage area tabulation in the post-development conditions, one (1) inch of runoff over all impervious surfaces within the LOD yields a lower volume requirement than the "Delta-2" volume requirement set forth by PA Code described above. Therefore, the proposed stormwater management design for this development meets both the criteria to procure an NPDES Permit as well as the criteria set forth by the Cheltenham Township Stormwater Ordinance.

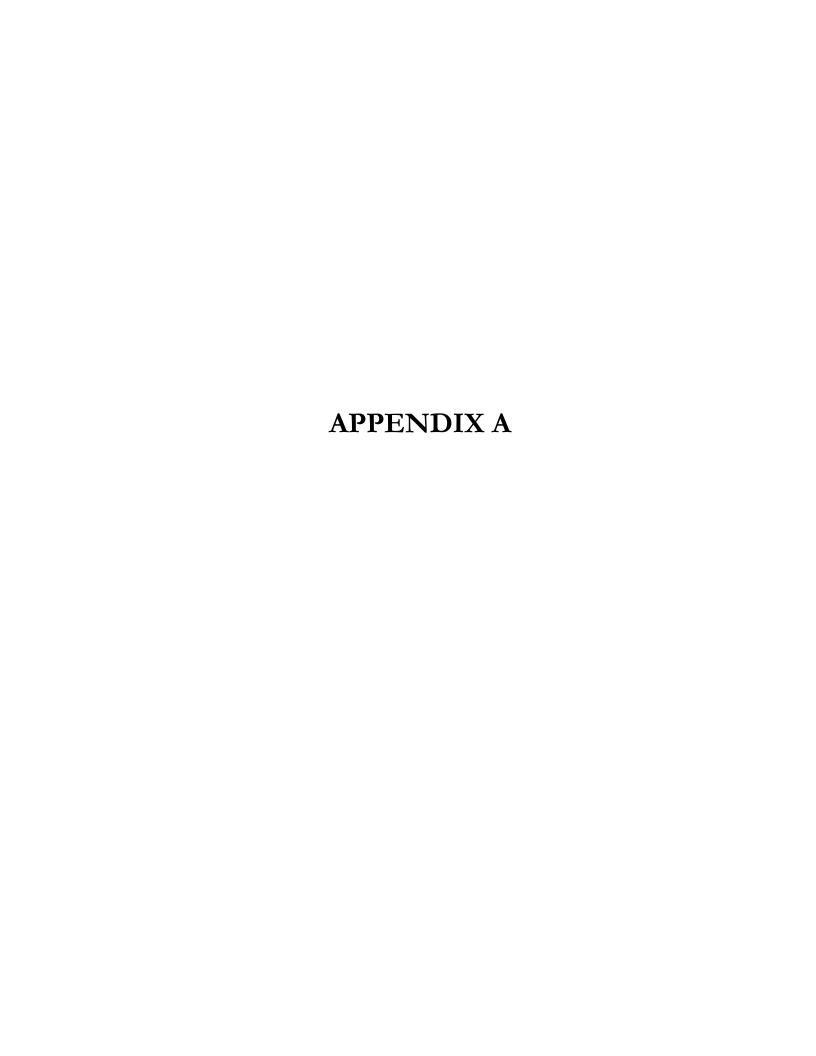
5.0 CONCLUSION

The report demonstrates target criteria for rate, volume and water quality are met through the protection of resources and the installation of BMPs. As such, the proposed design complies with the regulations of the Municipality and the PADEP NPDES Permit.

APPENDIX

APPENDIX

A:	Of	f-site Discharge Analysis
	1.	Existing Conditions & Photos
	2.	Proposed Conditions
	3.	Off-Site Discharge Comparison
	4.	Permanent Erosion Control Measures
B:	Sto	ormwater Management Designs
	1.	Drainage Area Calculations (NRCS & Rational Method) B-1
	2.	PADEP PCSM Spreadsheets B-6
	3.	Time of Concentration CalculationsB-12
	4.	Peak Rate Summary SheetsB-17
	5.	Basin Storage & Design Calculations
	6.	Loading Ratio Calculations
	7.	Conveyance System Model Results B-30
	8.	Riprap Apron Calculations
	9.	Level Spreader Calculations
	10.	Hydrographs B-36
C:	Re	ferences and Supporting Documents
	1.	NOAA Rainfall Data
	2.	Soils Report
	3.	FEMA Flood Map
	4.	Stormwater Infiltration Study & Report prepared by Penn's Trail Environmental
		LLC dated 2/2/2022
	5.	Wetland/Waters Investigation Report prepared by VW Consultants LLC dated April 21, 2023



OFF-SITE DISCHARGE ANALYSIS

Existing Conditions

The site drains in a southerly direction towards the Tacony Creek (A.K.A. Tookany Creek). The project has been determined to contain two (2) distinct study points, defined as Point of Discharge (POD) #1 and POD #2. POD #1 has been defined as the portion of the site that drains to Tookany Creek upstream of the recently constructed Township trail crossing of Tookany Creek and coincides with the discharge location of the proposed above ground infiltration basin (BMP ID 001) located along the rear of Lots 6 thru 8. POD #2 has been defined as the portion of the site that converges to the on-site wetland (Wetland A) and ultimately Tookany Creek downstream of the recently constructed Township trail crossing of Tookany Creek. In the existing conditions, both POD's receive primarily sheet flow and shallow concentrated flow from the upland residential properties. There are no distinct stormwater facilities or outfalls that drain to these POD's in the existing conditions and there are no signs of accelerated erosion resulting from drainage within the development area.

From POD #1, runoff converges at a berm just downstream of the recently constructed Township trail. Runoff then flows through an opening in the berm down a slope to low-lying area within the floodplain of Tookany Creek and ultimately into Tookany Creek itself. The flow path from POD#1 to Tookany Creek is fully on Township-owned land and the ground cover consists of the Township gravel trail and dense vegetation downslope of the trail. There are no signs of accelerated erosion in the existing conditions.

At POD #2, water converges within the upper portion of Wetland 'A' which is an area where small pools of surface water are present and bound by a berm that was previously part of a manmade water conveyance structure reported to have been a mill raceway. The mill raceway has since been abandoned and disconnected from the source of surface water. From the upper portion of Wetland 'A', surface water flows through an opening in the existing berm and travels downslope to the lower portion of Wetland 'A' along the Tookany Creek floodplain. There are no signs of accelerated erosion in the existing conditions.



Figure 1 - Photograph of the southern edge of the property facing towards the southwest corner. Looking towards POD #1 near the left portion of the photo.



Figure 2 - Photograph of the southern edge of the property in the vicinity of POD #1 facing towards the southeast corner.



Figure 3 - Photograph from the vicinity of POD #1 looking southeast towards the Township trail. The existing berm can be seen beginning at the bend in the trail. Runoff that crosses the trail gets redirected by the berm and flows to the southwest towards the opening in the berm.



Figure 4 - Photograph along the flow path to receiving waters downstream of POD #1. Standing along the existing berm looking southwest towards the opening in the berm.



Figure 5 - Photograph of the opening in the berm along the flow path from POD #1 to the receiving waters. Beyond this opening, runoff flows across densely vegetated low-lying land until reaching the Tookany Creek.



Figure 6 - Photograph of the abandoned & disconnected old mill race at the southern edge of the subject property, facing southeast towards POD #2 and the upper portion of Wetland 'A'.



Figure 7 - Photograph in the vicinity of POD #2 and the upper portion of Wetland 'A', looking south towards the opening in the berm that allows surface water to drain downslope to the lower portion of Wetland 'A' and ultimately Tookany Creek.

Proposed Conditions

In the proposed conditions, the same general drainage patterns are maintained to the greatest extent possible and the locations of POD #1 and POD #2 remain the same. Some of the area that was tributary to POD #2 in the existing conditions will be directed towards BMP ID 001 in the proposed conditions and subsequently POD #1. The discharge of BMP ID 001 will first drain to a level spreader (LS#1) prior to the outflow reaching POD #1. The level spreader has been designed to distribute the controlled runoff as sheet flow to the existing stabilized vegetated areas downstream of the subject development. POD #2 will continue to receive primarily sheet flow and shallow concentrated flow from upland residential properties in the proposed conditions.

Off-Site Discharge Comparison

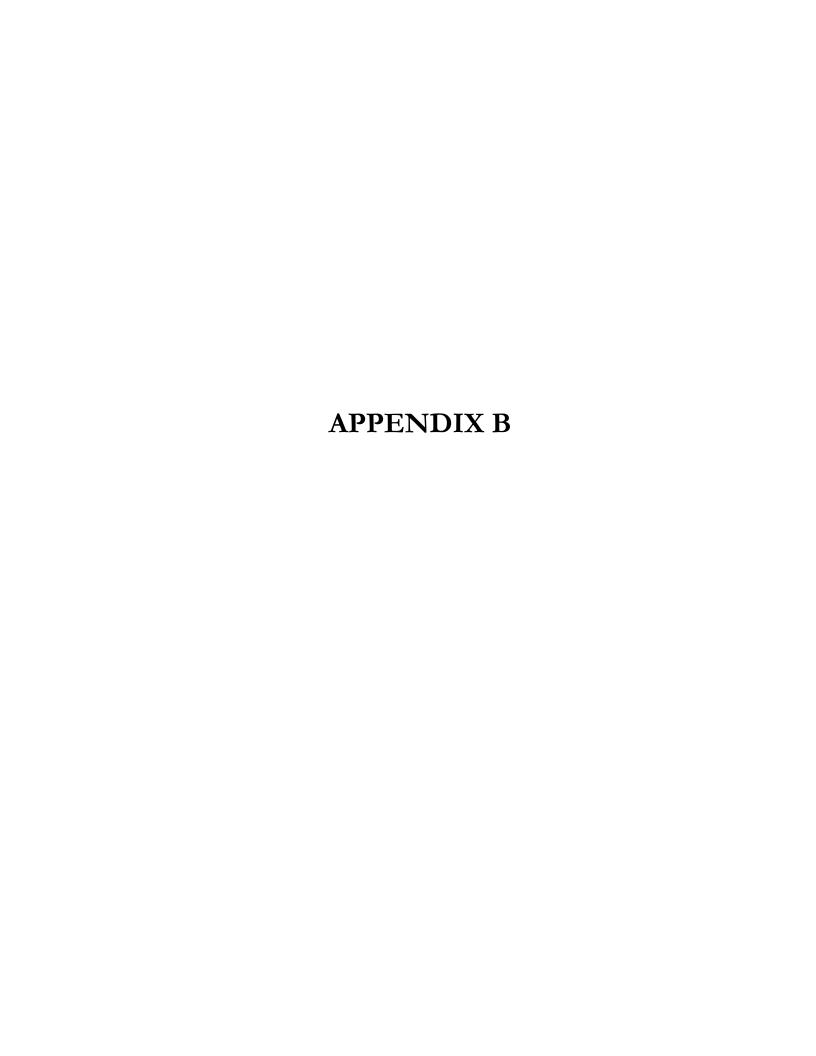
The same general drainage patterns and Points of Discharge are maintained between the predevelopment and post-development conditions. There is also a net reduction in the peak rate and volume of runoff draining to each POD. Since there are no signs of accelerated erosion as the site exists today (as documented in the photos above) and there is a reduction in peak rate and volume of runoff to each POD, there are no increase in erosion anticipated from this proposed development.

In addition, POD #2 coincides with Wetland 'A' as described in the Existing Conditions section of this analysis. Per the DEP Spreadsheet results for DP-002, there is a minor reduction in runoff volume and peak rate to DP-002 that results from the proposed development, and a decrease in pollutant loading that

results from the decrease in runoff volume. Therefore, the proposed development is not anticipated to degrade the quality of Wetland 'A'. Further, a Wetland/Waters Investigation has been prepared by VW Consultants LLC dated April 21, 2023 which has been included as Appendix C.5. of this report. This investigation documents that Wetland 'A' has two main portions, one being the small area of closed grading where surface water is present and the other being the lower portion downslope of the existing berm. For the upper portion that coincides with DP-002, it is believed to be fed by shallow groundwater and transmission of infiltrated water to this low point. The lower portion of the wetland is believed to be fed by regional groundwater discharge. Therefore, the slight reductions to surface runoff that will result from this development will have a de minimis impact on the source hydrology of the receiving wetland.

Permanent Erosion Control Measures

In addition to reducing the peak rate and volume of runoff draining to the receiving waters, the discharge of Sediment Trap #1/BMP ID 001 is proposed to have a level spreader to provide energy dissipation and distribute the basin outflow as sheet flow prior to reaching POD #1.





222 Curch Road [2154-10] PROJECT:

Cheltenham Township LOCATION:

COUNTY: Montgomery County, PA

PRE-DEV DRAINAGE AREA CALCULATIONS (NRCS)

Q = [(P - 0.2S)2 / (P + 0.8S)] * 1/12 * 43,560Reference Formula:

S = (1000/CN) - 10 P = 3.30 3.30

in. (rainfall depth of 2-year, 24-hour storm)

			Volume (Ft ³)	9,554	11,745	4,424	9,263						34,986
		Weighted CN	Value	73	92	74	62						
	Total	Drainage Area Weighted CN	(Ac.)	2.35	2.41	1.05	1.63						7.44
	Impervious	Sport Deliver	86	0.20	0.51	0.12	0.48						1.31
	Meadow	(HSG-C)	7.1	2.15	1.70	0.89	1.15						5.89
reas (Ac.)	Meadow	(HSG-B)	28	0.00	0.20	0.04	0.00						0.24
CN VALUES / Drainage Areas (Ac.)													0.00
CN VALU													0.00
													0.00
													00.00
	Orainage Area ID			DA to POD 001 (On-Site)	DA to POD 001 (Off-Site)	DA to POD 002 (On-Site)	DA to POD 002 (Off-Site)						Totals



222 Curch Road [2154-10] **Cheltenham Township** PROJECT: LOCATION:

Montgomery County, PA COUNTY:

POST-DEV DRAINAGE AREA CALCULATIONS (NRCS)

Reference Formula:

S = (1000/CN) - 10P = 3.30

Q = [(P - 0.2S)2 / (P + 0.8S)] * 1/12 * 43,560

in. (rainfall depth of 2-year, 24-hour storm)

			CN VALU	CN VALUES / Drainage Areas (Ac.)	Areas (Ac.)					
					Open	Open				
Drainage Area ID					Space/Lawns (HSG-B)	space/Lawns (HSG-C)	Impervious	Total Drainage Area	Weighted CN	Runoff
					61	74	86	(Ac.)	Value	Volume (Ft ³)
To BMP 001 (On-Site)*					0.00	1.34	1.16	2.50	85	18,285
To BMP 001 (Off-Site)					0.00	1.46	0.57	2.03	81	12,197
Bypass to POD #1 (On-Site)					0.00	0.38	0.08	0.46	82	2,413
Bypass to POD #1 (Off-Site)					0.20	0.57	0.14	0.91	52	4,195
Bypass to POD #2 (On-Site)					0.02	0.33	60:0	0.44	82	2,360
Bypass to POD #2 (Off-Site)					0.00	0.82	0.28	1.10	08	6,403
Totals	0.00	00:00	0.00	0.00	0.22	4.90	2.32	7.44		45,853

^{*} On-Site Drainage Area to BMP 001 accounts for an additional 500 SF (0.09 Ac) of impervious on Lots 1 thru 8 beyond what is currently displayed on the plans to allow for minor modifications to building footprint, walkways, patios, or other impervious surfaces.



PROJECT: 222 Curch Road [2154-10]
LOCATION: Cheltenham Township
COUNTY: Montgomery County, PA

PRE-DEVELOPMENT DRAINAGE AREA CALCULATIONS (Rational Method)

Drainage Avec	'	'C'-Value / Draiı	nage Areas (Ac.)		
Drainage Area ID	Impervious		Pervious	Woods	Total Area	Weighted
l lb	0.95		0.25	0.15	(Ac.)	'C'
DA to POD 001 (On-Site)	0.20		2.15	0.00	2.35	0.31
DA to POD 001 (Off-Site)	0.51		1.90	0.00	2.41	0.40
DA to POD 002 (On-Site)	0.12		0.93	0.00	1.05	0.33
DA to POD 002 (Off-Site)	0.48		1.15	0.00	1.63	0.46
Totals	1.31	0.00	6.13	0.00	7.44	



PROJECT: 222 Curch Road [2154-10]
LOCATION: Cheltenham Township
COUNTY: Montgomery County, PA

POST-DEVELOPMENT DRAINAGE AREA CALCULATIONS (Rational Method)

		C'-Value / Drai	nage Areas (Ac.)		
Drainage Area ID	Impervious	Pervious (Off-Site)	Pervious	Woods	Total Area	Weighted
	0.95	0.25	0.35	0.15	(Ac.)	'C'
To BMP 001 (On-Site)*	1.16	0.00	1.34	0.00	2.50	0.63
To BMP 001 (Off-Site)	0.57	1.46	0.00	0.00	2.03	0.45
Bypass to POD #1 (On-Site)	0.08	0.00	0.38	0.00	0.46	0.45
Bypass to POD #1 (Off-Site)	0.14	0.77	0.00	0.00	0.91	0.36
Bypass to POD #2 (On-Site)	0.09	0.00	0.35	0.00	0.44	0.47
Bypass to POD #2 (Off-Site)	0.28	0.82	0.00	0.00	1.10	0.43
Totals	2.32	3.05	2.07	0.00	7.44	

^{*} On-Site Drainage Area to BMP 001 accounts for an additional 500 SF (0.09 Ac) of impervious on Lots 1 thru 8 beyond what is currently displayed on the plans to allow for minor modifications to building footprint, walkways, patios, or other impervious surfaces.



INLET DRAINAGE AREA CALCULATIONS (Rational Method)

Storm Structure		'C'-Value / Drai	nage Areas (Ac.)		
ID	Impervious		Pervious		Total Area	Weighted
U	0.95		0.35		(Ac.)	'C'
INL-3	0.18		0.15		0.33	0.68
INL-4	0.38		0.79		1.17	0.54
INL-5	0.26		0.49		0.75	0.56
INL-6	0.72		0.98		1.70	0.60
Totals	1.54	0.00	2.41	0.00	3.95	



General Information

Quality

Rate

Volume

General

Instructions

rioject Name.	222 Church Road		Application Type:	PAG-02 NOI
County:	Montgomery		Municipality:	Cheltenham Township
Project Type: Sin	Single-Family Housing	bo	New Project	O Minor / Major Amendment
Total Project Site Area: (In Watershed)	7.44	acres	Total Earth Disturbance: (In Watershed)	nce: 3.40 acres
of Post-Constructio	No. of Post-Construction Discharge Points:	1	Start DP Numbering at:	at: 001

Discharge	Orainage Area	Earth Existing Discharge Area Disturbance in Impervious in	Existing Impervious in	Proposed Impervious in		£6 4J	Ch 93 Structural
Point (DP) No. (DA) (acres)	(DA) (acres)	DA (acres)	DA (acres)	DA (acres)	Receiving Waters	Class	BMP(s)
					Discharge to Non-Surface		
001	4.53	2.50	0.71	1.73	Waters (To Tookany Creek) WWF, MF	WWF, MF	Yes
Undetained					Discharge to Non-Surface		
Areas	1.37	0.46	0.00	0.22	Waters (To Tookany Creek) WWF, MF	WWF, MF	
Totals:	5.90	2.96	0.71	1.95			

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Volume Management

Project: 222 Church Road

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Que	
Rate	
Volume	
General	
Instructions	

Exempt from Meadow in Good Condition | | Automatically Calculate CN 1a, Runoff and Volume inches Alternative 2-Year / 24-Hour Storm Event: Alternative Source: Г inches No. Rows: 3.3 2-Year / 24-Hour Storm Event (NOAA Atlas 14):

Pre-Construction Conditions:	No. Rows: 4	☐ Exempt f	^r rom Meadow in	☐ Exempt from Meadow in Good Condition ☑ Automatically Calculate CN, Ia, Runoff and Volume	✓ Automa	tically Calculo	ıte CN, Ia, Runofj	^c and Volume
Land Cover			Area (acres)	Soil Group	CN	la (in)	Q Runoff (in)	la (in) Q Runoff (in) Runoff Volume (cf)
Pervious as Meadow			0.00	В	58	1.448	0.38	0
Pervious as Meadow			2.15	J	71	0.817	0.94	7,327
Impervious as Meadow			0.04	J	71	0.817	0.94	136
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	loofs, Driveways, Etc. (Exclu	uding ROW)	0.16	N/A	86	0.041	3.07	1,781

9,245

TOTAL (CF):

2.35 TOTAL (ACRES):

m

No. Rows:

Post-Construction Conditions:

Land Cover	Area (acres)	Soil Group		la (in)	Q Runoff (in)	CN la (in) Q Runoff (in) Runoff Volume (cf)	
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	0.00	В	61	1.279	0.49	0	
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	1.72	O	74	0.703	1.10	6,893	
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	1.24	N/A	86	0.041	3.07	13,806	

NET CHANGE IN VOLUME TO MANAGE (CF):

11,454

20,698

TOTAL (CF):

2.96

TOTAL (ACRES):

POD#1 Page 2

9/13/2023

Structural BMP Volume Credits: No. 3

No. Structural BMPs:

Discharge

MRC3

BMP Name

BMP No.

DP No.

Off-Site

Rain Garden / Bioretention

001

Start BMP Numbering at:

Media Depth (ft)	4.0
Vegeta- ted?	Yes
Infiltration Infiltration Vegeta- Rate (in/hr) Period (hrs) ted?	43
Infiltration Rate (in/hr)	99.0
Volume Infiltration Routed to / Vegetated Routed SMP (CF) Area (SF)	3,971
Volume Routed to BMP (CF)	18,285
ncremental Volume BMP DA Routed to (acres) BMP (CF)	2.50

ET Credit (CF)

Infiltration Credit (CF)

Storage Volume

(G

INFILTRATION & ET CREDITS (CF):

12,376

3,923

8,452

9,273 **Totals**:

8,452

NET CHANGE IN VOLUME TO MANAGE (CF): 11,454
TOTAL CREDITS (CF): 12,376

VOLUME REQUIREMENT SATISFIED

9/13/2023



Rate Control

Project: 222 Church Road

uality

ŏ	
Rate	
Volume	
General	
Instructions	

Precipitation Amounts:

NOAA 100-Year 24-Hour Storm Event (in): NOAA 50-Year 24-Hour Storm Event (in): NOAA 10-Year 24-Hour Storm Event (in): NOAA 2-Year 24-Hour Storm Event (in):

3.3	4.91	6.9	7.9

Alternative 100-Year 24-Hour Storm Event (in): Alternative 10-Year 24-Hour Storm Event (in): Alternative 50-Year 24-Hour Storm Event (in): Alternative 2-Year 24-Hour Storm Event (in):



✓ Report Summary of Peak Rates Only

Attach model input and output data or other calculations to support the rates reported below.

	Pec	Peak Discharge Rates (cfs)	fs)	
	Pre-Construction	Pre-Construction Post-Construction	Net Change	
2-Year Storm:	7.15	4.67	-2.48	Rat
10-Year Storm:	9.28	7.28	-2.00	Rat
50-Year Storm:	11.01	06'6	-1.11	Rat
100-Year Storm:	11.66	10.87	-0.79	Rat
				_

Page B-9

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Water Quality

Project: 222 Church Road

PRINT

Pre-Construction Pollutant Loads:

Quality

Rate

Volume

General

Instructions

(+code) word for the control of the	Land Cover for Water	Area	Soil	Runott	Polluta	Pollutant Conc. (mg/L) Pollutant Loads (lbs)	(mg/L)	Pollut	ant Loac	(sql) sl
ralid Cover (Floiii voldille Wolkslieet)	Quality	(acres) Group	Group	(cf)	SST	NT dT	N	TSS	ДL	NL
Pervious as Meadow	Grassland/Herbaceous	0.00	В	0	48.8	0.22	2.30	2.30 0.00 0.00	00.0	00.0
Pervious as Meadow	Grassland/Herbaceous	2.15	C	7,327	48.8	0.22	2.30	2.30 22.33 0.10	0.10	1.05
Impervious as Meadow	Grassland/Herbaceous	0.04	С	136	48.8	48.8 0.22 2.30 0.42 0.00	2.30	0.42	00.00	0.02
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	Residential	0.16 N/A	N/A	1,781	65.0	0.29 2.05 7.23 0.03	2.05	7.23	0.03	0.23
	TOTAL (ACRES): 2.35	2.35				T	TALS:	TOTALS: 29.97 0.13 1.30	0.13	1.30

Post-Construction Pollutant Loads (without BMPs):

(+codestaction control word) world	Land Cover for Water	Area	Soil	Runoff	Polluta	nt Conc.	(mg/L)	Pollutant Conc. (mg/L) Pollutant Loads (lbs)	ant Load	s (Ibs)
raild Cover (11011) Volunie VVOINSILEEU	Quality	(acres) Group	Group	(cf)	TSS	TP	NT dt	TSS TP	TP	N
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	Open Space	0.00	В	0	78.0	78.0 0.25 1.25	1.25	0.00	0.00	0.00
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	Open Space	1.72	С	6,893	78.0	0.25	1.25	78.0 0.25 1.25 33.57 0.11	0.11	0.54
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	Residential	1.24	N/A	13,806	65.0	0.29	2.05	65.0 0.29 2.05 56.03 0.25	0.25	1.77
	TOTAL (ACRES): 2.96	2.96				T	TALS:	TOTALS: 89.60 0.36 2.31	0.36	2.31

POLLUTANT LOAD REDUCTION REQUIREMENTS (LBS):

59.63

1.01

0.22

POD#1 Page 5

9/13/2023

>

No. Rows:

Land Cover	Area (acres)	Soil Group	S	la (in)	Q Runoff (in)	la (in) Q Runoff (in) Runoff Volume (cf)
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	0	В	61	1.279	0.49	0
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	0.38	J	74	0.703	1.10	1,523
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	0.08	W/N	86	0.041	3.07	168

Non-Structural BMP Water Quality Credits:

☐ Other (attach calculations)

□ Pervious Undetained Area Credit

Structural BMP Water Quality Credits:

☑ Use default BMP Outflows and Median BMP Outflow Concentrations

ON OC	BMP	O O O O O	3CS	BMP	Vol. Routed Inf. & ET	Inf. & ET	Capture & Buffer	Outflow	Outflo	v Conc.	Outflow Conc. (mg/L) Pollutant Loads (lbs)	Polluta	ant Load	s (Ibs)
7.	No.		IW	(acres)	to BMP (CF)	to BMP (CF) Credits (CF)	Credits (CF)	(CF)	TSS	ТР	N	TSS	ТР	TN
001	1	Rain Garden / Bioretention	1	2.50	2.50 18,285	12,376		5,909	10.00	0.24	10.00 0.24 0.96 3.69 0.09 0.35	3.69	60:0	0.35

	155	ISS IP IN	Z	
POLLUTANT LOADS FROM STRUCTURAL BMP (TREATED) OUTFLOWS (LBS): 3.69 0.09 0.35	3.69	0.09	0.35	
POLLUTANT LOADS FROM UNTREATED STORMWATER (LBS): 11.03 0.04 0.23	11.03	0.04	0.23	
NON-STRUCTURAL BMP WATER QUALITY CREDITS (LBS):				
NET POLLUTANT LOADS FROM SITE, POST-CONSTRUCTION (LBS): 14.72 0.13 0.59	14.72	0.13	0.59	
POLLUTANT LOADS FROM SITE, PRE-CONSTRUCTION (LBS): 29.97 0.13 1.30	29.97	0.13	1.30	

WATER QUALITY REQUIREMENT SATISFIED

CERTIFICATION

gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I further certify that the I certify under penalty of law and subject to the penalties of 18 Pa.C.S. § 4904 (relating to unsworn falsification to authorities) that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for structure, function, and calculations contained in this spreadsheet have not been modified in comparison to the spreadsheet DEP has posted to its website or, if modifications were made, an explanation of the modifications made is attached to this spreadsheet.

	Ĭ
Rober E. Blue, Jr., P.E.	preadsheet User Name

9/13/2023

9/12/2023

Date



General Information

Quality

Volume

General

Instructions

Application Type: PAG-02 NOI	Municipality: Cheltenham Township	• New Project O Minor / Major Amendment	Total Earth Disturbance: 3.40 acres (<i>In Watershed</i>)	Start DP Numbering at: 002
Project Name: 222 Church Road	County: Montgomery	Project Type: Single-Family Housing	Total Project Site Area: 7.44 acres (In Watershed)	No. of Post-Construction Discharge Points:

Discharge Point (DP) No.	Drainage Area (DA) (acres)	EarthExistingProposedDischargeDrainage AreaDisturbance in ProposedImpervious in Impervious Impervious in	Existing Impervious in DA (acres)	Proposed Impervious in DA (acres)	Receiving Waters	Ch. 93 Class	Ch. 93 Structural Class BMP(s)
002	1.54	0.44	09:0	0.37	Delineated Wetlands Tributary to Tookany Creek WWF, MF	WWF, MF	No
Undetained Areas							
Totals:	1.54	0.44	9.0	0.37			

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PROJECT SITE MEETS SMALL SITE EXCEPTION - RATE WORKSHEET NOT REQUIRED





Volume Management

Project: 222 Church Road

thes Alternative 2-Year / 24-Hour Storm Event:

☐ Exempt from Meadow in Good Condition ☑ Automatically Calculate CN, Ia, Runoff and Volume

No. Rows: 4

Pre-Construction Conditions:

Land Cover	Area (acres)	Soil Group	S	la (in)	Q Runoff (in)	la (in) Q Runoff (in) Runoff Volume (cf)
Pervious as Meadow	0.04	B	58	1.448	88:0	55
Pervious as Meadow	0.89	O	71	0.817	0.94	3,033
Impervious as Meadow	0.02	O	71	0.817	0.94	89
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	0.10	N/A	86	0.041	3.07	1,113
TOTAL (ACRES):	1.05				TOTAL (CF):	4,269

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6
:: No. Rows
Post-Construction Conditions

Land Cover	Area (acres)	Area (acres) Soil Group	CN	la (in)	Q Runoff (in)	la (in) Q Runoff (in) Runoff Volume (cf)
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	0.02	В	61	1.279	0.49	35
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	0.33	Э	74	0.703	1.10	1,322
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	60:0	N/A	86	0.041	3.07	1,002
TOTAL (ACRES):	0.44				TOTAL (CF):	2,360

NET CHANGE IN VOLUME TO MANAGE (CF):

-1,910

POD#2 Page 2

9/12/2023

Non-Structural BMP Volume Credits:

ET Credit (CF)		
Infiltration Credit (CF)		
Storage Volume (CF)		Totals:
Media Depth (ft)		
Vegeta- ted?		
Infiltration Period (hrs)		
Infiltration Rate (in/hr)		
Infiltration / Vegetated Area (SF)		
Volume Routed to BMP (CF)		
Incremental BMP DA (acres)		•
Discharge		
MRC3		
BMP Name		
BMP No.		
DP No.		
	BMP Name Discharge BMP DA Routed to Area (SF) Rate (in/hr) Period (hrs) Redia Vegeta- Media Volume (acres) BMP (CF) Area (SF) (Acres (in/hr) Period (hrs) Routed to (Acres (in/hr) Period (hrs) Routed (BMP BMP Name Z Discharge BMP DA Routed to / Vegetated No.

Other (attach calculations):

☐ Tree Planting Credit

TOTAL CREDITS (CF): VOLUME REQUIREMENT SATISFIED

-1,910

NET CHANGE IN VOLUME TO MANAGE (CF):

INFILTRATION & ET CREDITS (CF):

9/12/2023



Project: 222 Church Road

Rate Control

Quality	
Rate	
Volume	
General	
Instructions	

SMALL SITE EXCEPTION SATISFIED: RATE CONTROL NOT REQUIRED

Precipitation Amounts:

NOAA 50-Year 24-Hour Storm Event (in): NOAA 10-Year 24-Hour Storm Event (in): NOAA 2-Year 24-Hour Storm Event (in):

4.91 6.9 7.9 3.3

Alternative 100-Year 24-Hour Storm Event (in): Alternative 10-Year 24-Hour Storm Event (in): Alternative 50-Year 24-Hour Storm Event (in): Alternative 2-Year 24-Hour Storm Event (in):

✓ Report Summary of Peak Rates Only

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NOAA 100-Year 24-Hour Storm Event (in):

Attach model input and output data or other calculations to support the rates reported below.

	ъ	Peak Discharge Rates (cfs)	fs)	
	Pre-Construction	Post-Construction	Net Change	
2-Year Storm:	5.06	3.14	-1.92	Ra
10-Year Storm:	6.53	4.05	-2.48	Ra
50-Year Storm:	2.73	4.80	-2.93	Ra
100-Year Storm:	8.19	5.08	-3.11	Ra

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Water Quality

Project: 222 Church Road

PRINT

Pre-Construction Pollutant Loads:

Quality

Rate

Volume

General

Instructions

(+codellective control of control	Land Cover for Water	Area	Soil	Runoff	Polluta	Pollutant Conc. (mg/L) Pollutant Loads (lbs)	(mg/L)	Pollut	ant Load	(sql) s
ralid Cover (Floiii voldille Wolkslieet)	Quality	(acres) Group	Group	voidine (cf)	TSS	dТ	NT TP	SSI	dТ	NL
Pervious as Meadow	Grassland/Herbaceous	0.04	В	25	48.8	0.22 2.30 0.17 0.00	2.30	0.17	00.0	0.01
Pervious as Meadow	Grassland/Herbaceous	0.89	C	3,033	48.8	0.22 2.30 9.24 0.04	2.30	9.24	0.04	0.44
Impervious as Meadow	Grassland/Herbaceous	0.02	C	89	48.8	0.22 2.30 0.21 0.00	2.30	0.21	00.0	0.01
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	Residential	0.10 N/A	N/A	1,113	65.0	0.29 2.05 4.52 0.02	2.05	4.52	0.02	0.14
	TOTAL (ACRES): 1.05	1.05				T	TALS:	TOTALS: 14.14 0.06 0.60	90.0	09.0

Post-Construction Pollutant Loads (without BMPs):

(+codyland Mountain	Land Cover for Water	Area	Soil	Runoff	Polluta	nt Conc.	(mg/L)	Pollutant Conc. (mg/L) Pollutant Loads (lbs)	ant Load	s (Ibs)
raild Cover (11011) Voldine Worksheet)	Quality	(acres)	(acres) Group	(cf)	TSS	NT dt	NL	SST	TP	Ę
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover	Open Space	0.02	В	35	78.0	0.25	1.25	0.17	00.0	0.00
> 75%)										
Open Space (Lawns, Parks, Golf Courses,										
Cemeteries, Etc.) - Good Condition (Grass Cover	Open Space	0.33	U	1,322	78.0	0.25	1.25	6.44	0.02	0.10
>75%)										
Impervious Areas: Paved Parking Lots, Roofs,		Ö	4	9	Ĺ	Ċ	L C	,	ć	,
Driveways, Etc. (Excluding ROW)	Kesidential	60.0	N/A	1,002	65.0	0.29	2.05	65.0 0.29 2.05 4.07	0.02	0.13
	TOTAL (ACRES):	0.44				ĭ	OTALS:	TOTALS: 10.68 0.04 0.23	0.04	0.23

9/12/2023

00.0 POLLUTANT LOAD REDUCTION REQUIREMENTS (LBS):

0.00

0.00

Page 5

Σ

Land Cover	Area (acres)	Area (acres) Soil Group	CN	la (in)	Q Runoff (in)	CN la (in) Q Runoff (in) Runoff Volume (cf)
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	0.02	8	61	1.279	67'0	35
Open Space (Lawns, Parks, Golf Courses, Cemeteries, Etc.) - Good Condition (Grass Cover > 75%)	0.33	3	74	0.703	1.10	1,322
Impervious Areas: Paved Parking Lots, Roofs, Driveways, Etc. (Excluding ROW)	0.09	N/A	86	0.041	3.07	1,002

Non-Structural BMP Water Quality Credits:

☐ Other (attach calculations)

☐ Pervious Undetained Area Credit

Structural BMP Water Quality Credits:

☑ Use default BMP Outflows and Median BMP Outflow Concentrations

ı			
	(sql) s	NL	
	ant Load	TP	
	Polluta	TSS	
	mg/L)	TN TSS TP	
	v Conc. (TSS TP	
	Outflow Conc. (mg/L) Pollutant Loads (lbs)	TSS	
	Outflow		
	Capture & Buffer	Credits (CF)	
	Inf. & ET	Credits (CF)	
	Vol. Routed Inf. & ET	to BMP (CF) Credits (CF) Credits (CF)	
	BMP		
	SC?	-W	
	OMEN GIANG		
	BMP	No.	
-	ON GO		

NT	0.00	0.23		0.23	09.0
TP	0.00	0.04		0.04	90.0
TSS	0.00	10.68		10.68	14.14
	POLLUTANT LOADS FROM STRUCTURAL BMP (TREATED) OUTFLOWS (LBS): 0.00 0.00	POLLUTANT LOADS FROM UNTREATED STORMWATER (LBS): 10.68 0.04 0.23	NON-STRUCTURAL BMP WATER QUALITY CREDITS (LBS):	NET POLLUTANT LOADS FROM SITE, POST-CONSTRUCTION (LBS): 10.68 0.04 0.23	POLLUTANT LOADS FROM SITE, PRE-CONSTRUCTION (LBS): 14.14 0.06 0.60

CERTIFICATION

WATER QUALITY REQUIREMENT SATISFIED

gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I further certify that the I certify under penalty of law and subject to the penalties of 18 Pa.C.S. § 4904 (relating to unsworn falsification to authorities) that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for structure, function, and calculations contained in this spreadsheet have not been modified in comparison to the spreadsheet DEP has posted to its website or, if modifications were made, an explanation of the modifications made is attached to this spreadsheet.

	a.
oer E. Blue, Jr., P.E.	preadsheet User Name
Rober E. B	preadshee

9/12/2023

9/12/2023

Date



PROJECT: 222 Church Road [2154-10]

LOCATION: Cheltenham Township

COUNTY: Montgomery County, PA

TR-55 Method - Time of Concentration (Tc) Calculations POINT OF DISCHARGE #1 (PRE-DEVELOPMENT)

Sheet Flow Segment ID AB Range (natural)
1. Surface Description (table 3-1)
2. Manning's roughness coefficient., n (table 3-1) 3. Flow length, L
3. Flow length, L
4. Two-yr 24-hr rainfall, P ₂
5. Land slope, s
Shallow Concentrated Flow Segment ID BC CD DE EF 7. Surface Description (paved or unpaved) Paved Unpaved Paved Unpaved 8. Flow length, L FT 240 330 11 271 9. Watercourse slope, s FT/FT 0.0630 0.1270 0.0300 0.0616 10. Average velocity, V (figure 3-1) FT/Sec 5.14 5.77 3.55 4.01
Shallow Concentrated Flow Segment ID BC CD DE EF 7. Surface Description (paved or unpaved) Paved Unpaved Unpaved Unpaved 8. Flow length, L FT 240 330 11 271 9. Watercourse slope, s FT/FT 0.0630 0.1270 0.0300 0.0616 10. Average velocity, V (figure 3-1) FT/Sec 5.14 5.77 3.55 4.01
7. Surface Description (paved or unpaved) Paved Unpaved Paved Unpaved 8. Flow length, L 5. FT (PT) 240 330 11 271 9. Watercourse slope, s 5. FT/FT 0.0630 0.1270 0.0300 0.0616 10. Average velocity, V (figure 3-1) 5.77 3.55 4.01
7. Surface Description (paved or unpaved) Paved Unpaved Paved Unpaved 8. Flow length, L 5. FT (PT) 240 330 11 271 9. Watercourse slope, s 5. FT/FT 0.0630 0.1270 0.0300 0.0616 10. Average velocity, V (figure 3-1) 5.77 3.55 4.01
7. Surface Description (paved or unpaved) Paved Unpaved Paved Unpaved 8. Flow length, L 5. FT (PT) 240 330 11 271 9. Watercourse slope, s 5. FT/FT 0.0630 0.1270 0.0300 0.0616 10. Average velocity, V (figure 3-1) 5.77 3.55 4.01
8. Flow length, L FT 240 330 11 271 9. Watercourse slope, s FT/FT 0.0630 0.1270 0.0300 0.0616 10. Average velocity, V (figure 3-1) FT/Sec 5.14 5.77 3.55 4.01
9. Watercourse slope, s
10. Average velocity, V (figure 3-1)FT/Sec 5.14 5.77 3.55 4.01
11. T _c = L / 3600VHR 0.0130 + 0.0159 + 0.0009 + 0.0188 = 0.0485
<u>Channel Flow</u> Segment ID
12. Cross sectional flow area, aFT ²
13. Wetted perimeter, p _W FT
14. Hydraulic radius, r = a/p _W FT
15. Channel Slope, sFT/FT
16. Manning's roughness coefficientn
17. V=1.49r ^{2/3} s ^{1/2} / nFT/Sec
18. Flow length, LFT
19. T _c = L / 3600 VHR + + =
20. Cummulative Tc in Hours (Sum of Steps 6, 11, & 19)HR 0.1296
Tc in MINUTES = 7.8



PROJECT: 222 Church Road [2154-10]
LOCATION: Cheltenham Township

COUNTY: Montgomery County, PA

TR-55 Method - Time of Concentration (Tc) Calculations POINT OF DISCHARGE #2 (PRE-DEVELOPMENT)

Sheet Flow	Segment ID	AB		BC			
Surface Description (table 3-1)		Range (natural)		Smooth surfaces			
2. Manning's roughness coefficient., n (t	able 3-1)	0.130		0.01			
3. Flow length, L	FT	44		56			
4. Two-yr 24-hr rainfall, P ₂	IN	3.30		3.30			
5. Land slope, s	FT/FT	0.0700		0.1070			
6. $T_c = 0.007(nL)^{0.8} / P_2^{0.5} s^{0.4}$ (Eq. 3-3)	HR	0.0451	+	0.0064	+	=	0.0514

Shallow Concentrated Flow	Segment ID	CD		DE		EF	1	FG		GH		
7. Surface Description (paved or unpav	ved)	Unpaved		Paved		Unpaved		Paved		Unpaved		
8. Flow length, L	FT	221		181		130	1	13		128		
9. Watercourse slope, s	FT/FT	0.0990		0.0500		0.0540		0.0300		0.0680		
10. Average velocity, V (figure 3-1)	FT/Sec	5.09		4.58		3.75	1	3.55		4.21		
11. T _c = L / 3600V	HR	0.0121]+	0.0110	+	0.0096	+	0.0010	+	0.0084	=	0.0421

Channel Flow	Segment ID	HJ	1				
12. Cross sectional flow area, a	FT ²	7.00					
13. Wetted perimeter, p _W	FT	10.32					
14. Hydraulic radius, r = a/p _W	FT	0.678					
15. Channel Slope, s	FT/FT	0.0140					
16. Manning's roughness coefficient	n	0.030					
17. V=1.49r ^{2/3} s ^{1/2} / n	FT/Sec	4.5354					
18. Flow length, L	FT	125					
19. T _c = L / 3600 V	HR	0.0077	+	+		=	0.0077
20. Cummulative Tc in Hours (Sum of S	Steps 6, 11, & 19)			Н	R	0.1012
					Tc in MINUTES	i = [6.1



PROJECT: 222 Church Road [2154-10]

LOCATION: Cheltenham Township COUNTY: Montgomery County, PA

TR-55 Method - Time of Concentration (Tc) Calculations **TO BMP ID 001 (POST-DEVELOPMENT)**

Sheet Flow	Segment ID	AB					
Surface Description (table 3-1)		Range (natural)					
2. Manning's roughness coefficient.,	n <i>(table 3-1)</i>	0.130					
3. Flow length, L	FT	70					
4. Two-yr 24-hr rainfall, P ₂	IN	3.30					
5. Land slope, s	FT/FT	0.0320					
6. $T_c = 0.007 (nL)^{0.8} / P_2^{0.5} s^{0.4}$ (Eq. 3-3))HR	0.0893	+	+	=	0.0893	
	•	_			_	_	_

Shallow Concentrated Flow	Segment ID	ВС		CD		DE		
7. Surface Description (paved or unpay	red)	Paved		Unpaved		Paved		
8. Flow length, L	FT	240		317		76		
9. Watercourse slope, s	FT/FT	0.0630		0.1290		0.0530		
10. Average velocity, V (figure 3-1)	FT/Sec	5.14		5.82		4.71		
11. T _c = L / 3600V	HR	0.0130	+	0.0151	+	0.0045	=	0.0326

Channel Flow	Segment ID	EF] [FG	1		1	
12. Cross sectional flow area, a	FT ²	1.77		1.77				
13. Wetted perimeter, p _W	FT	4.71		4.71				
14. Hydraulic radius, r = a/p _W	FT	0.375		0.375			İ	
15. Channel Slope, s	FT/FT	0.0110		0.0075			İ	
16. Manning's roughness coefficient		0.012		0.012			İ	
17. V=1.49r ^{2/3} s ^{1/2} / n	FT/Sec	6.7721		5.5919			İ	
18. Flow length, L	FT	50		141				
19. T _c = L / 3600 V	HR	0.0021]+[0.0070	+		=	
20. Cummulative Tc in Hours (Sum of Step	os 6, 11, & 19)			-	НГ	₹	

0.0091 0.1310

Tc in MINUTES =



PROJECT: 222 Church Road [2154-10]

LOCATION: Cheltenham Township

COUNTY: Montgomery County, PA

TR-55 Method - Time of Concentration (Tc) Calculations POINT OF DISCHARGE #1 (POST-DEVELOPMENT)

Sheet Flow	Segment ID	AB	ΤГ		ا ٦		1	
<u> </u>	oogoneb	Range	┪┢		1			
1. Surface Description (table 3-1)		(natural)						
2. Manning's roughness coefficient., n (tal		0.130	┪┢		1			
3. Flow length, L	· ·	75			1			
4. Two-yr 24-hr rainfall, P ₂	H	3.30			11			
5. Land slope, s	l-	0.1330			11			
6. $T_c = 0.007(nL)^{0.8} / P_2^{0.5} s^{0.4}$ (Eq. 3-3)	L	0.0534	┪╻┝		+		1-[0.0534
	L							
Shallow Concentrated Flow	Segment ID	ВС	7 [CD	7 [DE		
7. Surface Description (paved or unpaved)	Unpaved		Paved		Unpaved		
8. Flow length, L	FT	69		119		326		
9. Watercourse slope, s	FT/FT	0.1300		0.0750		0.0537		
10. Average velocity, V (figure 3-1)	FT/Sec	5.84		5.60		3.74		
11. T _c = L / 3600V	HR	0.0033	7 + [0.0059	+	0.0242] = [0.0334
							_	
	-				_ ,		7	
Channel Flow	Segment ID							
12. Cross sectional flow area, a	FT ²							
13. Wetted perimeter, p _W	FT							
14. Hydraulic radius, r = a/p _W	FT							
15. Channel Slope, s	FT/FT							
16. Manning's roughness coefficient								
17. V=1.49r ^{2/3} s ^{1/2} / n	FT/Sec							
18. Flow length, L	FT							
19. T _c = L / 3600 V	HR		7+[+] = [
20. Cummulative Tc in Hours (Sum of S	Steps 6, 11, & 19)					Н	R	0.0868
						c in MINUTES		5.2



PROJECT: 222 Church Road [2154-10]

LOCATION: Cheltenham Township

COUNTY: Montgomery County, PA

TR-55 Method - Time of Concentration (Tc) Calculations POINT OF DISCHARGE #2 (POST-DEVELOPMENT)

Sheet Flow Seg	ment ID	AB								
		Range								
1. Surface Description (table 3-1)		(natural)								
2. Manning's roughness coefficient., n (table 3-	1)	0.130								
3. Flow length, L	FT	98								
4. Two-yr 24-hr rainfall, P ₂	IN	3.30								
5. Land slope, s	FT/FT	0.0950								
6. T _c =0.007(nL) ^{0.8} /P ₂ ^{0.5} s ^{0.4} (Eq. 3-3)	HR	0.0757	+		+] = [0.0757	1	
	•				_		-			
			_		_		,		7	
Shallow Concentrated Flow Seg	ment ID	BC		CD		DE		EF		
7. Surface Description (paved or unpaved)		Paved		Unpaved		Paved		Unpaved		
8. Flow length, L	FT	12		346		73		107		
9. Watercourse slope, s	FT/FT	0.0200		0.0660		0.0220		0.1120		
10. Average velocity, V (figure 3-1)	FT/Sec	2.90		4.15		3.04		5.42		
11. T _c = L / 3600V	HR	0.0012	+	0.0232	+	0.0067	+	0.0055]=[0.0298
	_		_							
Ohanna I Flans			7		1		1			
	ment ID				1		ł			
12. Cross sectional flow area, a	ŀ		-		-		1			
13. Wetted perimeter, p _W	H				-		-			
14. Hydraulic radius, r = a/p _W			4		-		_			
15. Channel Slope, s	-		-				-			
16. Manning's roughness coefficient			4		-					
17. V=1.49r ^{2/3} s ^{1/2} / n			1				1			
18. Flow length, L	L		1				⇃,		_	
19. T _c = L / 3600 V	L		+		+] = [
20. Cummulative Tc in Hours (Sum of Steps	6, 11, & 19))				HI	₹	0.1055		
					•	C in MINUTES	S =	6.3		



PROJECT: 222 Church Road [2154-10]
LOCATION: Cheltenham Township
COUNTY: Montgomery County, PA

Runoff Peak Rate Summary

Hydrograph ID			Return Pe	riod / Peak	Rate (CFS)		
nyurograpirio	1 Yr	2 Yr	5 Yr	10 Yr	25 Yr	50 Yr	100 Yr
Pre-Development - POD #1							
PRE-DEV TO POD #1 (ON-SITE)	2.57	3.08	3.62	4.00	4.44	4.74	5.02
Post-Development - POD #1							
POST-DEV INFLOW TO BMP001 (ON-SITE)	5.55	6.65	7.82	8.64	9.59	10.25	10.85
BMP001 ROUTING (ON-SITE)	0.00	0.08	0.68	1.11	1.60	1.94	2.27
POST-DEV BYPASS TO POD #1 (ON-SITE)	0.84	1.00	1.17	1.29	1.43	1.53	1.62
Post-Dev to POD #1 - On-Site Total	0.04	4.00	4.05	2.40	2.02	2.47	2.00
(Subject to Twp Peak Rate Requirements)	0.84	1.08	1.85	2.40	3.03	3.47	3.89
Allowable Peak Rate*	2.57	2.57	3.08	3.62	4.00	4.44	5.02
Difference (Prop Allow.)	-1.73	-1.49	-1.23	-1.22	-0.97	-0.97	-1.13
<u>Pre-Development - POD #2</u> PRE-DEV TO POD #2 (ON-SITE)	1.34	1.60	1.87	2.07	2.29	2.44	2.59
Post-Development - POD #2 POST-DEV BYPASS TO POD #2 (ON-SITE) (Subject to Twp Peak Rate Requirements)	0.80	0.95	1.12	1.23	1.37	1.46	1.55
Allowable Peak Rate*	1.34	1.34	1.60	1.87	2.07	2.29	2.59
Difference (Prop Allow.)	-0.54	-0.39	-0.48	-0.64	-0.70	-0.83	-1.04

Hudrograph ID			Return Pe	riod / Peak	Rate (CFS)		
Hydrograph ID	1 Yr	2 Yr	5 Yr	10 Yr	25 Yr	50 Yr	100 Yr
OVERALL TOTAL TO POD #1							
Overall Pre-Dev POD #1	5.96	7.15	8.40	9.28	10.30	11.01	11.66
Overall Post-Dev POD #1	3.34	4.67	6.15	7.28	8.76	9.90	10.87
Difference (Post-Dev - Pre-Dev)	-2.62	-2.48	-2.25	-2.00	-1.54	-1.11	-0.79
OVERALL TOTAL TO POD #2							
Overall Pre-Dev POD #2	4.23	5.06	5.92	6.53	7.25	7.73	8.19
Overall Post-Dev POD #2	2.62	3.14	3.67	4.05	4.49	4.80	5.08
Difference (Post-Dev - Pre-Dev)	-1.61	-1.92	-2.25	-2.48	-2.76	-2.93	-3.11
Overall Watershed							
Overall Total Pre-Dev Peak Rate	10.19	12.21	14.32	15.81	17.55	18.74	19.85
Overall Total Post-Dev Peak Rate	5.96	7.81	9.82	11.33	13.25	14.70	15.95
Difference (Post-Dev - Pre-Dev)	-4.23	-4.40	-4.50	-4.48	-4.30	-4.04	-3.90

 $^{{\}it * Per Cheltenham Township Stormwater Management Ordinance Section 290-23, District 'B'.}$

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	Dekalb	2.565	1	40	3,682				PRE-DEV POD #1 (ON-SITE)
2	Dekalb	3.394	1	40	4,872				PRE-DEV POD #1 (OFF-SITE)
3	Combine	5.960	1	40	8,553	1, 2			PRE-DEV TOTAL TO POD #1
5	Dekalb	1.337	1	30	1,439				PRE-DEV POD #2 (ON-SITE)
6	Dekalb	2.893	1	30	3,114				PRE-DEV POD #2 (OFF-SITE)
7	Combine	4.230	1	30	4,554	5, 6			PRE-DEV TOTAL TO POD #2
9	Dekalb	5.546	1	40	7,959				POST-DEV TO BMP001 (ON-SITE)
10	Dekalb	3.217	1	40	4,616				POST-DEV TO BMP001 (OFF-SITE)
11	Combine	8.762	1	40	12,576	9, 10			POST-DEV TOTAL TO BMP001
12	Reservoir	0.000	1	n/a	0	9	133.71	7,959	BMP001 ROUTE (ON-SITE)
13	Reservoir	1.172	1	70	3,300	11	134.34	11,198	BMP001 ROUTE (OVERALL)
14	Dekalb	0.839	1	25	753				POST-DEV BYPASS TO POD #1 (O
15	Dekalb	1.329	1	25	1,192				POST-DEV BYPASS TO POD #1 (O
17	Dekalb	0.798	1	30	859				POST-DEV BYPASS TO POD #2 (O
18	Dekalb	1.825	1	30	1,965				POST-DEV BYPASS TO POD #2 (O
19	Combine	2.623	1	30	2,824	17, 18			POST-DEV TOTAL TO POD #2
215	4-10 Hydraflo	ow.gpw			Return I	Period: 1 Ye		Wednesda	y, 09 / 13 / 2023

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

						Hydraf 	low Hydrograph 	ns Extension for A	utodesk® Civil 3D® by Autodesk, Inc. v2
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	Dekalb	3.078	1	40	4,417				PRE-DEV POD #1 (ON-SITE)
2	Dekalb	4.072	1	40	5,845				PRE-DEV POD #1 (OFF-SITE)
3	Combine	7.150	1	40	10,262	1, 2			PRE-DEV TOTAL TO POD #1
5	Dekalb	1.599	1	30	1,721				PRE-DEV POD #2 (ON-SITE)
6	Dekalb	3.460	1	30	3,724				PRE-DEV POD #2 (OFF-SITE)
7	Combine	5.059	1	30	5,445	5, 6			PRE-DEV TOTAL TO POD #2
9	Dekalb	6.654	1	40	9,549				POST-DEV TO BMP001 (ON-SITE)
10	Dekalb	3.859	1	40	5,539				POST-DEV TO BMP001 (OFF-SITE)
11	Combine	10.51	1	40	15,088	9, 10			POST-DEV TOTAL TO BMP001
12	Reservoir	0.080	1	79	273	9	134.04	9,519	BMP001 ROUTE (ON-SITE)
13	Reservoir	2.082	1	63	5,812	11	134.50	12,109	BMP001 ROUTE (OVERALL)
14	Dekalb	1.002	1	25	899				POST-DEV BYPASS TO POD #1 (O
15	Dekalb	1.586	1	25	1,422				POST-DEV BYPASS TO POD #1 (O
17	Dekalb	0.954	1	30	1,027				POST-DEV BYPASS TO POD #2 (O
18	Dekalb	2.183	1	30	2,349				POST-DEV BYPASS TO POD #2 (O
19	Combine	3.137	1	30	3,377	17, 18			POST-DEV TOTAL TO POD #2
215	i4-10 Hydraflo	ow.gpw			Return F	Period: 2 Ye	ear	Wednesda	y, 09 / 13 / 2023

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

		•				Hydraf	low Hydrograph	ns Extension for A	utodesk® Civil 3D® by Autodesk, Inc. v2
lyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	Dekalb	3.615	1	40	5,188				PRE-DEV POD #1 (ON-SITE)
2	Dekalb	4.783	1	40	6,865				PRE-DEV POD #1 (OFF-SITE)
3	Combine	8.398	1	40	12,053	1, 2			PRE-DEV TOTAL TO POD #1
5	Dekalb	1.872	1	30	2,015				PRE-DEV POD #2 (ON-SITE)
6	Dekalb	4.051	1	30	4,361				PRE-DEV POD #2 (OFF-SITE)
7	Combine	5.923	1	30	6,376	5, 6			PRE-DEV TOTAL TO POD #2
9	Dekalb	7.815	1	40	11,216				POST-DEV TO BMP001 (ON-SITE)
10	Dekalb	4.533	1	40	6,505				POST-DEV TO BMP001 (OFF-SITE)
11	Combine	12.35	1	40	17,721	9, 10			POST-DEV TOTAL TO BMP001
12	Reservoir	0.678	1	74	1,940	9	134.24	10,602	BMP001 ROUTE (ON-SITE)
13	Reservoir	3.128	1	58	8,445	11	134.66	12,989	BMP001 ROUTE (OVERALL)
14	Dekalb	1.171	1	25	1,051				POST-DEV BYPASS TO POD #1 (O
15	Dekalb	1.853	1	25	1,663				POST-DEV BYPASS TO POD #1 (O
17	Dekalb	1.117	1	30	1,203				POST-DEV BYPASS TO POD #2 (O
18	Dekalb	2.556	1	30	2,751				POST-DEV BYPASS TO POD #2 (O
19	Combine	3.673	1	30	3,954	17, 18			POST-DEV TOTAL TO POD #2
215	54-10 Hydraflo	ow.gpw			Return	Period: 5 Y	ear	Wednesda	ay, 09 / 13 / 2023

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

⊣yd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	Dekalb	3.995	1	40	5,734				PRE-DEV POD #1 (ON-SITE)
2	Dekalb	5.287	1	40	7,588				PRE-DEV POD #1 (OFF-SITE)
3	Combine	9.283	1	40	13,322	1, 2			PRE-DEV TOTAL TO POD #1
5	Dekalb	2.065	1	30	2,223				PRE-DEV POD #2 (ON-SITE)
6	Dekalb	4.469	1	30	4,810				PRE-DEV POD #2 (OFF-SITE)
7	Combine	6.534	1	30	7,033	5, 6			PRE-DEV TOTAL TO POD #2
9	Dekalb	8.638	1	40	12,397				POST-DEV TO BMP001 (ON-SITE)
10	Dekalb	5.010	1	40	7,191				POST-DEV TO BMP001 (OFF-SITE)
11	Combine	13.65	1	40	19,588	9, 10			POST-DEV TOTAL TO BMP001
12	Reservoir	1.109	1	71	3,121	9	134.33	11,128	BMP001 ROUTE (ON-SITE)
13	Reservoir	3.949	1	54	10,312	11	134.77	13,617	BMP001 ROUTE (OVERALL)
14	Dekalb	1.291	1	25	1,158				POST-DEV BYPASS TO POD #1 (O
15	Dekalb	2.043	1	25	1,832				POST-DEV BYPASS TO POD #1 (O
17	Dekalb	1.233	1	30	1,327				POST-DEV BYPASS TO POD #2 (O
18	Dekalb	2.819	1	30	3,035				POST-DEV BYPASS TO POD #2 (O
19	Combine	4.052	1	30	4,361	17, 18			POST-DEV TOTAL TO POD #2
 215	64-10 Hydraflo	ow.gpw			Return I	Period: 10 \	/ear	Wednesda	ıy, 09 / 13 / 2023

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

		<u> </u>				Hydraf	low Hydrograph	is Extension for A	utodesk® Civil 3D® by Autodesk, Inc. v2
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	Dekalb	4.435	1	40	6,365				PRE-DEV POD #1 (ON-SITE)
2	Dekalb	5.869	1	40	8,423				PRE-DEV POD #1 (OFF-SITE)
3	Combine	10.30	1	40	14,788	1, 2			PRE-DEV TOTAL TO POD #1
5	Dekalb	2.290	1	30	2,465				PRE-DEV POD #2 (ON-SITE)
6	Dekalb	4.955	1	30	5,334				PRE-DEV POD #2 (OFF-SITE)
7	Combine	7.245	1	30	7,799	5, 6			PRE-DEV TOTAL TO POD #2
9	Dekalb	9.588	1	40	13,761				POST-DEV TO BMP001 (ON-SITE)
10	Dekalb	5.561	1	40	7,982				POST-DEV TO BMP001 (OFF-SITE)
11	Combine	15.15	1	40	21,743	9, 10			POST-DEV TOTAL TO BMP001
12	Reservoir	1.595	1	67	4,485	9	134.42	11,643	BMP001 ROUTE (ON-SITE)
13	Reservoir	5.070	1	49	12,467	11	134.91	14,407	BMP001 ROUTE (OVERALL)
14	Dekalb	1.431	1	25	1,283				POST-DEV BYPASS TO POD #1 (O
15	Dekalb	2.264	1	25	2,031				POST-DEV BYPASS TO POD #1 (O
17	Dekalb	1.367	1	30	1,471				POST-DEV BYPASS TO POD #2 (O
18	Dekalb	3.126	1	30	3,365				POST-DEV BYPASS TO POD #2 (O
19	Combine	4.493	1	30	4,836	17, 18			POST-DEV TOTAL TO POD #2
215	4-10 Hydraflo	ow.gpw			Return F	Period: 25	/ear	Wednesda	y, 09 / 13 / 2023

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

		<u> </u>				Hydraf	low Hydrograph	is Extension for A	utodesk® Civil 3D® by Autodesk, Inc. v2
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	Dekalb	4.739	1	40	6,802				PRE-DEV POD #1 (ON-SITE)
2	Dekalb	6.271	1	40	9,000				PRE-DEV POD #1 (OFF-SITE)
3	Combine	11.01	1	40	15,802	1, 2			PRE-DEV TOTAL TO POD #1
5	Dekalb	2.444	1	30	2,631				PRE-DEV POD #2 (ON-SITE)
6	Dekalb	5.289	1	30	5,693				PRE-DEV POD #2 (OFF-SITE)
7	Combine	7.733	1	30	8,324	5, 6			PRE-DEV TOTAL TO POD #2
9	Dekalb	10.25	1	40	14,705				POST-DEV TO BMP001 (ON-SITE)
10	Dekalb	5.943	1	40	8,529				POST-DEV TO BMP001 (OFF-SITE)
11	Combine	16.19	1	40	23,234	9, 10			POST-DEV TOTAL TO BMP001
12	Reservoir	1.941	1	64	5,429	9	134.48	11,976	BMP001 ROUTE (ON-SITE)
13	Reservoir	5.947	1	48	13,957	11	135.01	14,996	BMP001 ROUTE (OVERALL)
14	Dekalb	1.526	1	25	1,369				POST-DEV BYPASS TO POD #1 (O
15	Dekalb	2.416	1	25	2,167				POST-DEV BYPASS TO POD #1 (O
17	Dekalb	1.459	1	30	1,570				POST-DEV BYPASS TO POD #2 (O
18	Dekalb	3.337	1	30	3,591				POST-DEV BYPASS TO POD #2 (O
19	Combine	4.795	1	30	5,162	17, 18			POST-DEV TOTAL TO POD #2
215	4-10 Hydraflo	ow.gpw			Return F	Period: 50	/ear	Wednesda	y, 09 / 13 / 2023

Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

		•				Hydraf 	low Hydrograph	s Extension for A	utodesk® Civil 3D® by Autodesk, Inc. v2
Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description
1	Dekalb	5.020	1	40	7,205				PRE-DEV POD #1 (ON-SITE)
2	Dekalb	6.643	1	40	9,534				PRE-DEV POD #1 (OFF-SITE)
3	Combine	11.66	1	40	16,739	1, 2			PRE-DEV TOTAL TO POD #1
5	Dekalb	2.590	1	30	2,788				PRE-DEV POD #2 (ON-SITE)
6	Dekalb	5.604	1	30	6,033				PRE-DEV POD #2 (OFF-SITE)
7	Combine	8.194	1	30	8,820	5, 6			PRE-DEV TOTAL TO POD #2
9	Dekalb	10.85	1	40	15,577				POST-DEV TO BMP001 (ON-SITE)
10	Dekalb	6.295	1	40	9,035				POST-DEV TO BMP001 (OFF-SITE)
11	Combine	17.15	1	40	24,612	9, 10			POST-DEV TOTAL TO BMP001
12	Reservoir	2.273	1	62	6,301	9	134.53	12,275	BMP001 ROUTE (ON-SITE)
13	Reservoir	6.691	1	47	15,336	11	135.10	15,539	BMP001 ROUTE (OVERALL)
14	Dekalb	1.618	1	25	1,451				POST-DEV BYPASS TO POD #1 (O
15	Dekalb	2.561	1	25	2,297				POST-DEV BYPASS TO POD #1 (O
17	Dekalb	1.546	1	30	1,664				POST-DEV BYPASS TO POD #2 (O
18	Dekalb	3.535	1	30	3,806				POST-DEV BYPASS TO POD #2 (O
19	Combine	5.081	1	30	5,469	17, 18			POST-DEV TOTAL TO POD #2
									2011010
215	4-10 Hydraflo	ow.gpw			Return F	Period: 100	Year	Wednesda	y, 09 / 13 / 2023

PROJECT: 222 Church Road [2154-10]
LOCATION: Cheltenham Township
COUNTY: Montgomery County, PA

BMP Storage Volume Calculations

		S	Surface Storage	je je		,	Subsurface Storage	Storage			Volu	Volume Credit		Infiltration De	Infiltration Dewatering Time
			Contour	Incr.	Total	Amended Soil	ed Soil	Stone	ne		Surface Storage	Subsurface	Total Storage	Infiltration	Dewatering
			Area	Storage	Storage	Depth	Void	Depth	Void	W.Q.	@ W.Q. Elev.	Storage	Below W.Q. Elev.	Design Rate	Time ¹
BMP ID	Stage	Elevation	(SF)	(CF)	(CF)	(FT)	Ratio	Ē	Ratio	Elev.	(CF)	(CF)	(CF)	(IN/HR)	(HR)
	0.00	133.00	3,971	0	0										
	1.00	134.00	690'5	4,508	4,508										
	2.00	135.00	6,222	5,635	10,143										
BMP ID 001	2.50	135.50	8/8/9	3,273	13,416	4.00	30%	0.00	40%	134.00	4,508	4,765	9,273	99'0	42.5
	3.00	136.00	7,664	3,633	17,049										
<u> </u>															
<u> </u>															
1															
<u> </u>															
<u> </u>															

NOTES:

Dewatering Time = $\frac{1}{(Infiltration Design Rate/12) * Bottom Contour Area}$ Total Storage Below W. Q. Elev. ¹ Dewatering Time is calculated as:

Pond No. 1 - BMP 001

Pond Data

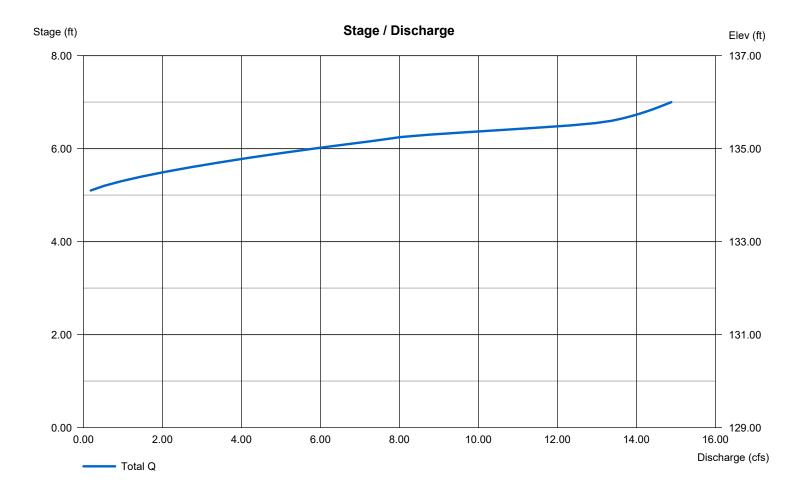
Pond storage is based on user-defined values.

Stage / Storage Table

Stage (ft)	Elevation (ft)	Contour area (sqft)	Incr. Storage (cuft)	Total storage (cuft)
0.00	129.00	n/a	0	0
4.00	133.00	n/a	4,765	4,765
5.00	134.00	n/a	4,508	9,273
6.00	135.00	n/a	5,635	14,908
6.50	135.50	n/a	3,273	18,181
7.00	136.00	n/a	3,633	21,814

Culvert / Orifice Structures Weir Structures [A] [B] [C] [PrfRsr] [A] [B] [C] [D] Rise (in) = 18.000.00 0.00 0.00 Crest Len (ft) = 10.44 1.75 0.00 0.00 Span (in) = 18.00 0.00 0.00 0.00 Crest El. (ft) = 135.25 134.00 0.00 0.00 = 3.33 No. Barrels Weir Coeff. 3.33 3.33 = 1 0 0 3.33 Invert El. (ft) = 132.13 0.00 0.00 0.00 Weir Type = 1 Rect = 26.00 0.00 0.00 0.00 Multi-Stage Yes Length (ft) = Yes No No n/a = 0.500.00 0.00 Slope (%) N-Value = .013 .013 .013 n/a Orifice Coeff. 0.60 0.60 0.60 Exfil.(in/hr) = 0.000 (by Wet area) = 0.60TW Elev. (ft) Multi-Stage = n/aNo No No = 0.00

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



ANTI-SEEP CO	DLLAR D	ESIGN			
Sed Trap		1			
RISER CREST ELEV.	(feet)	135.25			
INVERT OF OUTFLOW PIPE	(feet)	132.13			
DIAMETER OF PIPE / TYPE	(inches)	18 HDPE	RCP	RCP	RCP
LENGTH OF OUTFALL PIPE	(feet)	26			
PIPE SLOPE	(ft/ft)	0.0050			
EMBANKMENT SLOPE (X:1)	(ft/ft)	3			
Number of collars	(each)	2			
Permanent / Temporary		PERMANENT	PERMANENT	PERMANENT	PERMANENT
"Y"	(feet)	3.12			
SATURATED LENGTH, Ls	(feet)	22			
COLLAR PROJECTION, V	(feet)	1.00			
COLLAR SIZE	(feet)	3.50			
COLLAR SPACING	(feet)	7			
MAXIMUM COLLAR SPACING	(feet)	14			



PROJECT: 222 Church Road [2154-10]

LOCATION: Cheltehnam Township
COUNTY: Montgomery County, PA

Emergency Spillway Sizing Calculations For: BMP ID 001

100-Year Storm Inflow (Q): 17.15 CFS (From Post-Development Routing Analysis)

Emergency Spillway Capacity Calculations

Q = CLH^1.5

Weir Coefficient (C): 2.63

Length (L): **25** FT

Flow Depth (H) = 0.41 FT

Freeboard & Velocity Calculations

Elevation of Spillway: 135.50

Top of Berm Elevation: 136.50

Elevation of Flow (Based

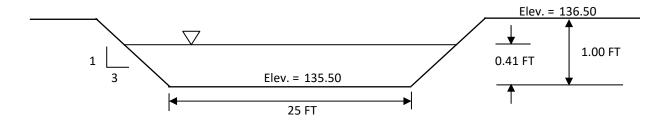
on Depth Calculated Above): 135.91

Provided Freeboard = 0.59 FT

Spillway Opening Side Slope (H:V): 3:1

Flow Area (A) = **10.71** SF

Flow Velocity (V) = $Q / A = \begin{bmatrix} 1.60 \\ FT/SEC \end{bmatrix}$





PROJECT: 222 Curch Road [2154-10]
LOCATION: Cheltenham Township
COUNTY: Montgomery County, PA

PCSM BMP Loading Ratio Calculations

	Raw Drainage	Raw Drainage Area to BMP	Pre-Trea	Pre-Treatment BMP Tabulation		Resultant (Net) Drainage Area	Drainage Area	BMP	Loadin	Loading Ratio
BMP ID	Overall	Impervious		Overall Area	Impervious Area	Or all area	Impervious	Infiltration		
No.	No. Drainage Area Drainage Area	Drainage Area	BMP Type	Treated	Treated	Overall Area	Area	Area	Overall ¹	Impervious ²
	(SF)	(SF)		(SF)	(SF)	(SF)	(SF)	(SF)		
100	197,327	75,359	Sump & Snout	172,062	67,082	25,265	8,276	3,971	6.4:1	2.1:1

Notes: ¹ Maximum of 8:1 is recommended for the Overall Loading Ratio

² Maximum of 5:1 is recommended for the Impervious Loading Ratio; however, in carbonate geology areas, a maximum of 3:1 is recommended

Project Name: 222 Church Road

03-01-2023

Storm Sewer Tabulation

Stormwater Studio 2023 v 3.0.0.31

a .									1	WS
Line	•		_	7	က	4	2	9		veyance.s
e Elev	Du	(£)	136.00	138.11	141.80	141.80	144.02	135.00		0 SWM Con
Surface Elev	dn	(#)	138.11	141.80	144.02	140.37	146.66	134.75		Project File: 2154-10 SWM Conveyance.sws
ilev	Du	(#)	134.31	135.78	136.37	136.44	137.12	133.50		Projec
HGL Elev	ф	(#)	134.86	136.02	136.49	136.82	139.60	133.53		
Elev	Б	(#)	133.00	133.71	134.76	135.54	135.52	132.00		
Invert Elev	dn	(ft)	133.51	134.26	135.32	135.90	138.97	132.13		
<u>ə</u>	Slope	(%)	92.0	0.75	<u>+</u> + + + + + + + + + + + + + + + + + +	0.51	3.00	0.50		
Line	Size	(in)	24	24	18	24	18	18		
ocity	l϶V	(ft/s)	6.52	4.82	4.18	4.77	2.70	2.72		
scity	Cap	(cfs)	19.72	19.59	11.06	16.15	18.19	8.77		
Q lst	οT	(cfs)	14.50	14.62	6.74	6.61	2.72	4.73		
ytien	əjul	(in/hr)	6.32	6.37	6.40	6.48	6.48	6.48		
ဥ	Syst	(min)	5.57	5.39	5.26	2.00	5.00	0.00		
=	Inlet	(min)	5.0	5.0	5.0	5.0	5.0	0.0		
4	Total		2.30	2.30	1.05	1.02	0.42	0.00		yrs.
C×A	Incr		0.00	0.22	0.63	1.02	0.42	0.00		od = 10-
Isnoi	Rat	(2)	0.00	0.68	0.54	09.0	0.56	0.00		turn Peri
Area	Total	(ac)	3.950	3.950	1.920	1.700	0.750	0.000		s.idf, Ref
Drng Area	Incr	(ac)	0.000	0:330	1.170	1.700	0.750	0.000		itensities
цзби	PΤ	(ft)	67.57	73.04	50.44	70.57	114.99	26.02		NOAA Ir
Line ID			MH2-FES1	INL3-MH2	INL4-INL3	INL6-INL3	INL5-INL4	OS1-LS#1		Notes: IDF File = 2154-10NOAA Intensities.idf, Return Period = 10-yrs.

Project Name: 222 Church Road

03-01-2023

Storm Sewer Tabulation

Stormwater Studio 2023 v 3.0.0.31

4.									WS
Line	•		_	7	က	4	2	9	veyance.s
e Elev	Du	(£)	136.00	138.11	141.80	141.80	144.02	135.00	0 SWM Con
Surface Elev	dn	(#)	138.11	141.80	144.02	140.37	146.66	134.75	Project File: 2154-10 SWM Conveyance.sws
lev	Du	(#)	134.87	135.93	136.62	136.50	137.29	133.50	Projec
HGL Elev	dn	(#)	135.05	136.26	136.88	136.87	139.64	133.55	
Elev	Б	(#)	133.00	133.71	134.76	135.54	135.52	132.00	
Invert Elev	dn	(ft)	133.51	134.26	135.32	135.90	138.97	132.13	
<u>ə</u>	Slope	(%)	92.0	0.75	<u>+</u> + + + + + + + + + + + + + + + + + +	0.51	3.00	0.50	
Line	Size	(in)	24	24	18	24	18	18	
ocity	Velocity		5.80	5.22	4.27	4.94	2.87	3.36	
scity	Capacity		19.72	19.59	11.06	16.15	18.19	8.77	
D lat	D lefal Q		16.26	16.39	7.55	7.41	3.05	5.87	
ytien	Intensity		7.08	7.14	7.18	7.26	7.26	7.26	
ဥ	Syst	(min)	5.55	5.38	5.25	5.00	5.00	00.00	
=	Inlet	(min)	5.0	5.0	5.0	5.0	5.0	0.0	
C×A	Total		2.30	2.30	1.05	1.02	0.42	0.00	yrs.
ပ်	Incr		0.00	0.22	0.63	1.02	0.42	0.00	iod = 25
lsnoi	Rat	(C)	0.00	0.68	0.54	09.0	0.56	0.00	turn Per
Drng Area	Total	(ac)	3.950	3.950	1.920	1.700	0.750	0.000	s.idf, Re
Drng	Incr	(ac)	0.000	0.330	1.170	1.700	0.750	0.000	ntensitie
цзби	ү збиә¬		67.57	73.04	50.44	70.57	114.99	26.02	NOAA Ir
Line ID			MH2-FES1	INL3-MH2	INL4-INL3	INL6-INL3	INL5-INL4	OS1-LS#1	Notes: IDF File = 2154-10NOAA Intensities.idf, Return Period = 25-yrs.

Project Name: 222 Church Road

03-01-2023

Storm Sewer Tabulation

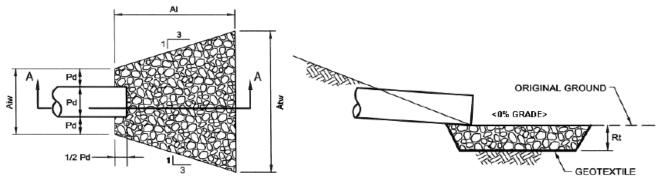
Stormwater Studio 2023 v 3.0.0.31

									6
Line			1	2	က	4	2	9	eyance.sw
Elev	Dn	(ft)	136.00	138.11	141.80	141.80	144.02	135.00	SWM Conv
Surface Elev	dn	(#)	138.11	141.80	144.02	140.37	146.66	134.75	Project File: 2154-10 SWM Conveyance.sws
ilev	П	(#)	135.06	135.96	136.95	137.05	137.83	133.50	Project
HGL Elev	dn	(#)	135.51	136.47	137.29	137.11	139.69	133.58	
Elev	n O	(#)	133.00	133.71	134.76	135.54	135.52	132.00	
Invert Elev	dn	(#)	133.51	134.26	135.32	135.90	138.97	132.13	
<u> </u>	Slope	(%)	92.0	0.75	1.7	0.51	3.00	0.50	
Line	Size	(in)	24	24	18	24	18	18	
ocity	Velocity		5.96	6.01	4.92	3.82	3.11	4.13	
scity	Capacity		19.72	19.59	11.06	16.15	18.19	8.77	
D lat	οT	(cfs)	18.72	18.88	8.70	8.53	3.51	7.25	
nsity	Intensity		8.15	8.22	8.27	8.37	8.37	8.37	
ی	Syst	(min)	5.53	5.36	5.24	5.00	5.00	0.00	
F	Inlet	(min)	5.0	5.0	5.0	2.0	5.0	0.0	
C×A	Total		2.30	2.30	1.05	1.02	0.42	00.00	0-yrs.
Ú	Incr		00'0	0.22	0.63	1.02	0.42	00.00	riod = 10
lsnoi	Rat	(C)	00.00	0.68	0.54	09:0	0.56	00.00	turn Per
Drng Area	Total	(ac)	3.950	3.950	1.920	1.700	0.750	0.000	s.idf, Re
Drng	Incr	(ac)	0.000	0.330	1.170	1.700	0.750	0.000	ntensitie
գյճս	Гепдін		67.57	73.04	50.44	70.57	114.99	26.02	NOAA
Line ID			MH2-FES1	INL3-MH2	INL4-INL3	INL6-INL3	INL5-INL4	OS1-LS#1	Notes: IDF File = 2154-10NOAA Intensities.idf, Return Period = 100-yrs.



PROJECT: 222 Church Road [2154-10]
LOCATION: Cheltenham Township
COUNTY: Montgomery County, PA

RIPRAP APRON SUMMARY CHART



PLAN VIEW

SECTION A - A

		RIP	RAP	APRON			
OUTLET NO.	PIPE DIA Pd (IN)	SIZE (R)	THICKNESS Rt (IN)	LENGTH Al (FT)	INITIAL WIDTH Aiw (FT)	TERMINAL WIDTH Atw (FT)	
FES#1	24	R-4	18.0	22.0	6.0	14.8	



PROJECT: 222 Church Road [2154-10] LOCATION: **Cheltenham Township**

COUNTY: **Montgomery County, PA**

RIPRAP APRON SIZING CALCULATIONS

FOR: FES#1

Design Inputs Full Flow/Equivalency Calcs, Slopes < 0.05 FT/FT

 $Q_f = \frac{0.464}{n} * D^{8/3} * S^{1/2}$ Qf = 21.40 CFS Pipe Material: **HDPE** 0.012 Manning's n:

Pipe Diameter, D: 24 IN

Pipe Slope, S: 0.0076 FT/FT Discharge Ratio = $\frac{d}{D} = \frac{Q_d}{Q_f}$ Design Discharge, Qd: 14.50 **CFS**

Design Velocity, V: 6.52 **FPS** Discharge Ratio =

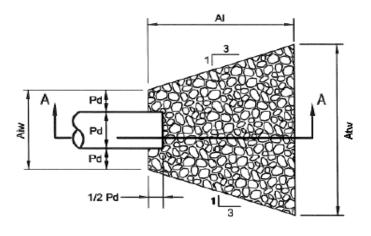
Pipe Inv. Elev. @ Discharge: 133.00

> Tailwater Elevation: % Full = 134.79 0.63

Tailwater Condition, Tw: Area * Ratio = MAX 1.98 SF Full Flow Area of Pipe, A: Equiv. Full-Flow Pipe Size = 3.14 **SF** 18 IN

> **RIPRAP APRON SIZE** R-SIZE = **R-4** INITIAL WIDTH, Aiw = 6.0 FT d50 =6.0 IN **TERMINAL WIDTH, Atw =** 14.8 FT LENGTH, La* = Rt = 18.0 IN 22.0 FT

> > * PER FIGURE 9.4 OF THE E&S MANUAL



PLAN VIEW



PROJECT: 222 Church Road [2154-10]

LOCATION: Cheltenham Township

COUNTY: Montgomery County, PA

Level Spreader Calculations Level Spreader #1

$$V = 1.5 * Cw * H^{1/2}$$

 $H = (V / 1.5 * Cw)^{2}$

Cw =

H =

H* =

Down Slope Ground Cover Conditions	
Grass/Thicket	

- Max Allowable Velocity
- Weir Coefficient (Rectangular Weir)
- Driving Head
- Flow Depth over Level Spreader

Weir Equation

1.33 FT/SEC

3.0

0.09 FT

0.70 IN

$$Q_{100} = Cw * L * H^{3/2}$$

$$L = Q_{100} / Cw * H^{3/2}$$

Q100 =	6.69 FT ³ /SEC
Cw =	3.0
H =	0.087 FT
L=	86 FT

- 100-yr Storm Flow (From Routing Calculations)
- Weir Coefficient
- Driving Head (Calculated Above) Minimum Length of Level Spreader

Underdrain Capacity Calculations

$$Q = C_d A (2gh)^{1/2}$$

$$\Delta - \pi r^2$$

A - 10						
Cd =	0.6					

- Orifice Coefficient

P =	2
r =	0.5 IN
A =	0.011 SF
Δ =	1 57 IN ²

- # of Perferations per Linear Foot
- Radius of Perforation Orifice
- Area of Orifice (SF)
- Area of Orifice (SQ.IN.)

g =	32.2 FT/SEC ²
h =	0.5 FT
Q =	0.037 CFS
Q =	16.67 GPM

Gravitational Constant

- Head
- Orifice Flow (CFS)
- Orifice Flow (GPM)

PennDOT Pub 408 Section 610.2(a)1.c Perforations - Area per Linear Foot

1.57 IN²/LF Provided

>

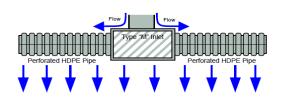
1.4 IN²/LF Requirement

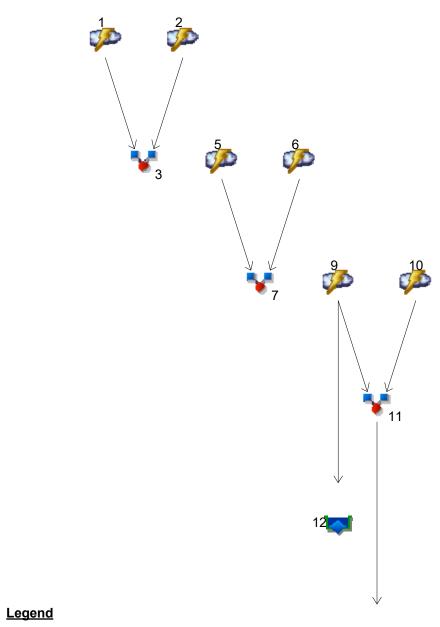
PADEP Design Standard

16.67 GPM/LF Provided

Plan View
NTS

10 GPM/LF Requirement





Hyd.	<u>Origin</u>	<u>Description</u>	13	14	15 3	17	18
1	Dekalb	PRE-DEV POD #1 (ON-SITE)		-	-	-	-
2	Dekalb	PRE-DEV POD #1 (OFF-SITE)				\	/
3	Combine	PRE-DEV TOTAL TO POD #1				\	
5	Dekalb	PRE-DEV POD #2 (ON-SITE)				\	
6	Dekalb	PRE-DEV POD #2 (OFF-SITE)				\	/
7	Combine	PRE-DEV TOTAL TO POD #2				\	/
9	Dekalb	POST-DEV TO BMP001 (ON-SITE)				\searrow	V
10	Dekalb	POST-DEV TO BMP001 (OFF-SITE)				i i	•
11	Combine	POST-DEV TOTAL TO BMP001				•	¹ 19
12	Reservoir	BMP001 ROUTE (ON-SITE)					
13	Reservoir	BMP001 ROUTE (OVERALL)					
14	Dekalb	POST-DEV BYPASS TO POD #1 (ON-SITE)					
15	Dekalb	POST-DEV BYPASS TO POD #1 (OFF-SITE)					
17	Dekalb	POST-DEV BYPASS TO POD #2 (ON-SITE)					
18	Dekalb	POST-DEV BYPASS TO POD #2 (OFF-SITE)					
19	Combine	POST-DEV TOTAL TO POD #2					

Project: 2154-10 Hydraflow.gpw

Wednesday, 09 / 13 / 2023

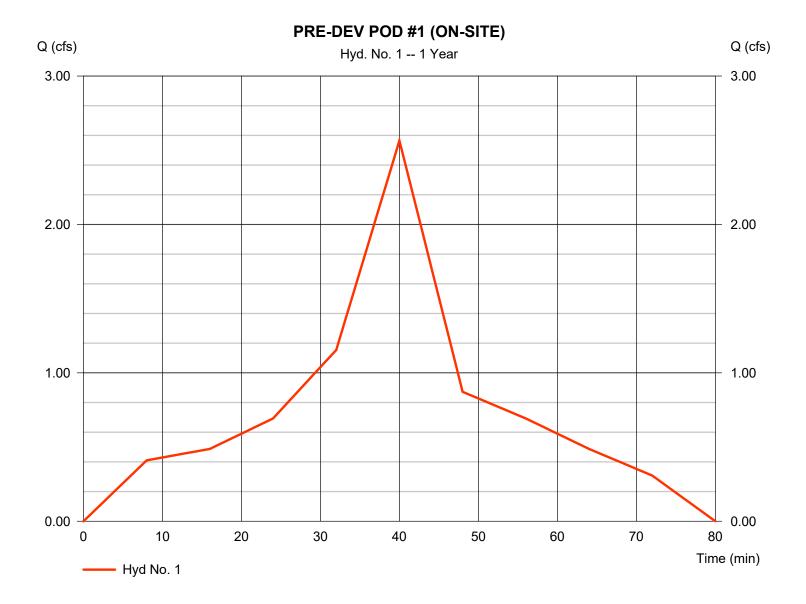
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 1

PRE-DEV POD #1 (ON-SITE)

= 2.565 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 1 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 3,682 cuft Runoff coeff. Drainage area = 2.350 ac= 0.31Tc by User $= 8.00 \, \text{min}$ Intensity = 3.521 in/hrIDF Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



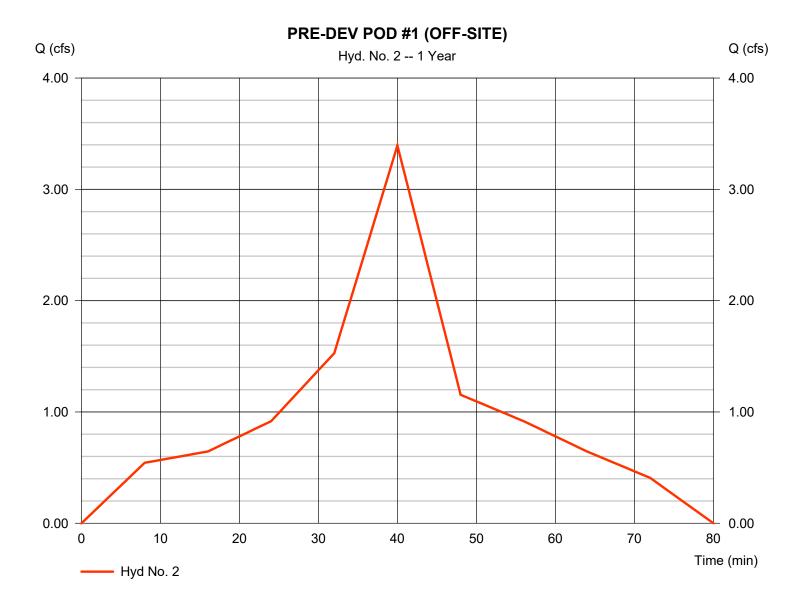
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 2

PRE-DEV POD #1 (OFF-SITE)

= 3.394 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 1 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 4,872 cuftRunoff coeff. Drainage area = 2.410 ac= 0.4Tc by User Intensity = 3.521 in/hr $= 8.00 \, \text{min}$ IDF Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



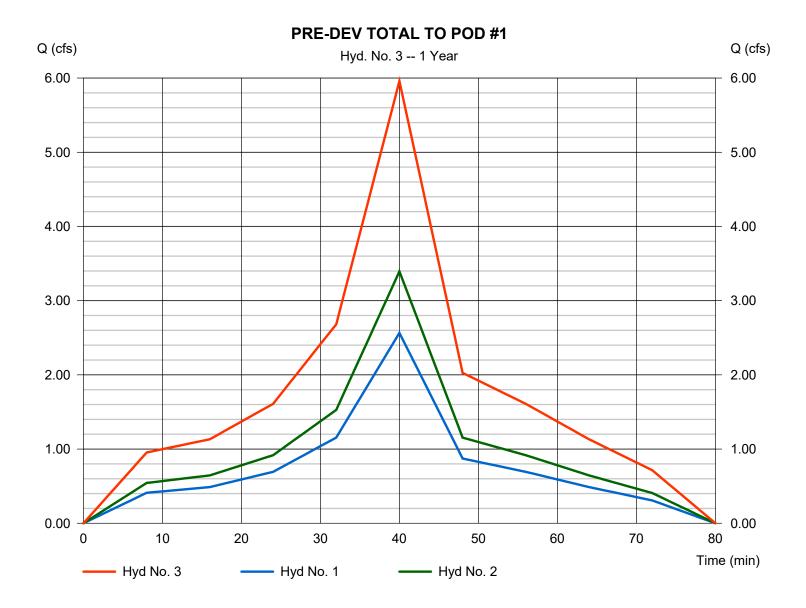
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 3

PRE-DEV TOTAL TO POD #1

Hydrograph type = 5.960 cfs= Combine Peak discharge Time to peak Storm frequency = 1 yrs= 40 min Time interval = 1 min Hyd. volume = 8,553 cuft Inflow hyds. = 1, 2 Contrib. drain. area = 4.760 ac



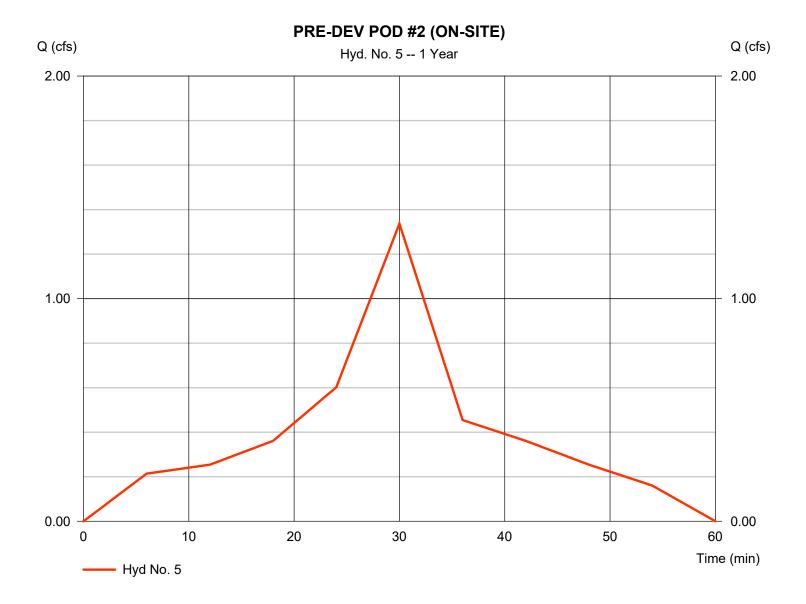
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 5

PRE-DEV POD #2 (ON-SITE)

= 1.337 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 1 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 1,439 cuftRunoff coeff. Drainage area = 1.050 ac= 0.33Tc by User $= 6.00 \, \text{min}$ Intensity = 3.859 in/hr**IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



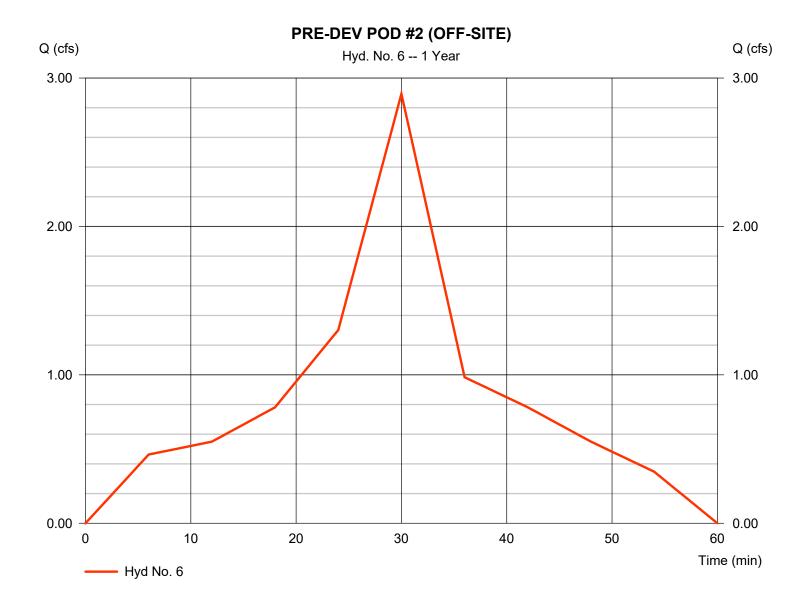
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 6

PRE-DEV POD #2 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 2.893 cfsStorm frequency = 1 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 3,114 cuftRunoff coeff. Drainage area = 1.630 ac= 0.46Tc by User Intensity = 3.859 in/hr $= 6.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



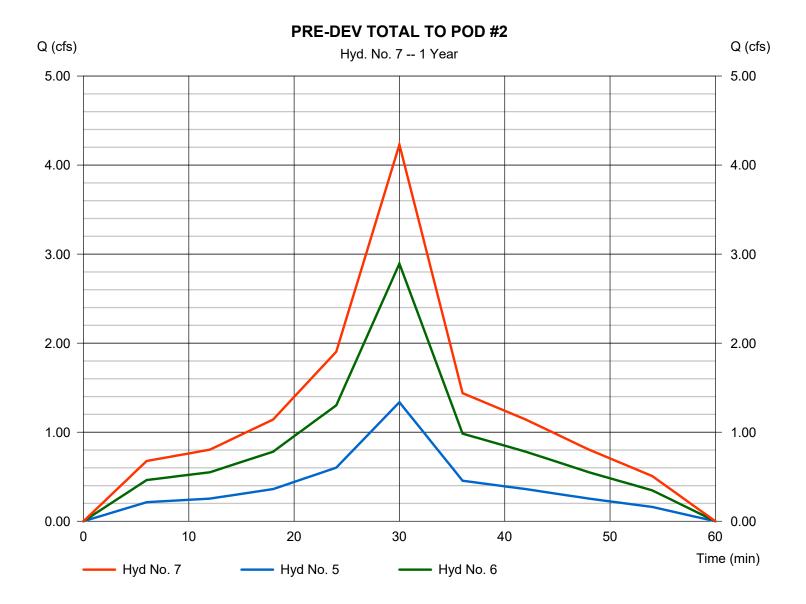
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 7

PRE-DEV TOTAL TO POD #2

Hydrograph type Peak discharge = 4.230 cfs= Combine Time to peak Storm frequency = 1 yrs= 30 min Time interval = 1 min Hyd. volume = 4,554 cuft Inflow hyds. Contrib. drain. area = 2.680 ac= 5, 6



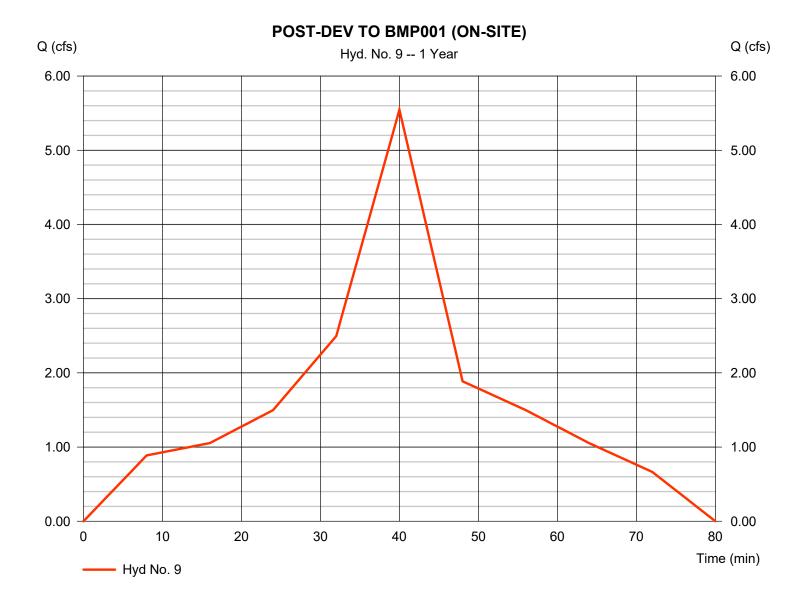
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 9

POST-DEV TO BMP001 (ON-SITE)

Hydrograph type = Dekalb Peak discharge = 5.546 cfsStorm frequency Time to peak = 40 min = 1 yrsTime interval = 1 min Hyd. volume = 7,959 cuftRunoff coeff. Drainage area = 2.500 ac= 0.63Tc by User $= 8.00 \, \text{min}$ Intensity = 3.521 in/hr**IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



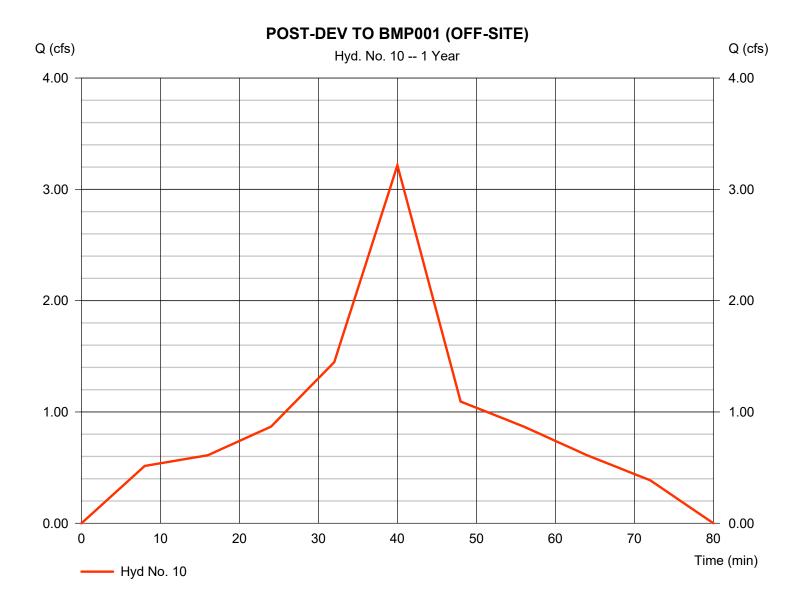
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 10

POST-DEV TO BMP001 (OFF-SITE)

= 3.217 cfsHydrograph type = Dekalb Peak discharge Storm frequency Time to peak = 40 min = 1 yrsTime interval = 1 min Hyd. volume = 4,616 cuftRunoff coeff. Drainage area = 2.030 ac= 0.45Tc by User Intensity = 3.521 in/hr $= 8.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



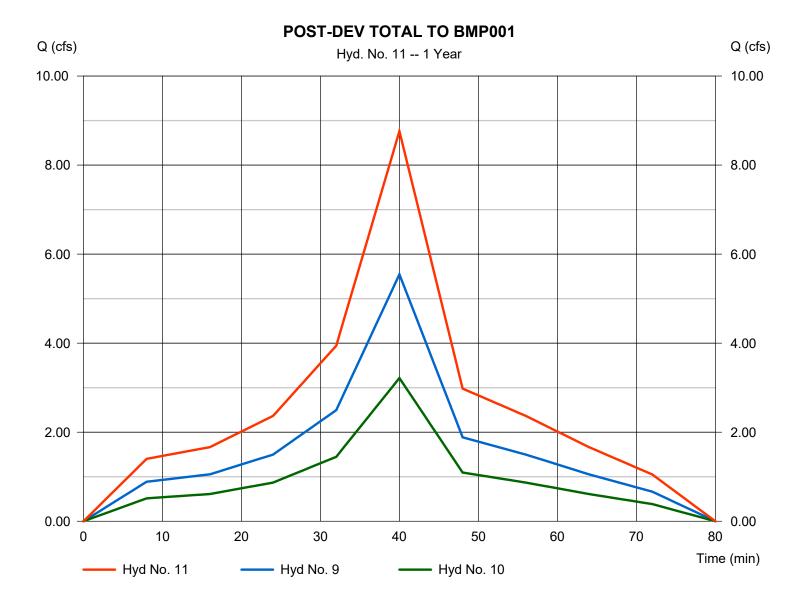
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 11

POST-DEV TOTAL TO BMP001

Hydrograph type Peak discharge = 8.762 cfs= Combine Time to peak Storm frequency = 1 yrs= 40 min Time interval = 1 min Hyd. volume = 12,576 cuft Inflow hyds. = 9, 10 Contrib. drain. area = 4.530 ac



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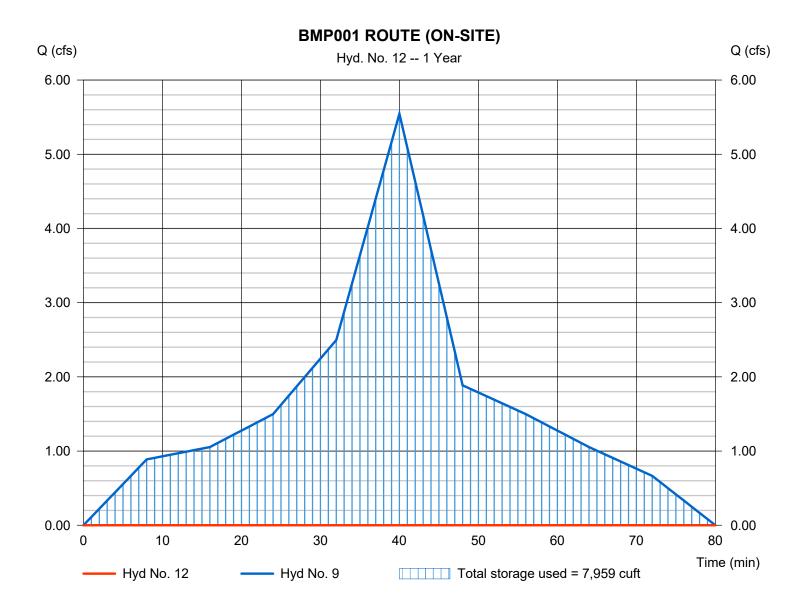
Wednesday, 09 / 13 / 2023

Hyd. No. 12

BMP001 ROUTE (ON-SITE)

Hydrograph type = Reservoir Peak discharge = 0.000 cfsStorm frequency Time to peak = n/a= 1 yrsTime interval = 1 min Hyd. volume = 0 cuft Inflow hyd. No. = 9 - POST-DEV TO BMP001 (OMas) Temp vation $= 133.71 \, \text{ft}$ Reservoir name = BMP 001 Max. Storage = 7,959 cuft

Storage Indication method used.



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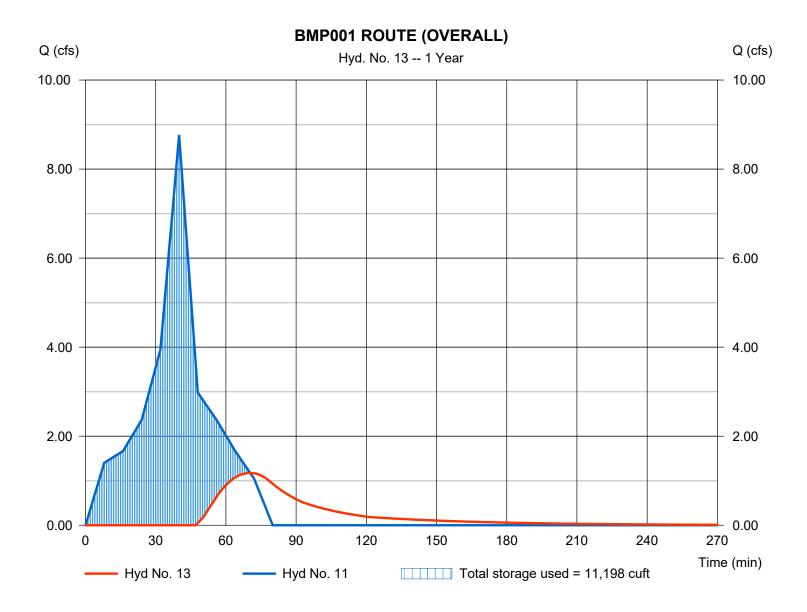
Wednesday, 09 / 13 / 2023

Hyd. No. 13

BMP001 ROUTE (OVERALL)

Hydrograph type = Reservoir Peak discharge = 1.172 cfsStorm frequency Time to peak = 70 min = 1 yrsTime interval = 1 min Hyd. volume = 3,300 cuft= 11 - POST-DEV TOTAL TO BNWP2001 Elevation Inflow hyd. No. = 134.34 ftReservoir name = BMP 001 Max. Storage = 11,198 cuft

Storage Indication method used.



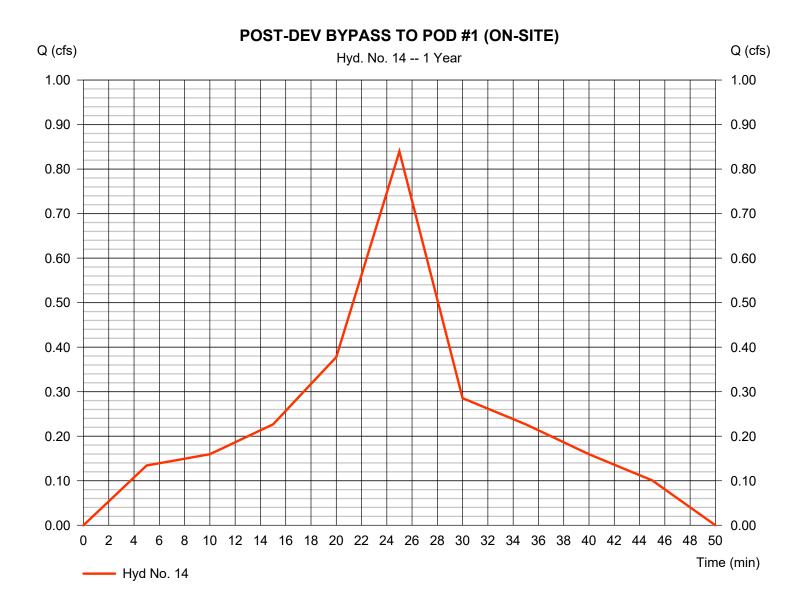
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Wednesday, 09 / 13 / 2023

Hyd. No. 14

POST-DEV BYPASS TO POD #1 (ON-SITE)

Hydrograph type = Dekalb Peak discharge = 0.839 cfsStorm frequency Time to peak = 25 min = 1 yrsTime interval = 1 min Hyd. volume = 753 cuft Runoff coeff. Drainage area = 0.460 ac= 0.45Tc by User Intensity $= 5.00 \, \text{min}$ = 4.055 in/hrIDF Curve = 2154-10_NOAA Intensities_HyAlsan/Revol Diffi b fact = n/a



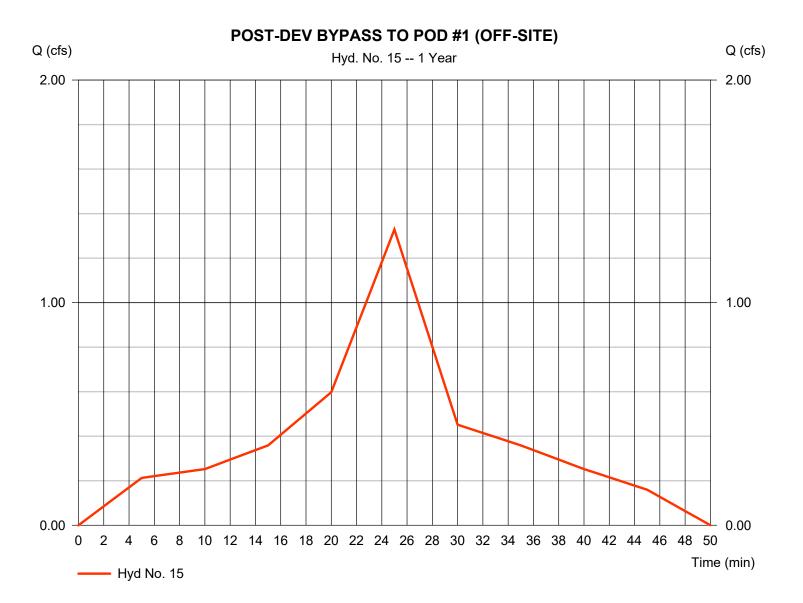
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Wednesday, 09 / 13 / 2023

Hyd. No. 15

POST-DEV BYPASS TO POD #1 (OFF-SITE)

= 1.329 cfsHydrograph type = Dekalb Peak discharge Storm frequency Time to peak = 25 min = 1 yrsTime interval = 1 min Hyd. volume = 1,192 cuft Runoff coeff. = 0.36Drainage area = 0.910 acTc by User $= 5.00 \, \text{min}$ Intensity = 4.055 in/hrIDF Curve = 2154-10_NOAA Intensities_HyAlsat/liRved Dyfn fact = n/a



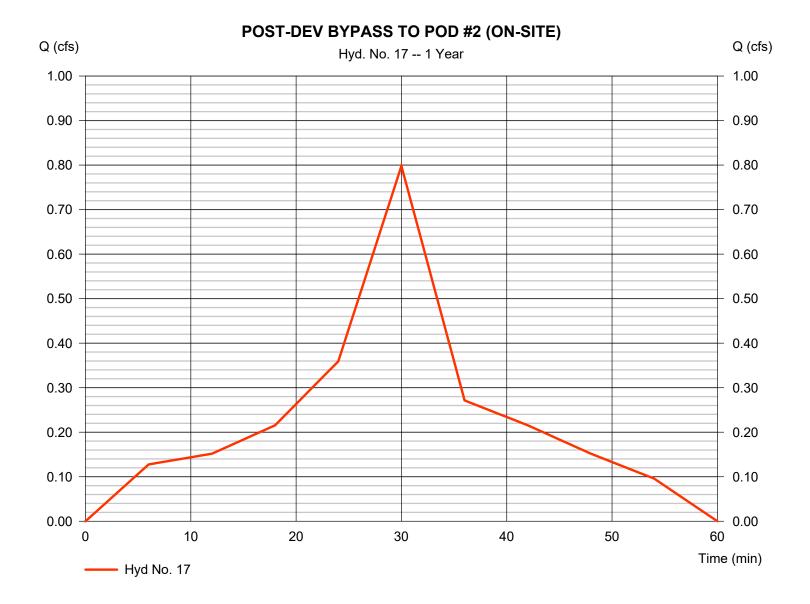
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Wednesday, 09 / 13 / 2023

Hyd. No. 17

POST-DEV BYPASS TO POD #2 (ON-SITE)

Hydrograph type = Dekalb Peak discharge = 0.798 cfsStorm frequency Time to peak = 30 min = 1 yrsTime interval = 1 min Hyd. volume = 859 cuft Runoff coeff. Drainage area = 0.440 ac= 0.47Tc by User Intensity = 3.859 in/hr $= 6.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



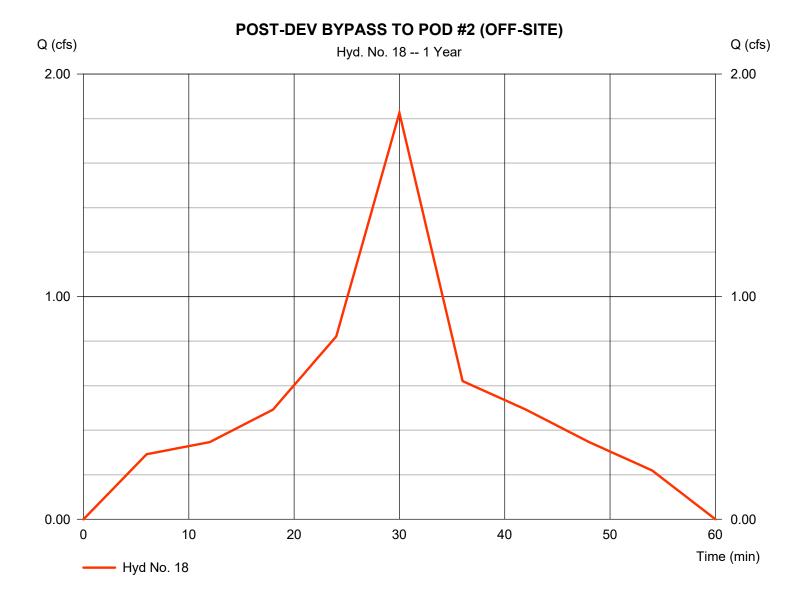
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Wednesday, 09 / 13 / 2023

Hyd. No. 18

POST-DEV BYPASS TO POD #2 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 1.825 cfsStorm frequency Time to peak = 30 min = 1 yrsTime interval = 1 min Hyd. volume = 1,965 cuft Runoff coeff. Drainage area = 1.100 ac= 0.43Tc by User $= 6.00 \, \text{min}$ Intensity = 3.859 in/hr**IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



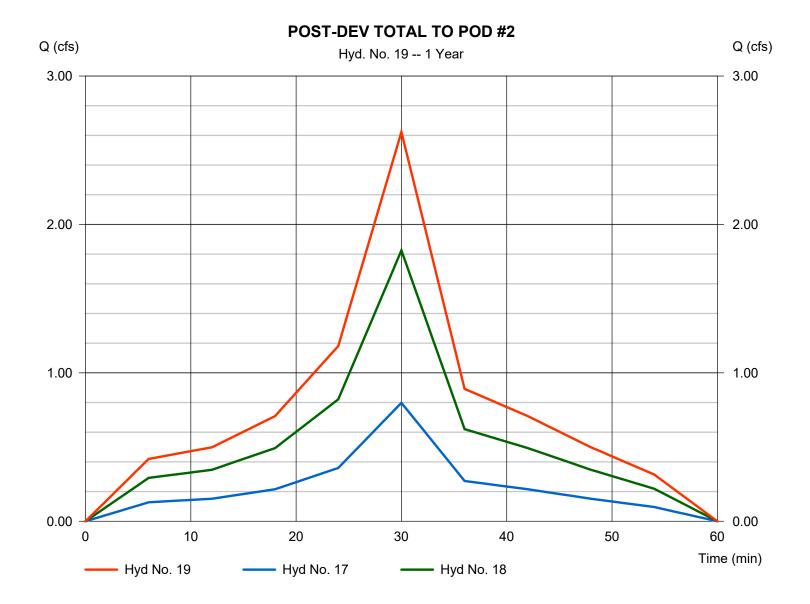
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Wednesday, 09 / 13 / 2023

Hyd. No. 19

POST-DEV TOTAL TO POD #2

Hydrograph type Peak discharge = 2.623 cfs= Combine Time to peak Storm frequency = 1 yrs= 30 min Time interval = 1 min Hyd. volume = 2,824 cuft Inflow hyds. = 17, 18 Contrib. drain. area = 1.540 ac



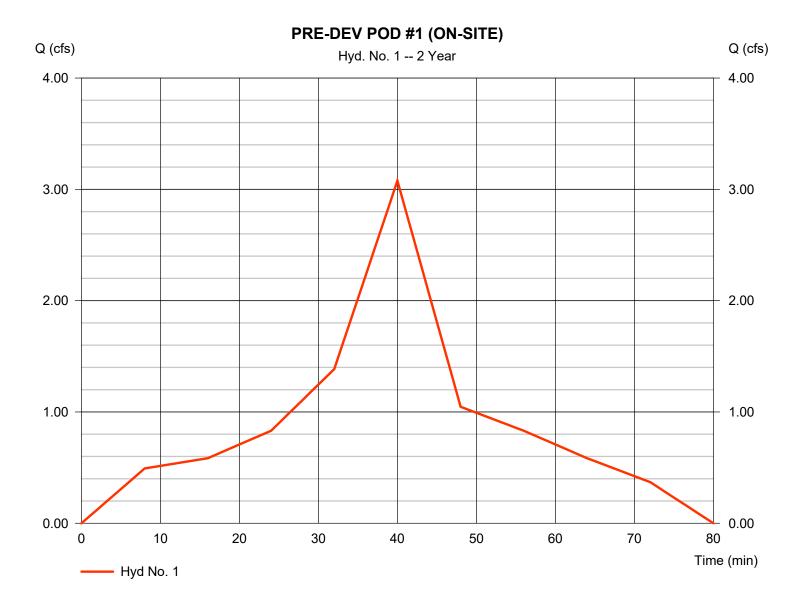
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Wednesday, 09 / 13 / 2023

Hyd. No. 1

PRE-DEV POD #1 (ON-SITE)

Hydrograph type = Dekalb Peak discharge = 3.078 cfsStorm frequency = 2 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 4,417 cuftRunoff coeff. Drainage area = 2.350 ac= 0.31Tc by User = 8.00 min Intensity = 4.224 in/hrIDF Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



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= 4.224 in/hr

Wednesday, 09 / 13 / 2023

 $= 8.00 \, \text{min}$

Hyd. No. 2

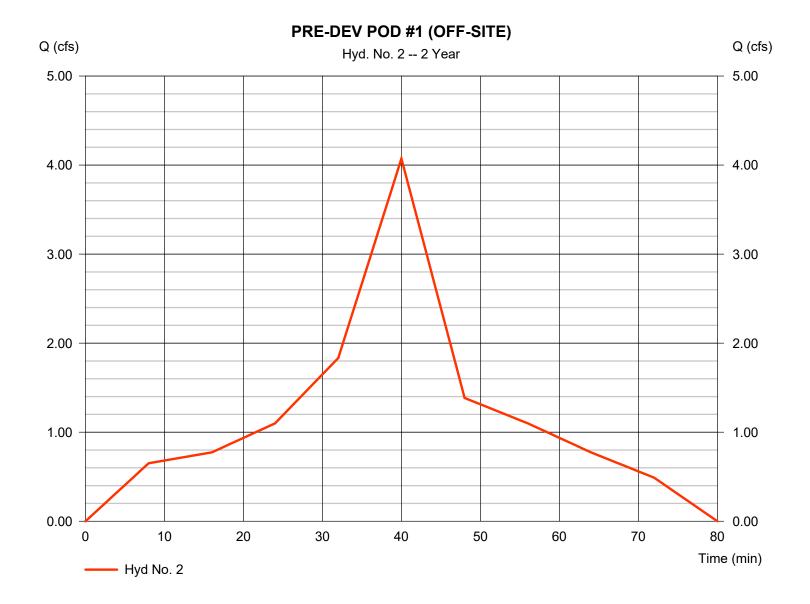
Intensity

PRE-DEV POD #1 (OFF-SITE)

= 4.072 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 2 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 5,845 cuftRunoff coeff. Drainage area = 2.410 ac= 0.4

Tc by User

IDF Curve = 2154-10_NOAA Intensities_Hy&Lset/likevol Dyfnb fact = n/a



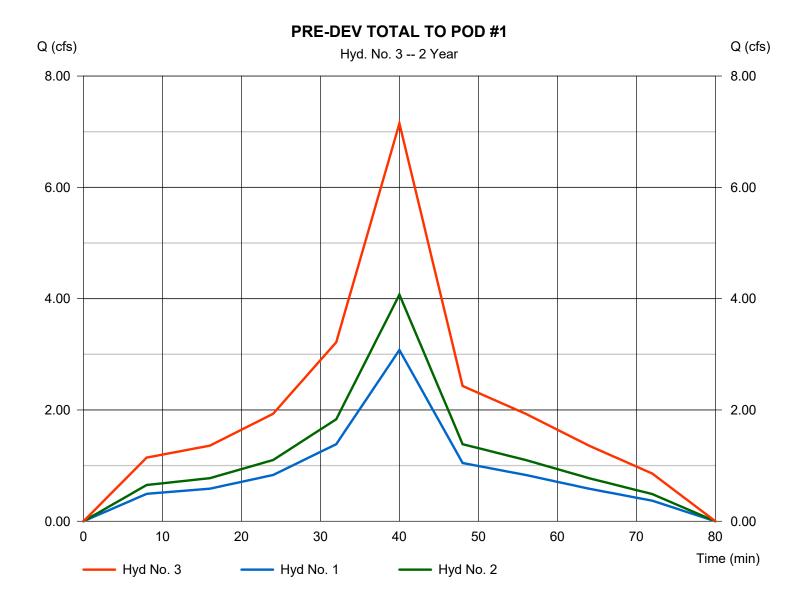
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Wednesday, 09 / 13 / 2023

Hyd. No. 3

PRE-DEV TOTAL TO POD #1

Hydrograph type Peak discharge = 7.150 cfs= Combine Time to peak Storm frequency = 2 yrs= 40 min Time interval = 1 min Hyd. volume = 10,262 cuft Inflow hyds. = 1, 2 Contrib. drain. area = 4.760 ac



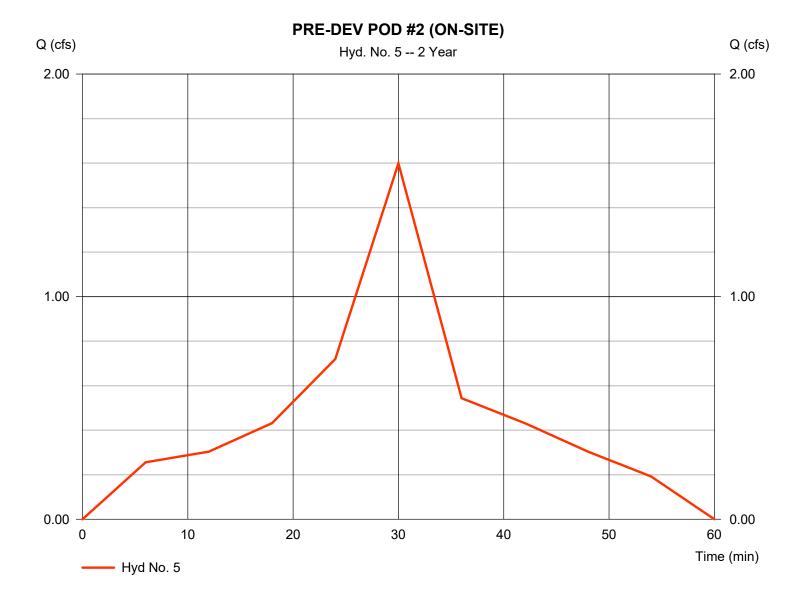
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Wednesday, 09 / 13 / 2023

Hyd. No. 5

PRE-DEV POD #2 (ON-SITE)

= 1.599 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 2 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 1,721 cuft Runoff coeff. = 0.33Drainage area = 1.050 acTc by User $= 6.00 \, \text{min}$ Intensity = 4.615 in/hr**IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



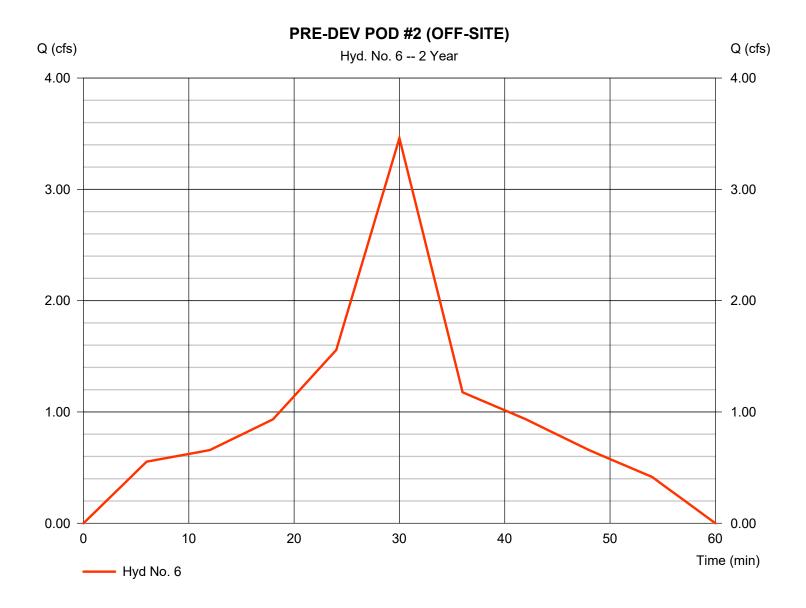
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Wednesday, 09 / 13 / 2023

Hyd. No. 6

PRE-DEV POD #2 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 3.460 cfsStorm frequency = 2 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 3,724 cuftRunoff coeff. Drainage area = 1.630 ac= 0.46Tc by User Intensity = 4.615 in/hr $= 6.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



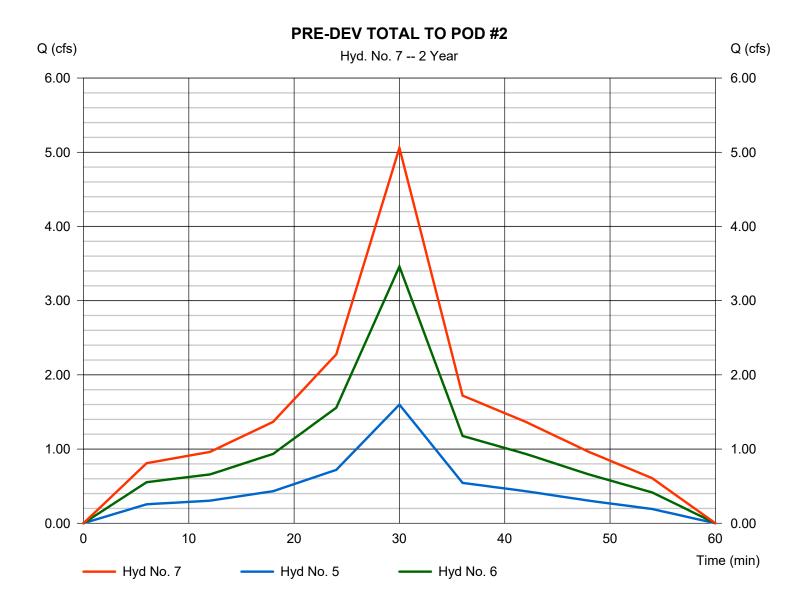
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Wednesday, 09 / 13 / 2023

Hyd. No. 7

PRE-DEV TOTAL TO POD #2

Hydrograph type Peak discharge = 5.059 cfs= Combine Time to peak Storm frequency = 2 yrs= 30 min Time interval = 1 min Hyd. volume = 5,445 cuftInflow hyds. Contrib. drain. area = 5, 6= 2.680 ac



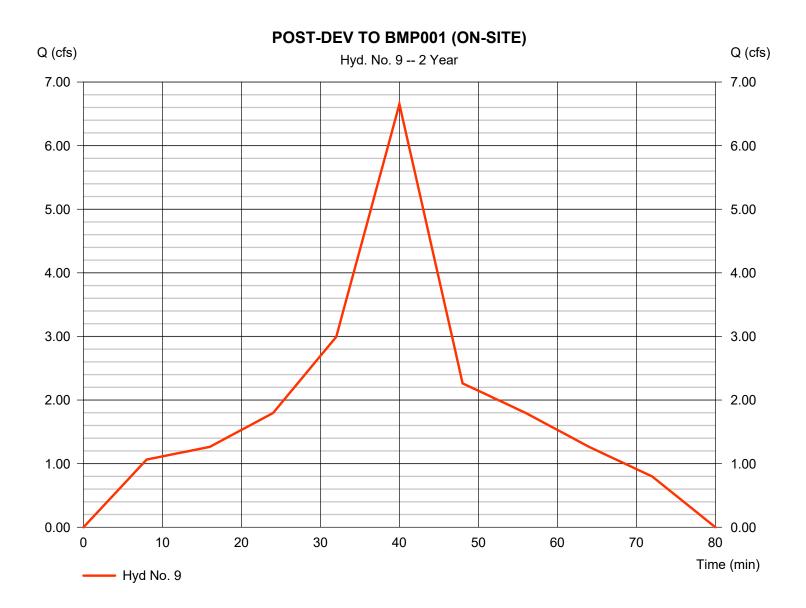
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Wednesday, 09 / 13 / 2023

Hyd. No. 9

POST-DEV TO BMP001 (ON-SITE)

= 6.654 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 2 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 9,549 cuftRunoff coeff. Drainage area = 2.500 ac= 0.63Tc by User Intensity = 4.224 in/hr $= 8.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



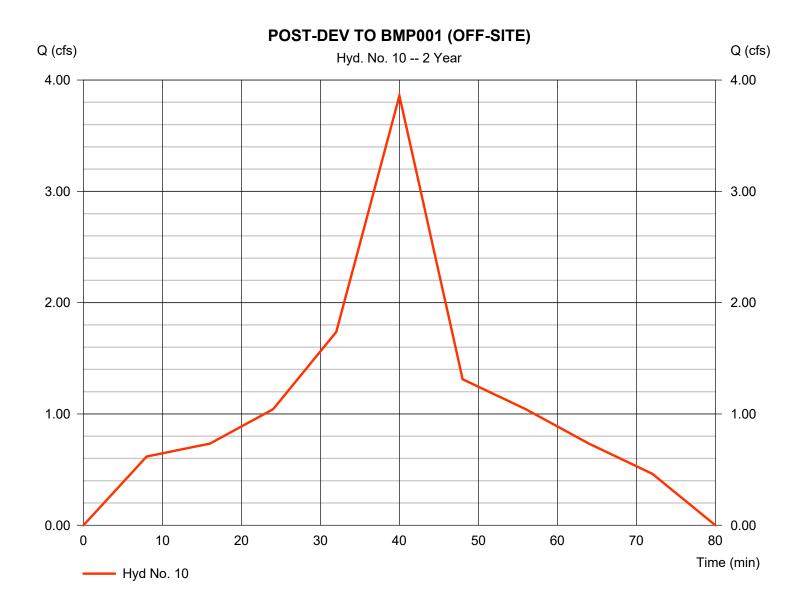
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Wednesday, 09 / 13 / 2023

Hyd. No. 10

POST-DEV TO BMP001 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 3.859 cfsStorm frequency = 2 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 5,539 cuftRunoff coeff. Drainage area = 2.030 ac= 0.45Tc by User Intensity = 4.224 in/hr $= 8.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



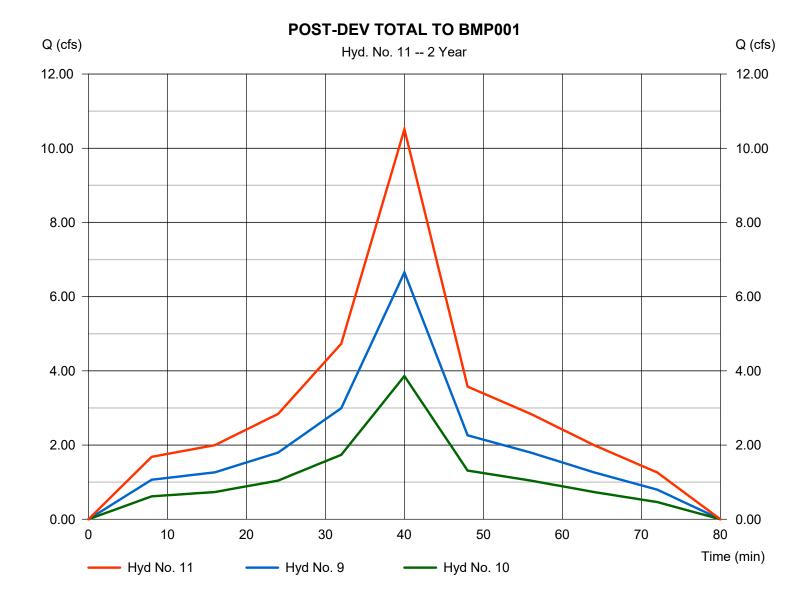
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Wednesday, 09 / 13 / 2023

Hyd. No. 11

POST-DEV TOTAL TO BMP001

Hydrograph type Peak discharge = 10.51 cfs= Combine Time to peak Storm frequency = 2 yrs= 40 min Time interval = 1 min Hyd. volume = 15,088 cuft Inflow hyds. = 9, 10 Contrib. drain. area = 4.530 ac



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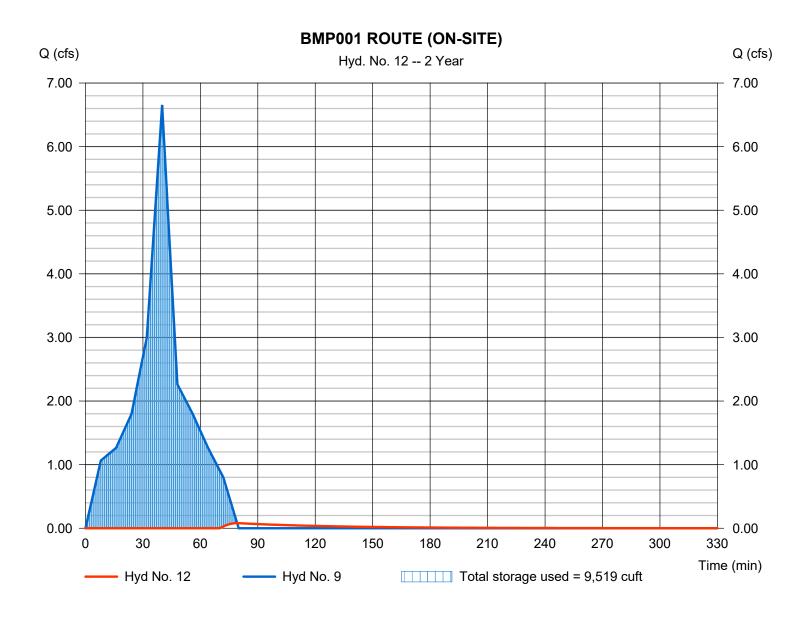
Wednesday, 09 / 13 / 2023

Hyd. No. 12

BMP001 ROUTE (ON-SITE)

Hydrograph type = Reservoir Peak discharge = 0.080 cfsStorm frequency Time to peak = 79 min = 2 yrsTime interval = 1 min Hyd. volume = 273 cuft = 9 - POST-DEV TO BMP001 (OMas/ITEE) vation Inflow hyd. No. = 134.04 ftReservoir name = BMP 001 Max. Storage = 9,519 cuft

Storage Indication method used.



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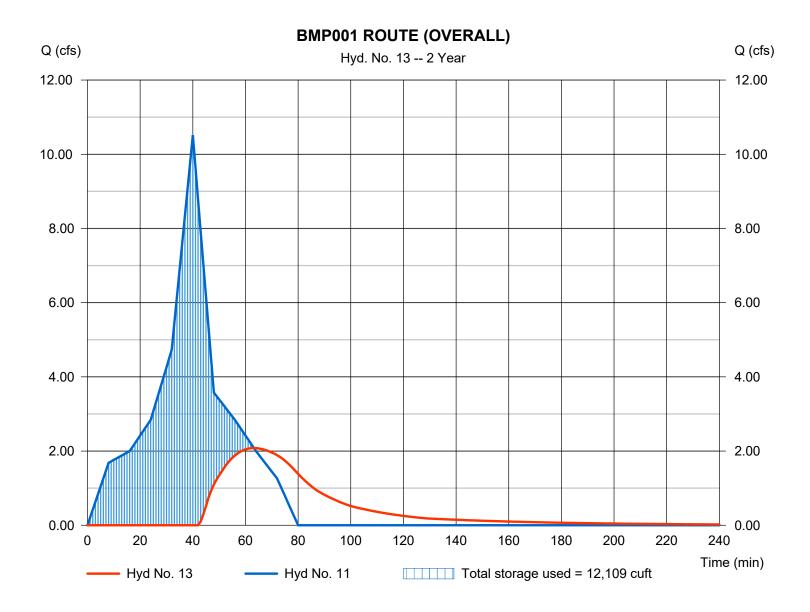
Wednesday, 09 / 13 / 2023

Hyd. No. 13

BMP001 ROUTE (OVERALL)

Hydrograph type = Reservoir Peak discharge = 2.082 cfsStorm frequency Time to peak = 63 min = 2 yrsTime interval = 1 min Hyd. volume = 5.812 cuft= 11 - POST-DEV TOTAL TO BNWP2001 Elevation Inflow hyd. No. = 134.50 ftReservoir name = BMP 001 Max. Storage = 12,109 cuft

Storage Indication method used.



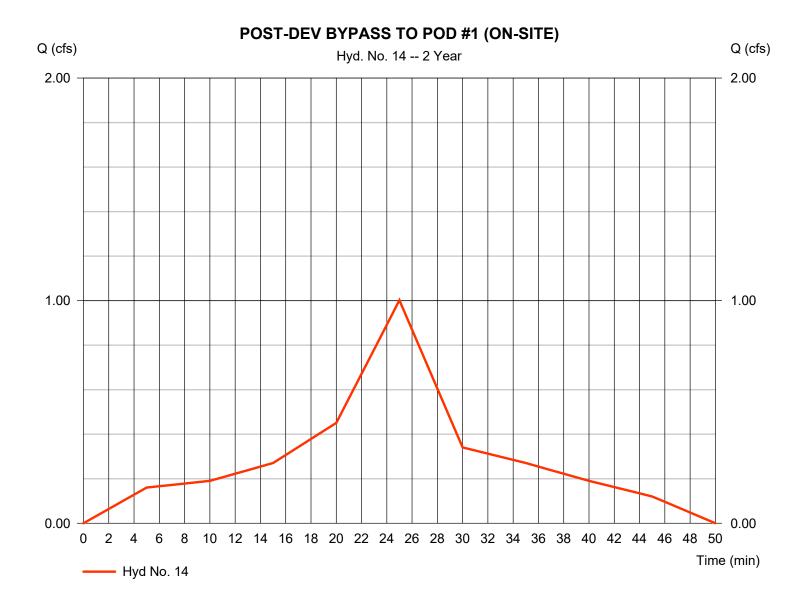
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Wednesday, 09 / 13 / 2023

Hyd. No. 14

POST-DEV BYPASS TO POD #1 (ON-SITE)

= 1.002 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 2 yrsTime to peak = 25 min Time interval = 1 min Hyd. volume = 899 cuft Runoff coeff. Drainage area = 0.460 ac= 0.45Tc by User $= 5.00 \, \text{min}$ Intensity = 4.840 in/hrIDF Curve = 2154-10_NOAA Intensities_HyAlsadianediane fact = n/a



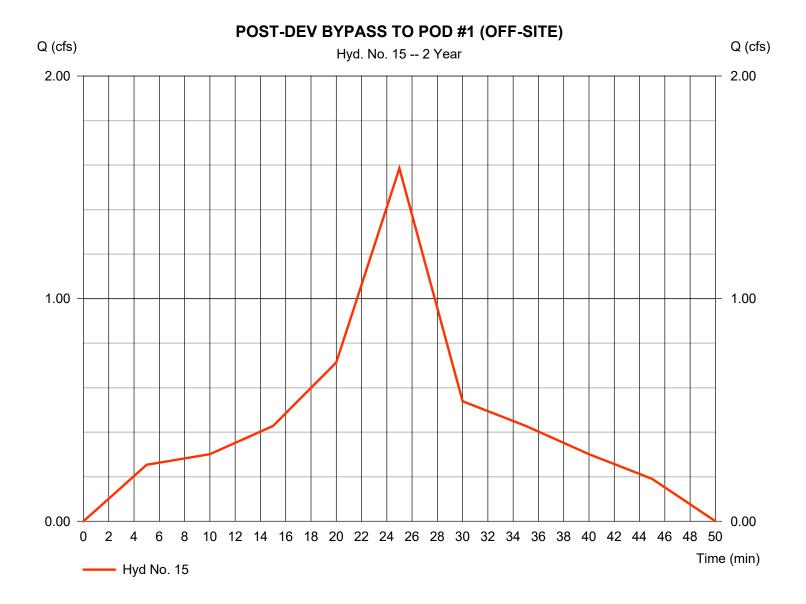
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Wednesday, 09 / 13 / 2023

Hyd. No. 15

POST-DEV BYPASS TO POD #1 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 1.586 cfsStorm frequency = 2 yrsTime to peak = 25 min Time interval = 1 min Hyd. volume = 1,422 cuft Runoff coeff. Drainage area = 0.910 ac= 0.36Tc by User $= 5.00 \, \text{min}$ Intensity = 4.840 in/hrIDF Curve = 2154-10_NOAA Intensities_HyAlsat/liRved Dyfn fact = n/a



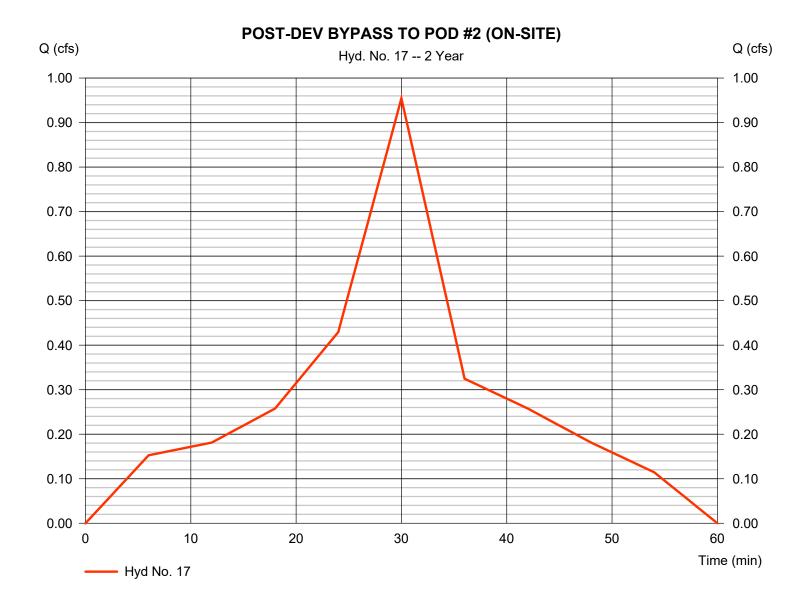
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Wednesday, 09 / 13 / 2023

Hyd. No. 17

POST-DEV BYPASS TO POD #2 (ON-SITE)

Hydrograph type = Dekalb Peak discharge = 0.954 cfsStorm frequency = 2 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 1,027 cuftRunoff coeff. Drainage area = 0.440 ac= 0.47Tc by User Intensity = 4.615 in/hr $= 6.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



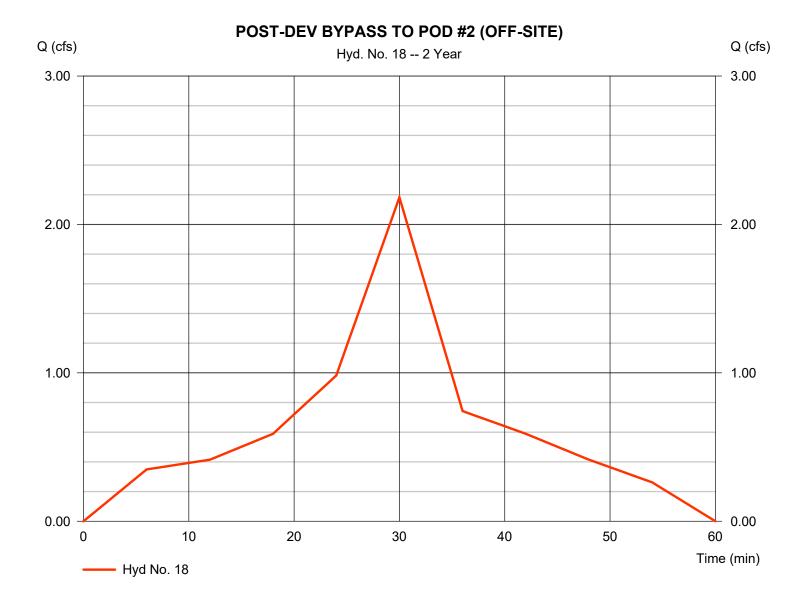
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Wednesday, 09 / 13 / 2023

Hyd. No. 18

POST-DEV BYPASS TO POD #2 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 2.183 cfsStorm frequency = 2 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 2,349 cuftRunoff coeff. Drainage area = 1.100 ac= 0.43Tc by User = 6.00 min Intensity = 4.615 in/hr**IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



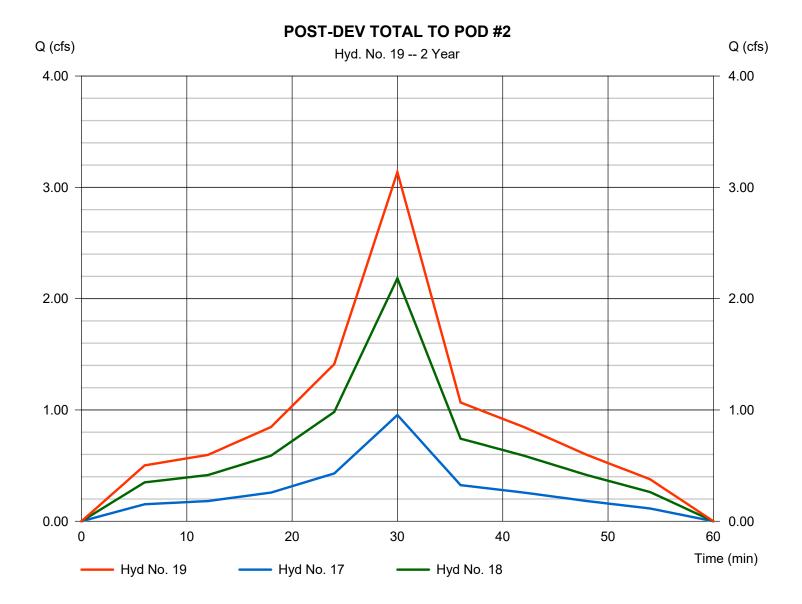
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Wednesday, 09 / 13 / 2023

Hyd. No. 19

POST-DEV TOTAL TO POD #2

Hydrograph type Peak discharge = 3.137 cfs= Combine Time to peak Storm frequency = 2 yrs= 30 min Time interval = 1 min Hyd. volume = 3,377 cuftInflow hyds. = 17, 18 Contrib. drain. area = 1.540 ac



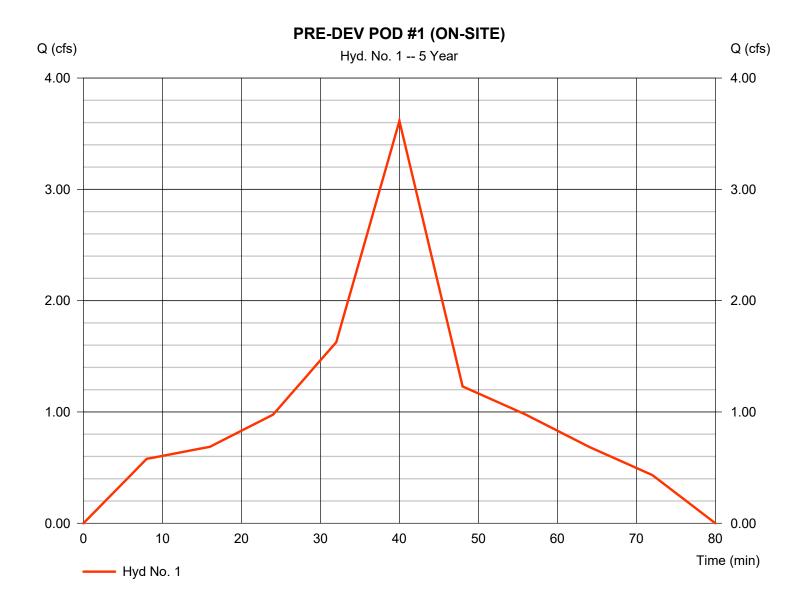
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Wednesday, 09 / 13 / 2023

Hyd. No. 1

PRE-DEV POD #1 (ON-SITE)

Hydrograph type = Dekalb Peak discharge = 3.615 cfsStorm frequency = 5 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 5,188 cuftRunoff coeff. Drainage area = 2.350 ac= 0.31Tc by User $= 8.00 \, \text{min}$ Intensity = 4.962 in/hr**IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



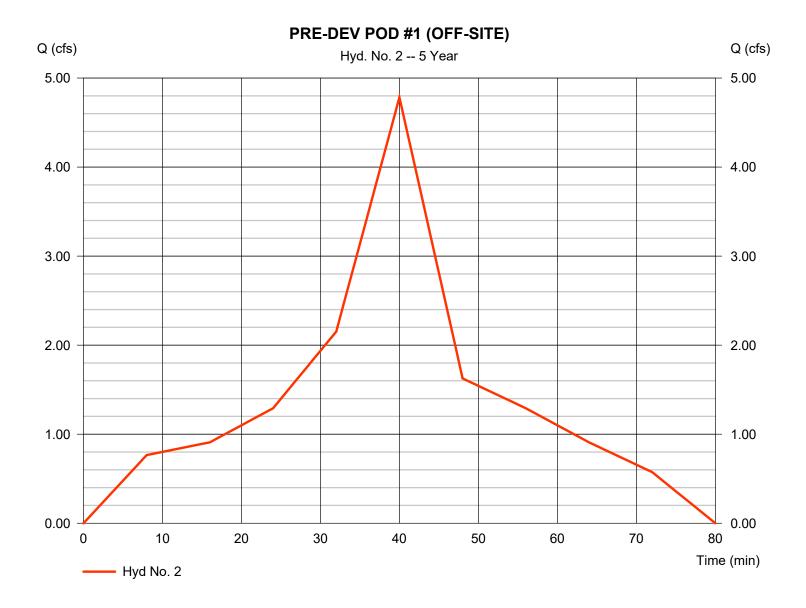
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Wednesday, 09 / 13 / 2023

Hyd. No. 2

PRE-DEV POD #1 (OFF-SITE)

= 4.783 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 5 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 6,865 cuftRunoff coeff. Drainage area = 2.410 ac= 0.4Tc by User Intensity = 4.962 in/hr $= 8.00 \, \text{min}$ IDF Curve = 2154-10_NOAA Intensities_HyAlsan/Revol Diffi b fact = n/a



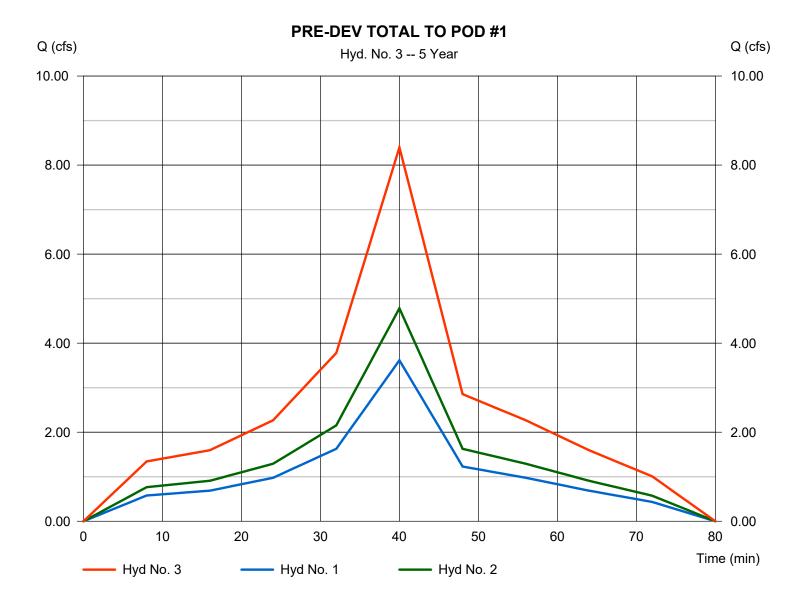
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Wednesday, 09 / 13 / 2023

Hyd. No. 3

PRE-DEV TOTAL TO POD #1

Hydrograph type Peak discharge = 8.398 cfs= Combine Time to peak Storm frequency = 5 yrs= 40 min Time interval = 1 min Hyd. volume = 12,053 cuftInflow hyds. = 1, 2 Contrib. drain. area = 4.760 ac



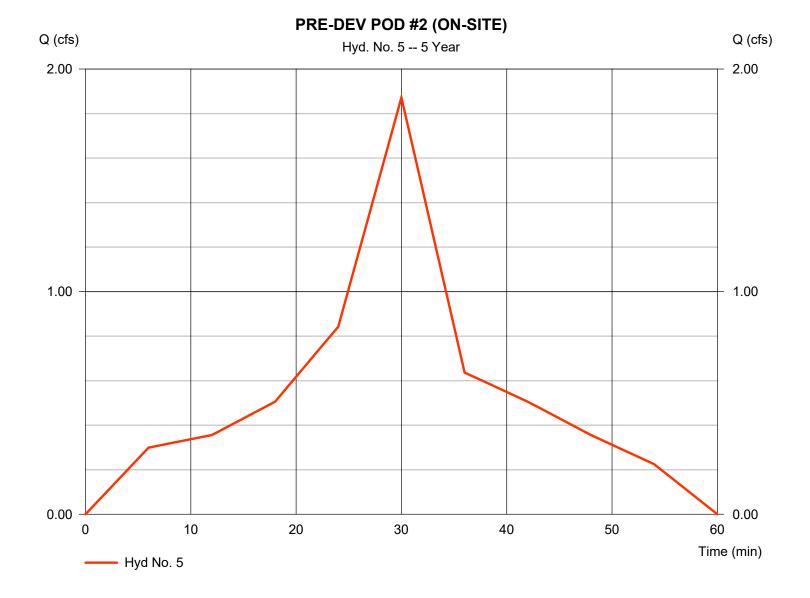
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Wednesday, 09 / 13 / 2023

Hyd. No. 5

PRE-DEV POD #2 (ON-SITE)

Hydrograph type = Dekalb Peak discharge = 1.872 cfsStorm frequency = 5 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 2,015 cuftRunoff coeff. Drainage area = 1.050 ac= 0.33Tc by User $= 6.00 \, \text{min}$ Intensity = 5.403 in/hr**IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



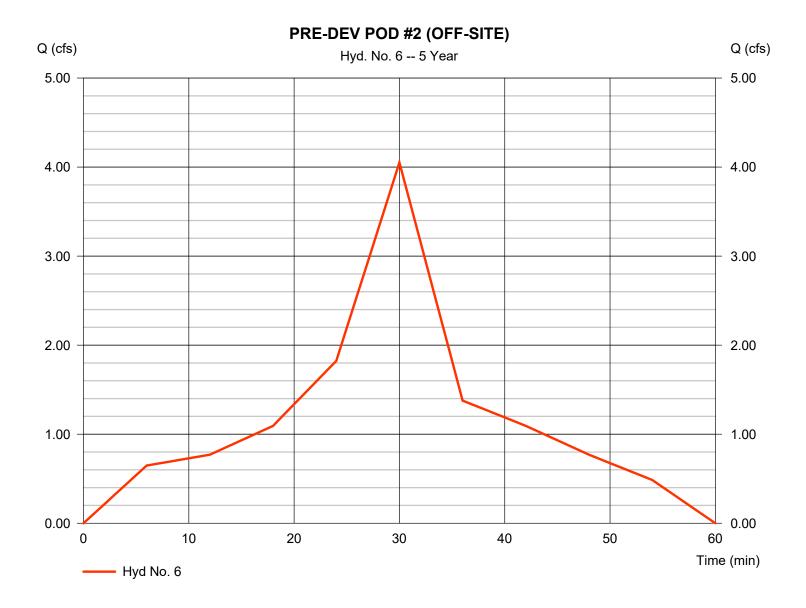
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 6

PRE-DEV POD #2 (OFF-SITE)

= 4.051 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 5 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 4,361 cuftRunoff coeff. Drainage area = 1.630 ac= 0.46Tc by User = 6.00 min Intensity = 5.403 in/hr**IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



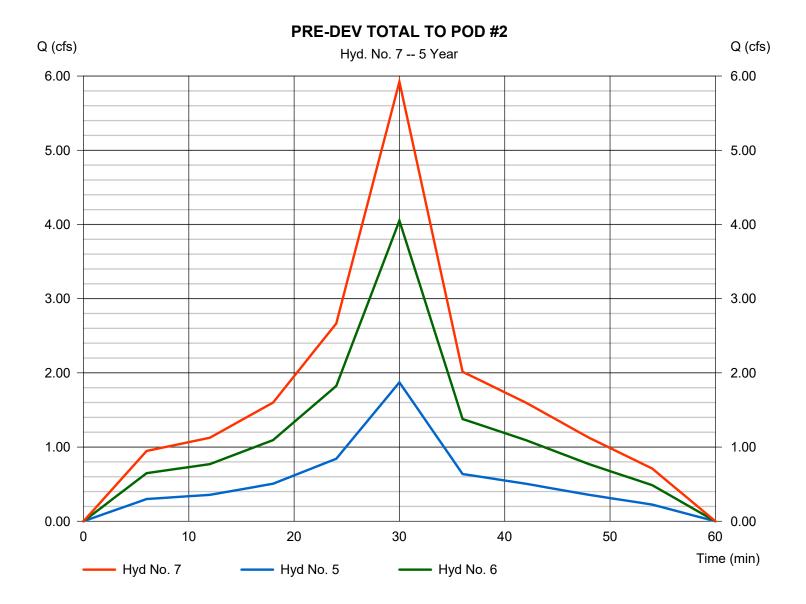
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 7

PRE-DEV TOTAL TO POD #2

Hydrograph type Peak discharge = 5.923 cfs= Combine Time to peak Storm frequency = 5 yrs= 30 min = 6,376 cuft Time interval = 1 min Hyd. volume Inflow hyds. Contrib. drain. area = 2.680 ac= 5, 6



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

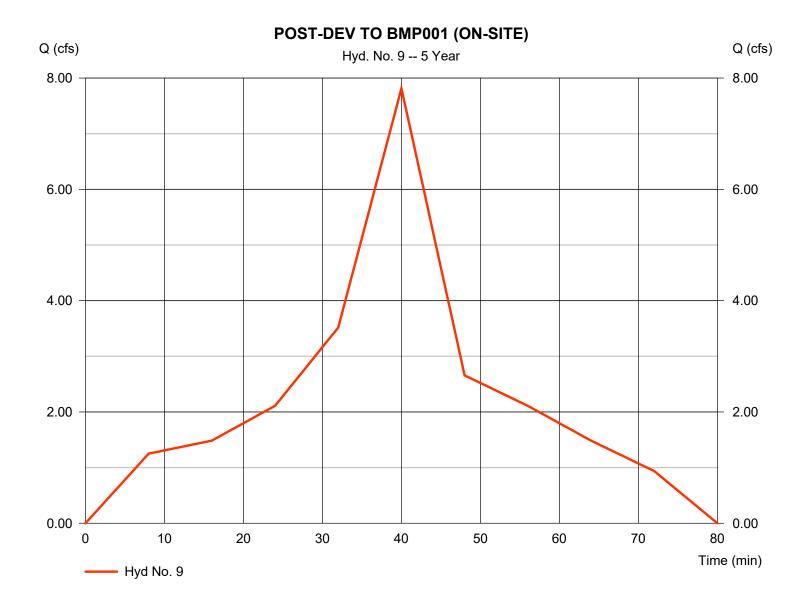
Wednesday, 09 / 13 / 2023

Hyd. No. 9

POST-DEV TO BMP001 (ON-SITE)

= 7.815 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 5 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 11,216 cuft Runoff coeff. Drainage area = 2.500 ac= 0.63Tc by User $= 8.00 \, \text{min}$ Intensity = 4.962 in/hr

IDF Curve = 2154-10_NOAA Intensities_Hy&lsædilikevod DMnb fact = n/a



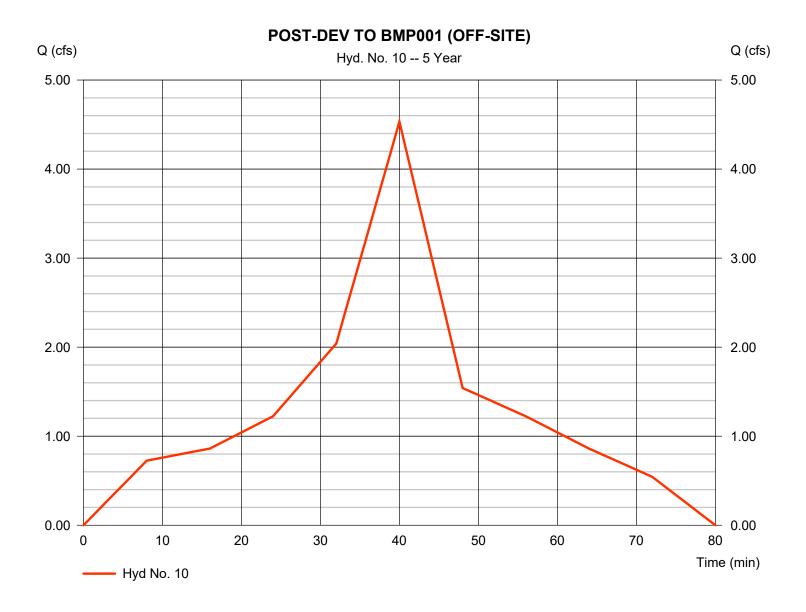
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 10

POST-DEV TO BMP001 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 4.533 cfsStorm frequency = 5 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 6,505 cuftRunoff coeff. Drainage area = 2.030 ac= 0.45Tc by User Intensity = 4.962 in/hr $= 8.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



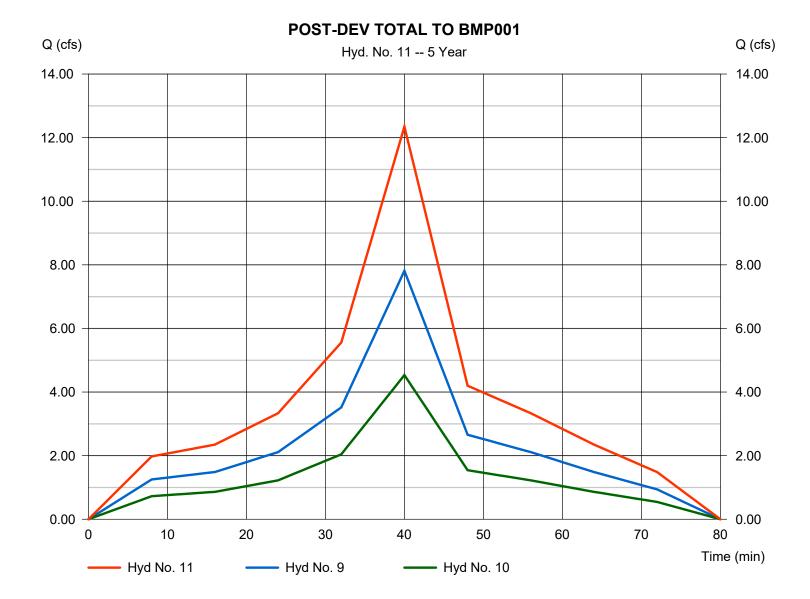
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 11

POST-DEV TOTAL TO BMP001

Hydrograph type Peak discharge = 12.35 cfs= Combine Time to peak Storm frequency = 5 yrs= 40 min Time interval = 1 min Hyd. volume = 17,721 cuft Inflow hyds. = 9, 10 Contrib. drain. area = 4.530 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

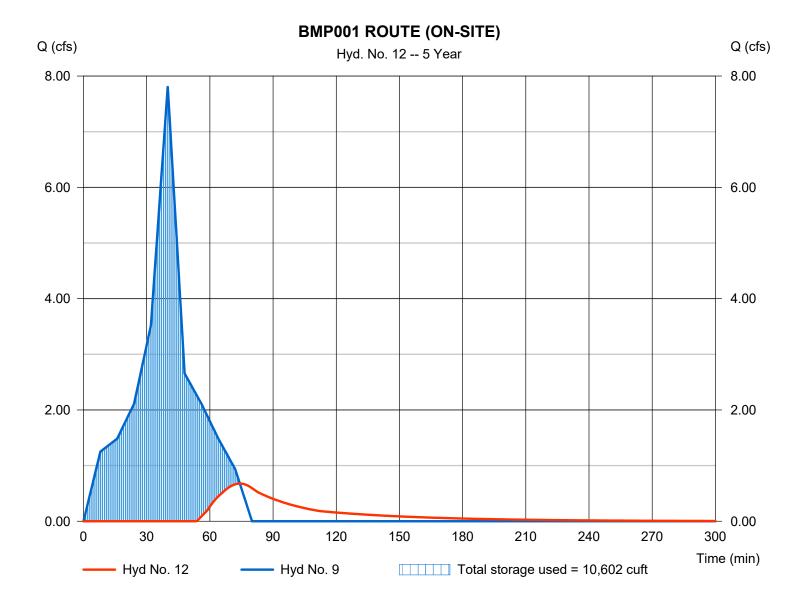
Wednesday, 09 / 13 / 2023

Hyd. No. 12

BMP001 ROUTE (ON-SITE)

Hydrograph type = Reservoir Peak discharge = 0.678 cfsStorm frequency = 5 yrsTime to peak = 74 min Time interval = 1 min Hyd. volume = 1,940 cuftInflow hyd. No. = 9 - POST-DEV TO BMP001 (OMas) Temp vation = 134.24 ftReservoir name = BMP 001 Max. Storage = 10,602 cuft

Storage Indication method used.



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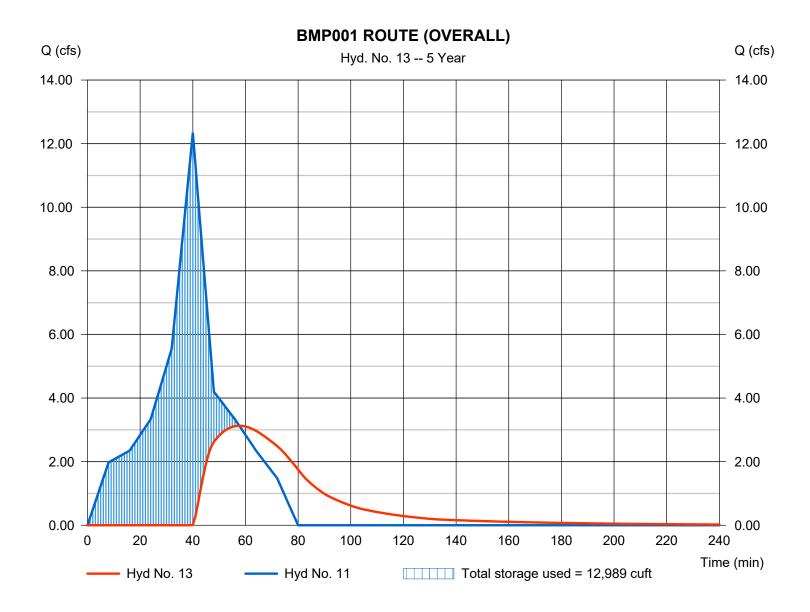
Wednesday, 09 / 13 / 2023

Hyd. No. 13

BMP001 ROUTE (OVERALL)

Hydrograph type = Reservoir Peak discharge = 3.128 cfsStorm frequency Time to peak = 58 min = 5 yrsTime interval = 1 min Hyd. volume = 8,445 cuft = 11 - POST-DEV TOTAL TO BNWP2001 Elevation Inflow hyd. No. = 134.66 ftReservoir name = BMP 001 Max. Storage = 12,989 cuft

Storage Indication method used.



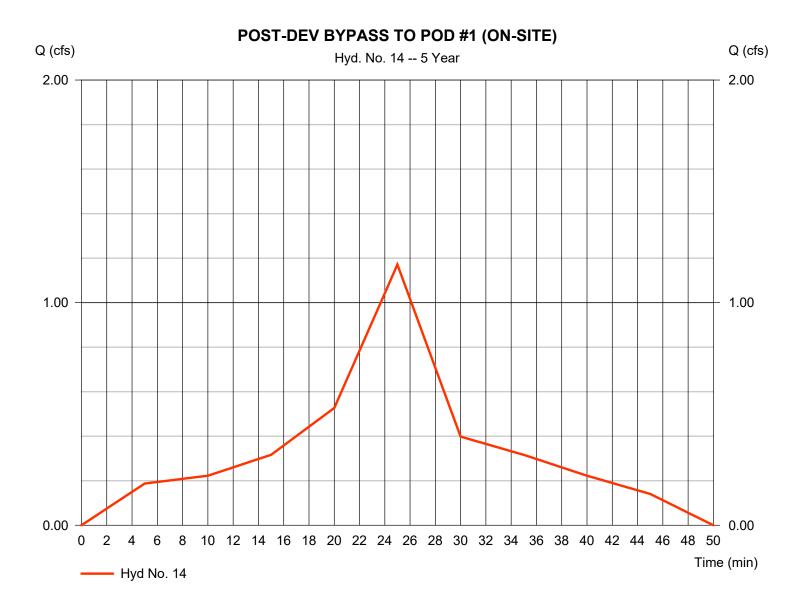
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 14

POST-DEV BYPASS TO POD #1 (ON-SITE)

= 1.171 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 5 yrsTime to peak = 25 min Time interval = 1 min Hyd. volume = 1,051 cuftRunoff coeff. Drainage area = 0.460 ac= 0.45Tc by User $= 5.00 \, \text{min}$ Intensity = 5.658 in/hrIDF Curve = 2154-10_NOAA Intensities_HyAlsadianediane fact = n/a



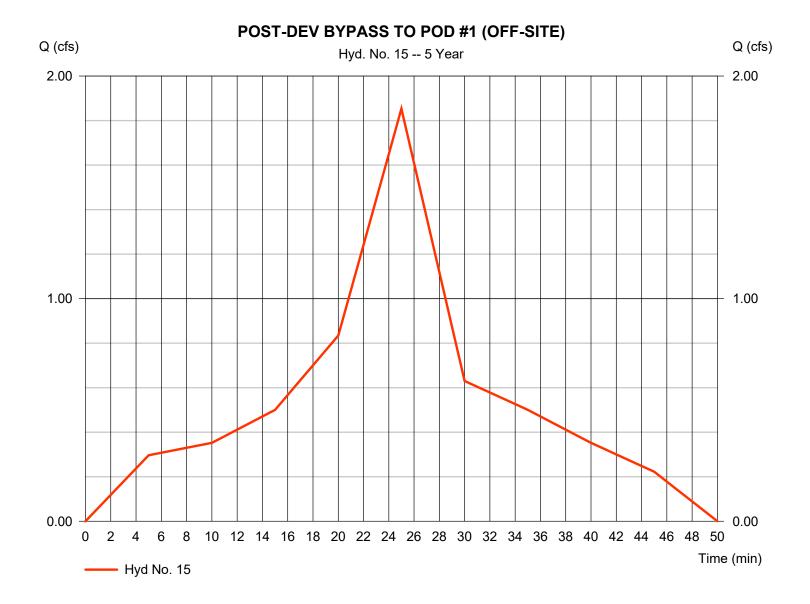
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 15

POST-DEV BYPASS TO POD #1 (OFF-SITE)

= 1.853 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 5 yrsTime to peak = 25 min Time interval = 1 min Hyd. volume = 1,663 cuftRunoff coeff. Drainage area = 0.910 ac= 0.36Tc by User $= 5.00 \, \text{min}$ Intensity = 5.658 in/hrIDF Curve = 2154-10_NOAA Intensities_HyAlsadianediane fact = n/a



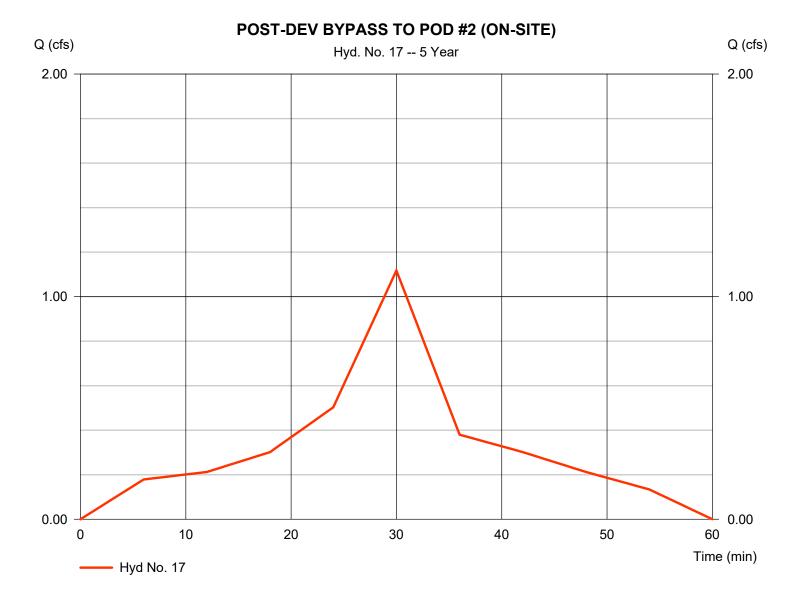
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 17

POST-DEV BYPASS TO POD #2 (ON-SITE)

= 1.117 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 5 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 1,203 cuftRunoff coeff. Drainage area = 0.440 ac= 0.47Tc by User Intensity = 5.403 in/hr $= 6.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



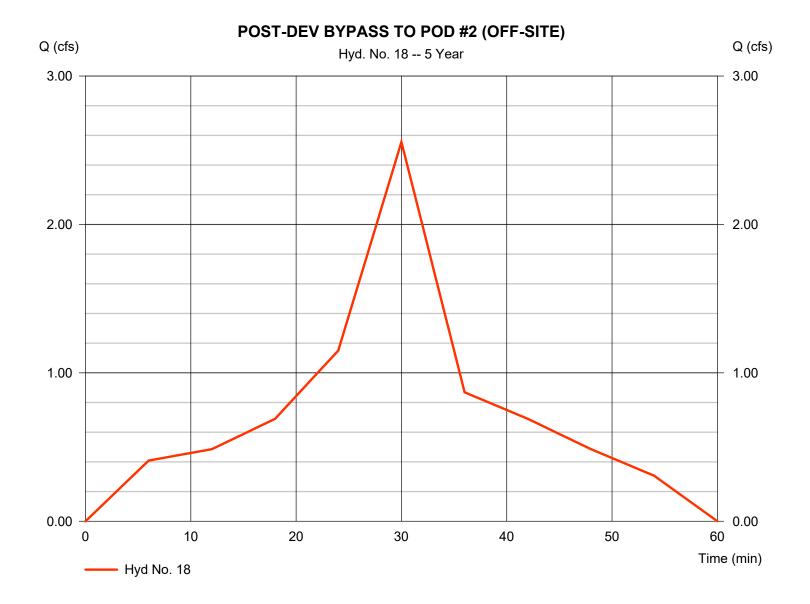
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 18

POST-DEV BYPASS TO POD #2 (OFF-SITE)

= 2.556 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 5 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 2,751 cuftRunoff coeff. Drainage area = 1.100 ac= 0.43Tc by User = 6.00 min Intensity = 5.403 in/hr**IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



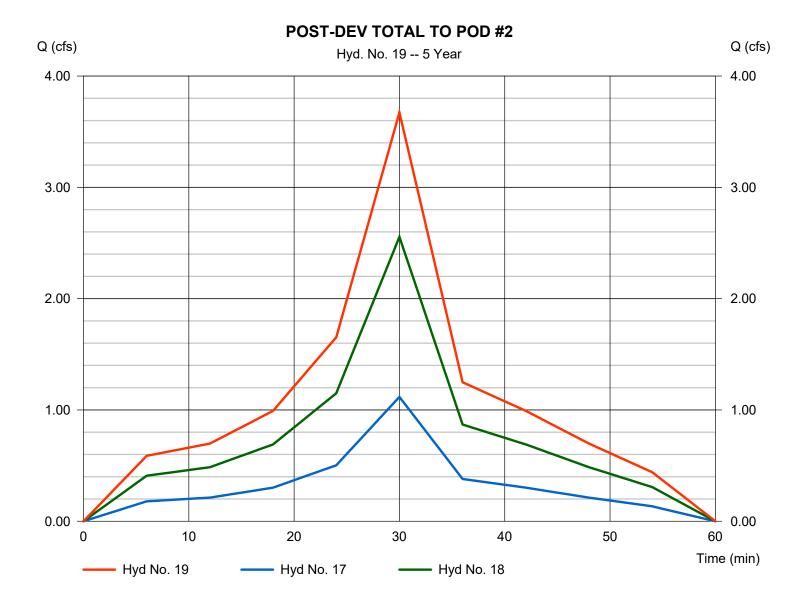
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 19

POST-DEV TOTAL TO POD #2

Hydrograph type Peak discharge = 3.673 cfs= Combine Time to peak Storm frequency = 5 yrs= 30 min Time interval = 1 min Hyd. volume = 3,954 cuftInflow hyds. = 17, 18 Contrib. drain. area = 1.540 ac



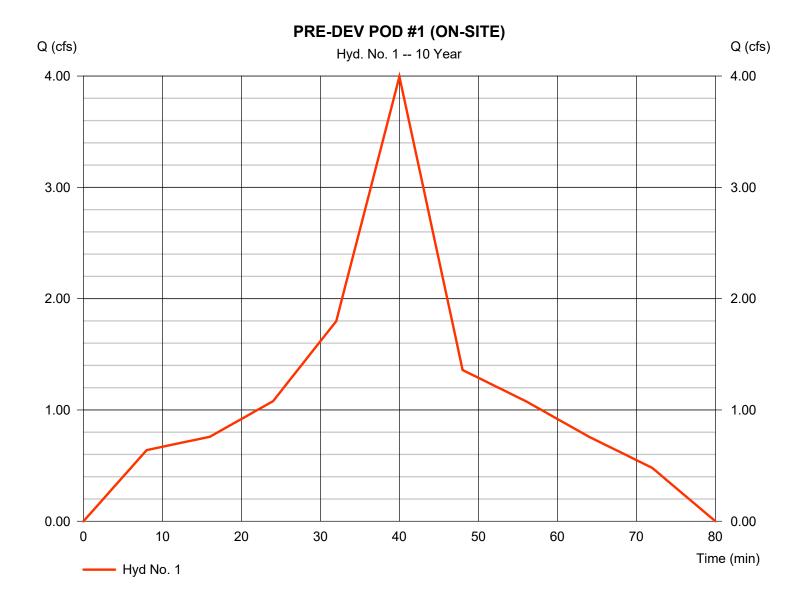
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Wednesday, 09 / 13 / 2023

Hyd. No. 1

PRE-DEV POD #1 (ON-SITE)

Hydrograph type = Dekalb Peak discharge = 3.995 cfsStorm frequency = 10 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 5,734 cuftRunoff coeff. Drainage area = 2.350 ac= 0.31Tc by User Intensity = 5.485 in/hr $= 8.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

= n/a

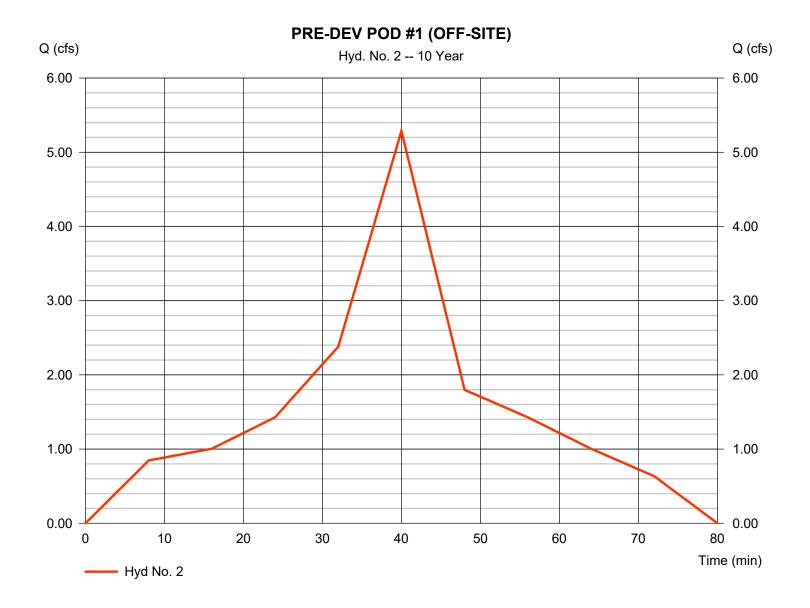
Hyd. No. 2

IDF Curve

PRE-DEV POD #1 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 5.287 cfsStorm frequency = 10 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 7,588 cuftRunoff coeff. Drainage area = 2.410 ac= 0.4Tc by User Intensity = 5.485 in/hr $= 8.00 \, \text{min}$

= 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact



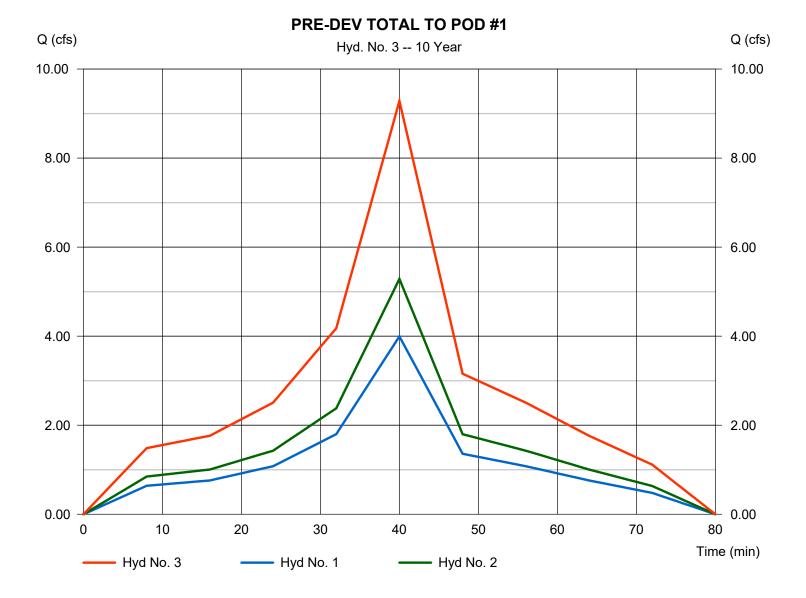
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Wednesday, 09 / 13 / 2023

Hyd. No. 3

PRE-DEV TOTAL TO POD #1

Hydrograph type = Combine Peak discharge = 9.283 cfsTime to peak Storm frequency = 10 yrs= 40 min Time interval = 1 min Hyd. volume = 13,322 cuft Inflow hyds. = 1, 2 Contrib. drain. area = 4.760 ac



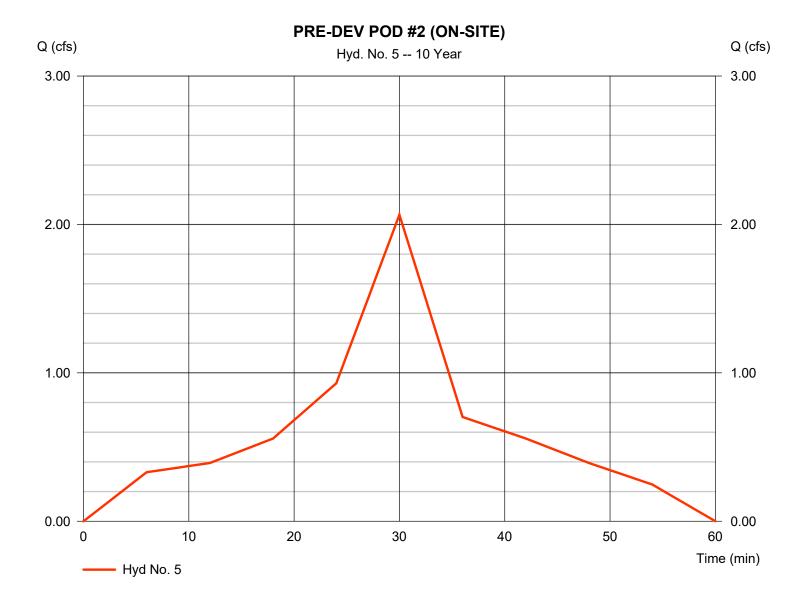
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 5

PRE-DEV POD #2 (ON-SITE)

= 2.065 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 10 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 2,223 cuftRunoff coeff. = 0.33Drainage area = 1.050 acTc by User Intensity = 5.960 in/hr $= 6.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



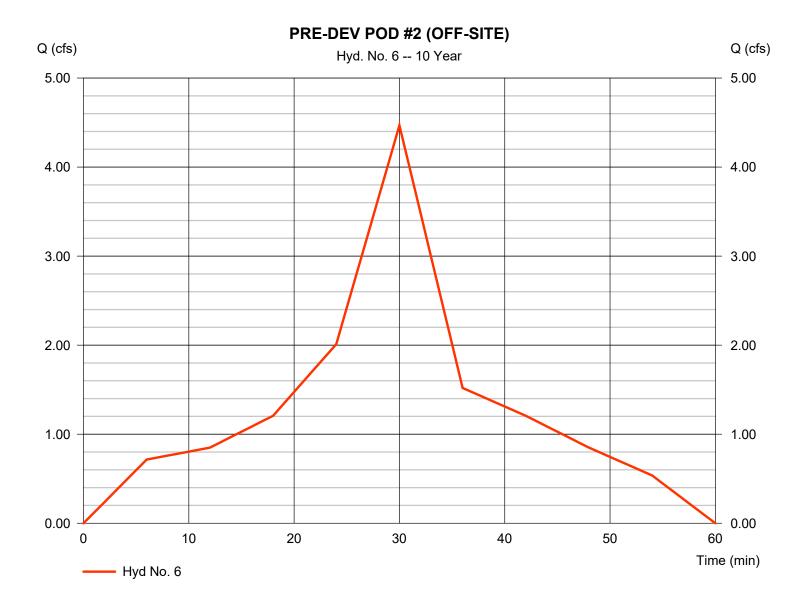
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Wednesday, 09 / 13 / 2023

Hyd. No. 6

PRE-DEV POD #2 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 4.469 cfsStorm frequency = 10 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 4.810 cuftRunoff coeff. Drainage area = 1.630 ac= 0.46Tc by User Intensity = 5.960 in/hr $= 6.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_HyAlsan/Revol Diffi b fact = n/a



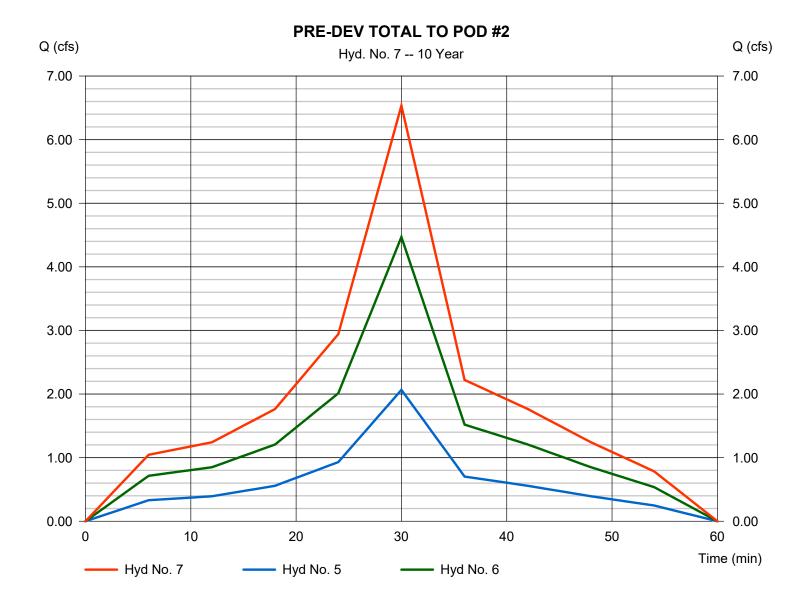
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 7

PRE-DEV TOTAL TO POD #2

Hydrograph type = Combine Peak discharge = 6.534 cfsTime to peak Storm frequency = 10 yrs= 30 min Time interval = 1 min Hyd. volume = 7,033 cuftInflow hyds. Contrib. drain. area = 2.680 ac= 5, 6



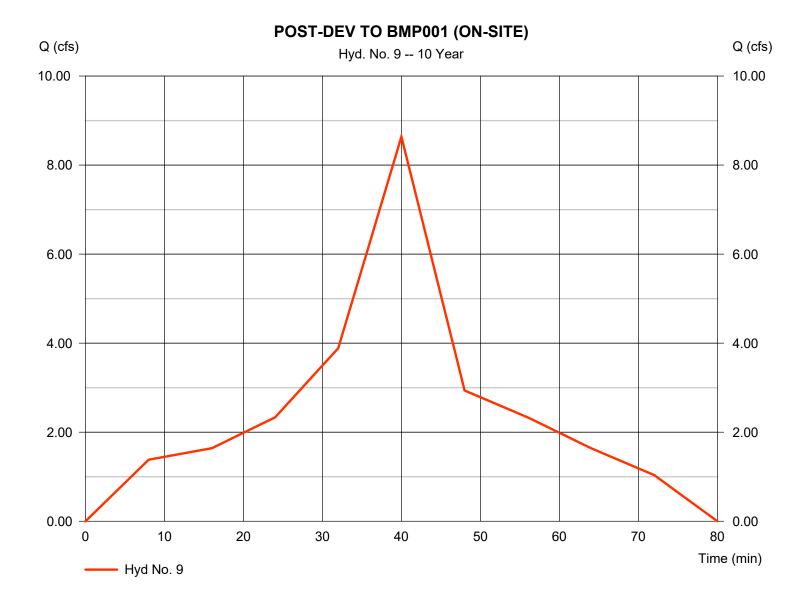
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Wednesday, 09 / 13 / 2023

Hyd. No. 9

POST-DEV TO BMP001 (ON-SITE)

Peak discharge = 8.638 cfsHydrograph type = Dekalb Storm frequency = 10 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 12,397 cuftRunoff coeff. Drainage area = 2.500 ac= 0.63Tc by User $= 8.00 \, \text{min}$ Intensity = 5.485 in/hr**IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



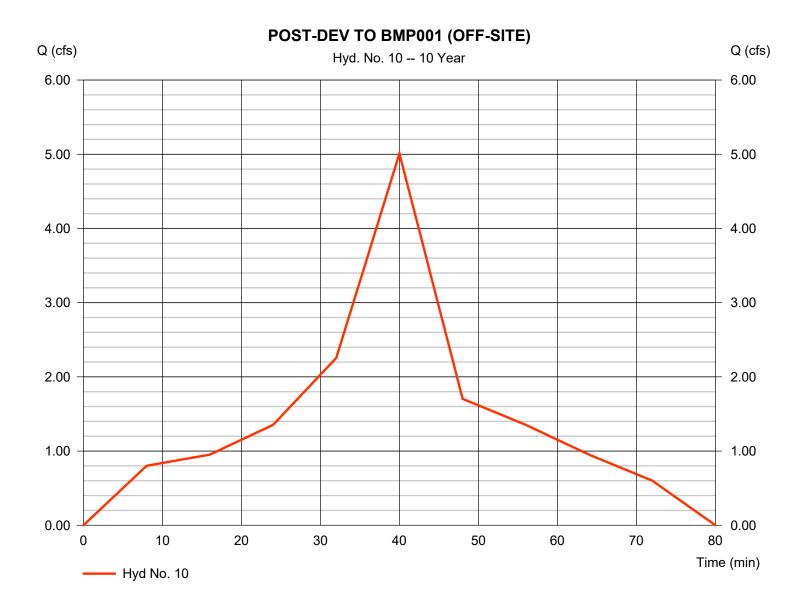
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 10

POST-DEV TO BMP001 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 5.010 cfsStorm frequency = 10 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 7,191 cuftRunoff coeff. Drainage area = 2.030 ac= 0.45Tc by User Intensity = 5.485 in/hr $= 8.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



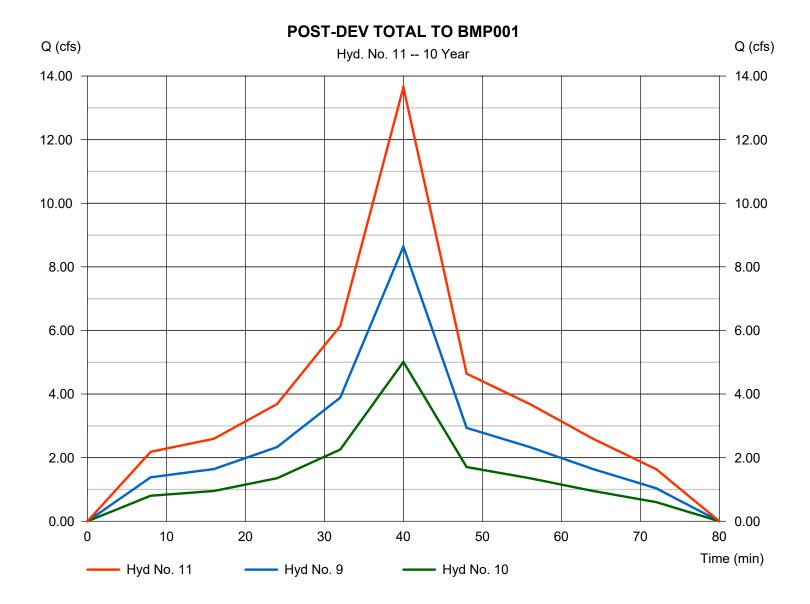
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 11

POST-DEV TOTAL TO BMP001

Hydrograph type = Combine Peak discharge = 13.65 cfsTime to peak Storm frequency = 10 yrs= 40 min Time interval = 1 min Hyd. volume = 19,588 cuft Inflow hyds. = 9, 10 Contrib. drain. area = 4.530 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

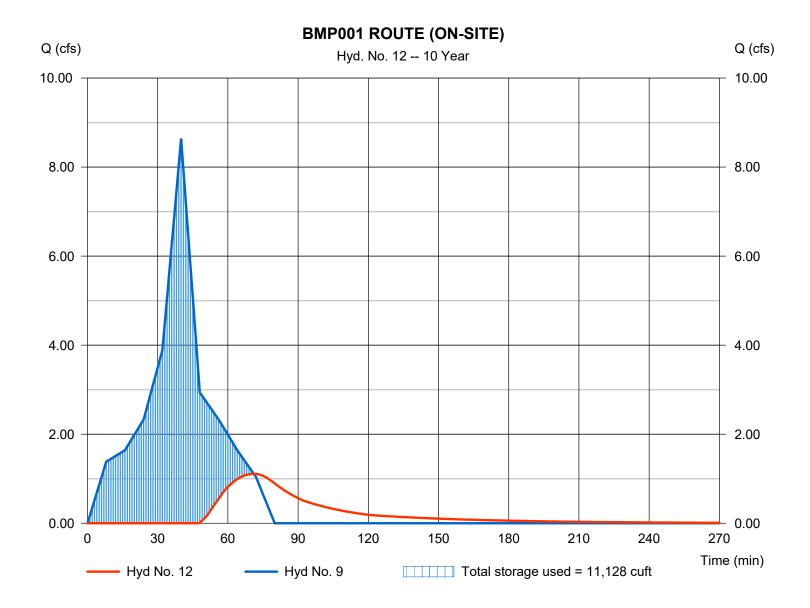
Wednesday, 09 / 13 / 2023

Hyd. No. 12

BMP001 ROUTE (ON-SITE)

Hydrograph type = Reservoir Peak discharge = 1.109 cfsStorm frequency = 10 yrsTime to peak = 71 min Time interval = 1 min Hyd. volume = 3,121 cuftInflow hyd. No. = 9 - POST-DEV TO BMP001 (OMas) Temp vation = 134.33 ftReservoir name = BMP 001 Max. Storage = 11,128 cuft

Storage Indication method used.



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

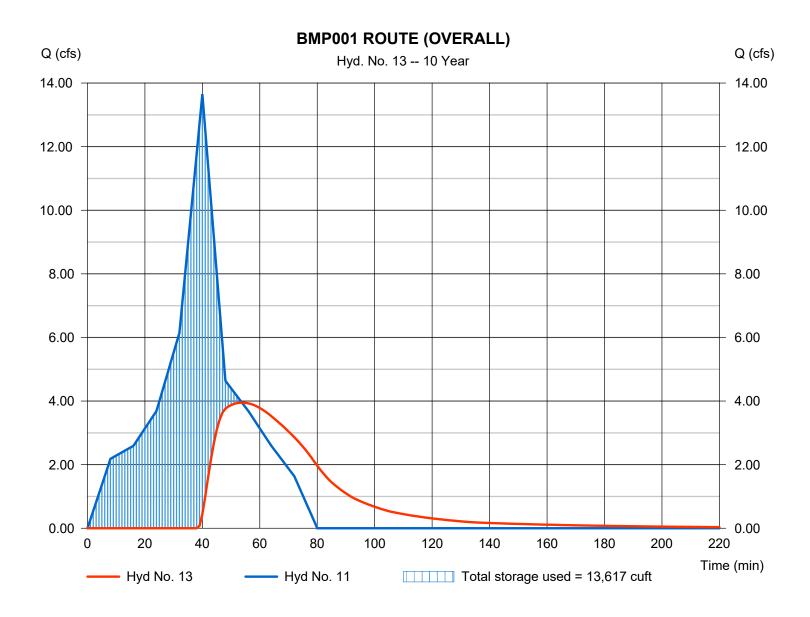
Wednesday, 09 / 13 / 2023

Hyd. No. 13

BMP001 ROUTE (OVERALL)

Hydrograph type = Reservoir Peak discharge = 3.949 cfsStorm frequency = 10 yrsTime to peak = 54 min Time interval = 1 min Hyd. volume = 10,312 cuft= 11 - POST-DEV TOTAL TO BNWP2001 Elevation Inflow hyd. No. = 134.77 ft= 13,617 cuft Reservoir name = BMP 001 Max. Storage

Storage Indication method used.



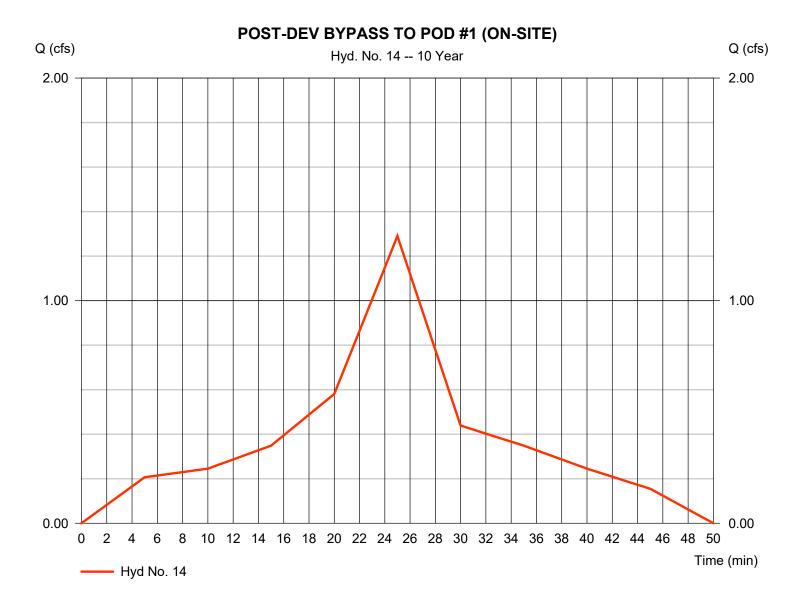
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Wednesday, 09 / 13 / 2023

Hyd. No. 14

POST-DEV BYPASS TO POD #1 (ON-SITE)

= 1.291 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 10 yrsTime to peak = 25 min Time interval = 1 min Hyd. volume = 1,158 cuftRunoff coeff. Drainage area = 0.460 ac= 0.45Tc by User $= 5.00 \, \text{min}$ Intensity = 6.235 in/hrIDF Curve = 2154-10_NOAA Intensities_HyAlsadianediane fact = n/a



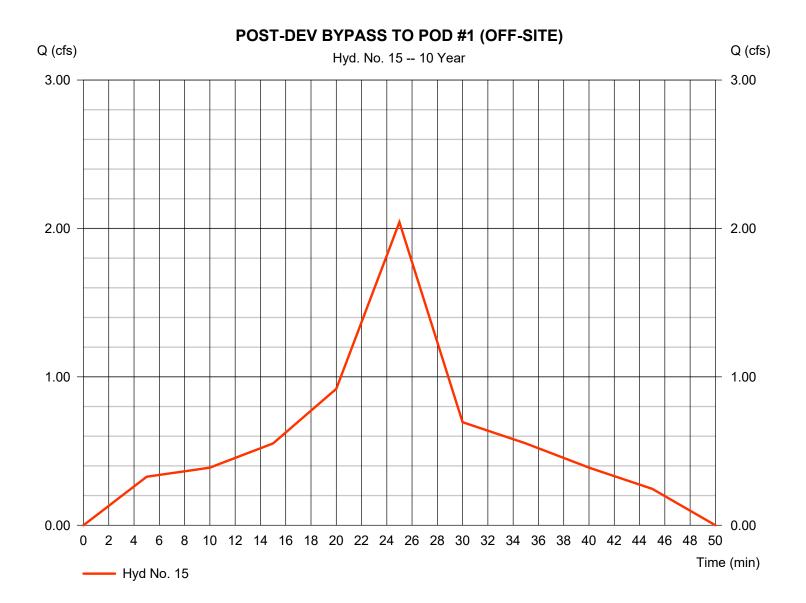
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Wednesday, 09 / 13 / 2023

Hyd. No. 15

POST-DEV BYPASS TO POD #1 (OFF-SITE)

= 2.043 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 10 yrsTime to peak = 25 min Time interval = 1 min Hyd. volume = 1,832 cuft Runoff coeff. Drainage area = 0.910 ac= 0.36Tc by User $= 5.00 \, \text{min}$ Intensity = 6.235 in/hrIDF Curve = 2154-10_NOAA Intensities_HyAlsadianediane fact = n/a



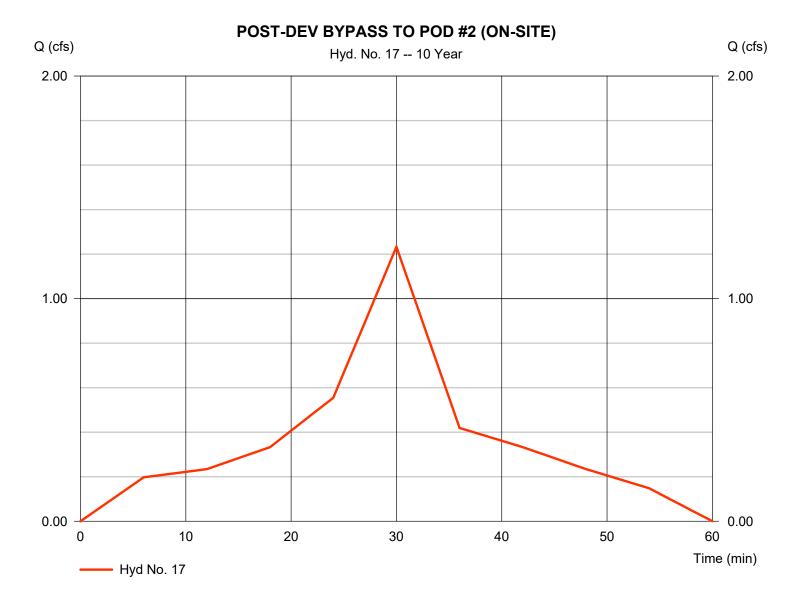
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Wednesday, 09 / 13 / 2023

Hyd. No. 17

POST-DEV BYPASS TO POD #2 (ON-SITE)

= 1.233 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 10 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 1,327 cuftRunoff coeff. Drainage area = 0.440 ac= 0.47Tc by User Intensity = 5.960 in/hr $= 6.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



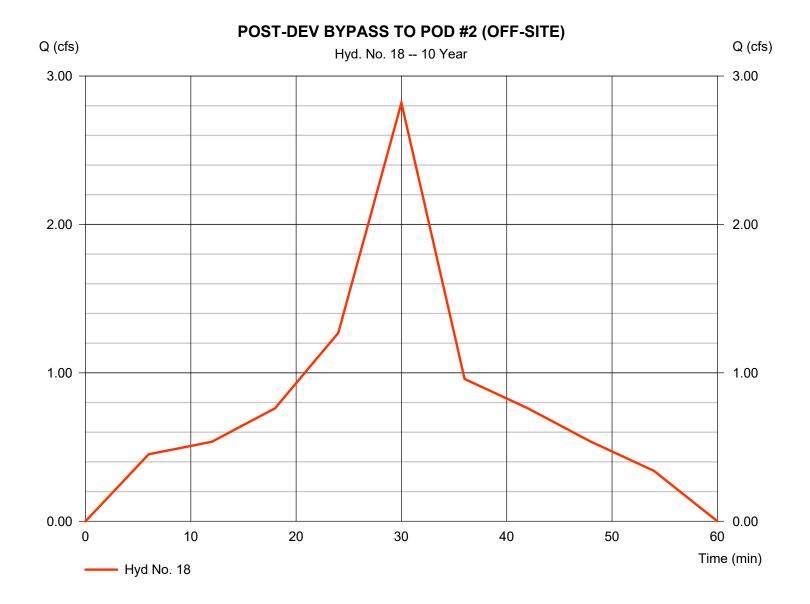
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 18

POST-DEV BYPASS TO POD #2 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 2.819 cfsStorm frequency = 10 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 3,035 cuftRunoff coeff. Drainage area = 1.100 ac= 0.43Tc by User = 6.00 min Intensity = 5.960 in/hr**IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



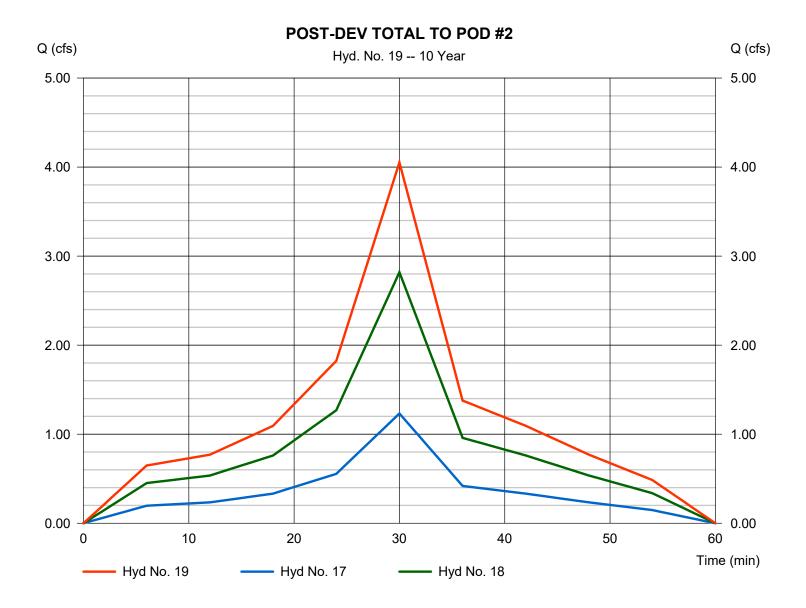
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 19

POST-DEV TOTAL TO POD #2

Hydrograph type = Combine = 4.052 cfsPeak discharge Time to peak Storm frequency = 10 yrs= 30 min Time interval = 1 min Hyd. volume = 4,361 cuftInflow hyds. = 17, 18 Contrib. drain. area = 1.540 ac



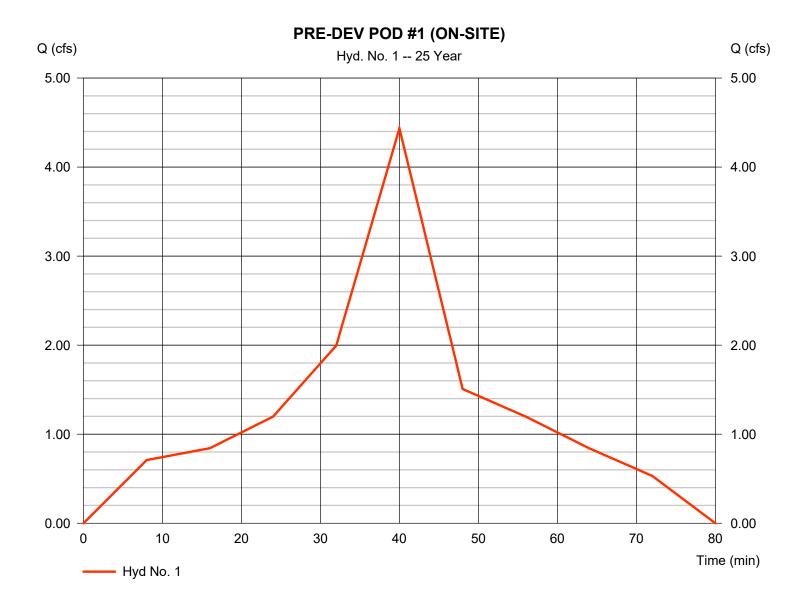
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Wednesday, 09 / 13 / 2023

Hyd. No. 1

PRE-DEV POD #1 (ON-SITE)

Hydrograph type = Dekalb Peak discharge = 4.435 cfsStorm frequency = 25 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 6,365 cuftRunoff coeff. Drainage area = 2.350 ac= 0.31Tc by User = 8.00 min Intensity = 6.088 in/hrIDF Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



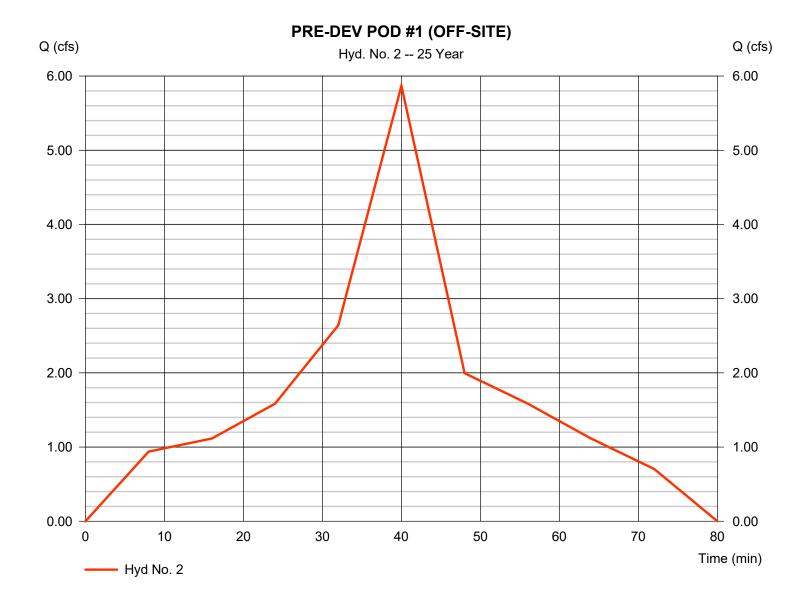
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 2

PRE-DEV POD #1 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 5.869 cfsStorm frequency = 25 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 8,423 cuft Runoff coeff. Drainage area = 2.410 ac= 0.4Tc by User Intensity = 6.088 in/hr $= 8.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



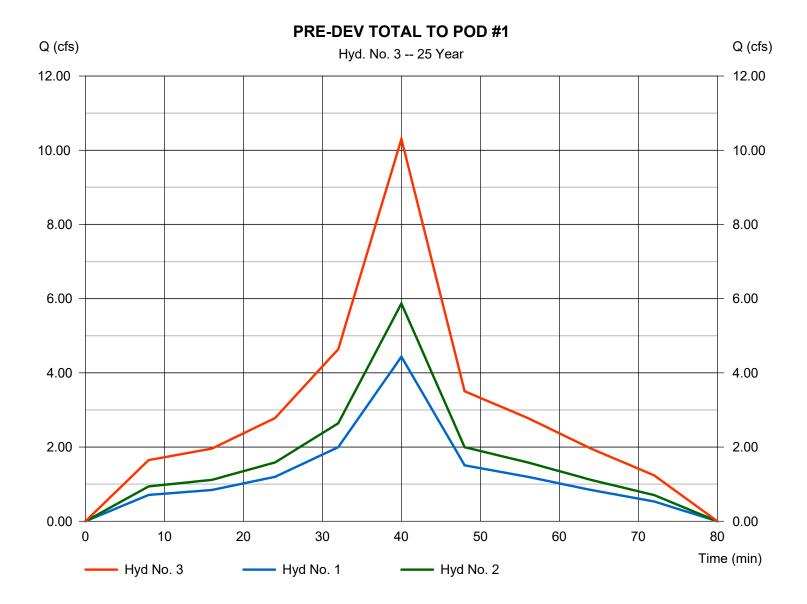
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 3

PRE-DEV TOTAL TO POD #1

Hydrograph type = Combine Peak discharge = 10.30 cfsTime to peak Storm frequency = 25 yrs= 40 min Time interval = 1 min Hyd. volume = 14,788 cuft Inflow hyds. = 1, 2 Contrib. drain. area = 4.760 ac



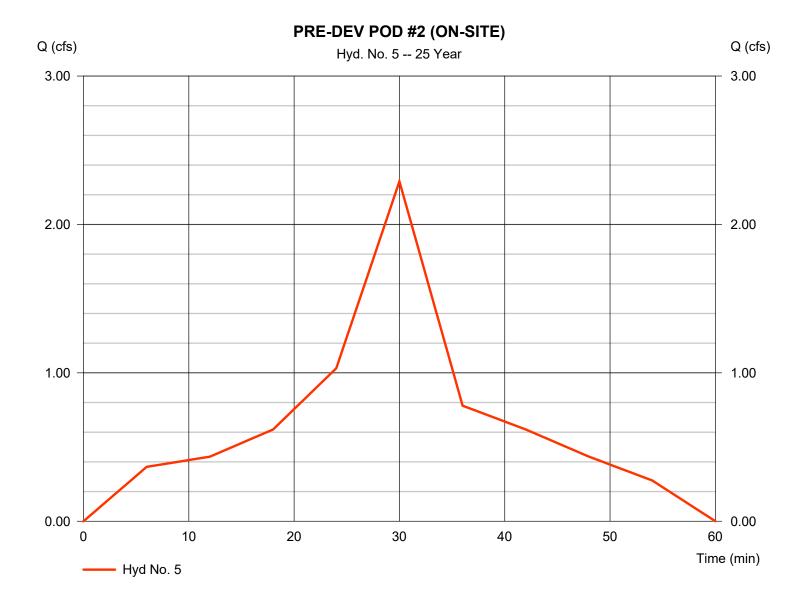
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 5

PRE-DEV POD #2 (ON-SITE)

= 2.290 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 25 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 2,465 cuftRunoff coeff. Drainage area = 1.050 ac= 0.33Tc by User = 6.00 min Intensity = 6.609 in/hr**IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



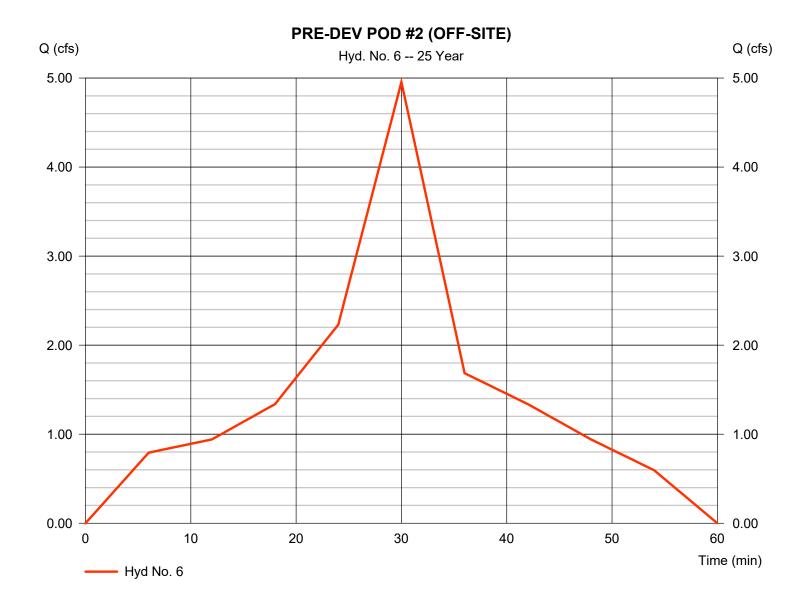
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Wednesday, 09 / 13 / 2023

Hyd. No. 6

PRE-DEV POD #2 (OFF-SITE)

= 4.955 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 25 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 5,334 cuftRunoff coeff. Drainage area = 1.630 ac= 0.46Tc by User Intensity $= 6.00 \, \text{min}$ = 6.609 in/hr**IDF** Curve = 2154-10_NOAA Intensities_HyAlsan/Revol Diffi b fact = n/a



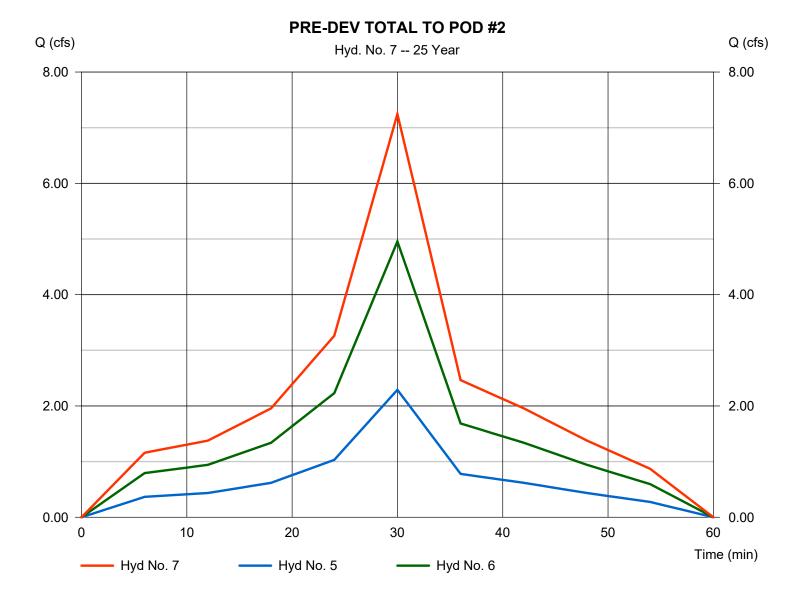
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Wednesday, 09 / 13 / 2023

Hyd. No. 7

PRE-DEV TOTAL TO POD #2

Hydrograph type = Combine Peak discharge = 7.245 cfsTime to peak Storm frequency = 25 yrs= 30 min Time interval = 1 min Hyd. volume = 7,799 cuftInflow hyds. Contrib. drain. area = 2.680 ac= 5, 6



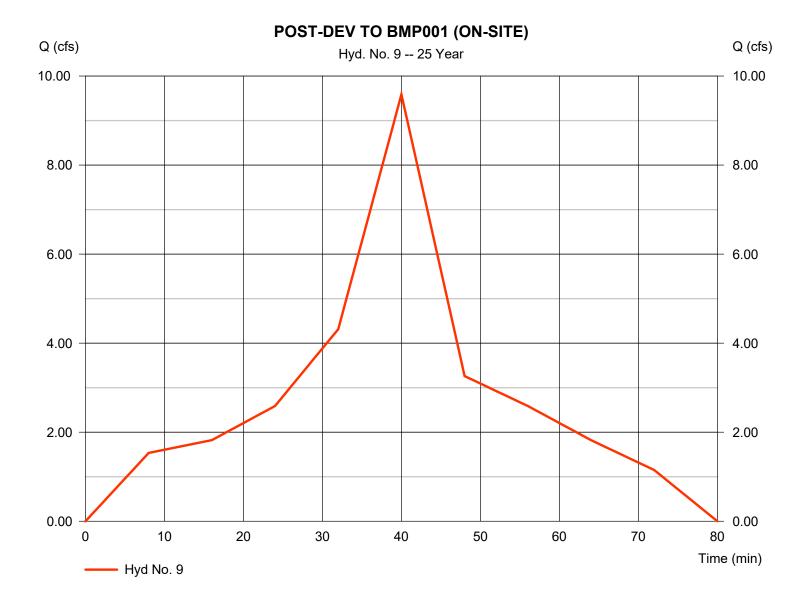
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 9

POST-DEV TO BMP001 (ON-SITE)

Peak discharge Hydrograph type = Dekalb = 9.588 cfsStorm frequency = 25 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 13,761 cuftRunoff coeff. Drainage area = 2.500 ac= 0.63Tc by User = 8.00 min Intensity = 6.088 in/hr**IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



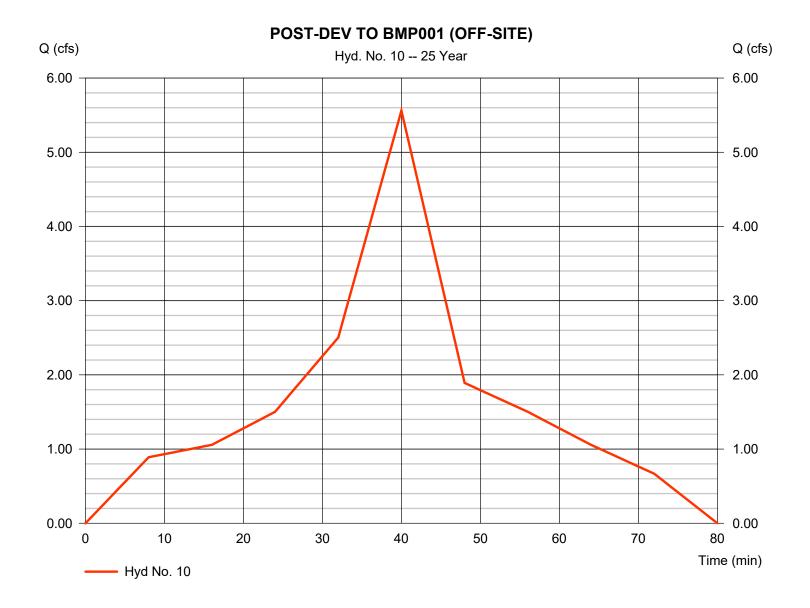
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 10

POST-DEV TO BMP001 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 5.561 cfsStorm frequency = 25 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 7,982 cuftRunoff coeff. Drainage area = 2.030 ac= 0.45Tc by User $= 8.00 \, \text{min}$ Intensity = 6.088 in/hr**IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



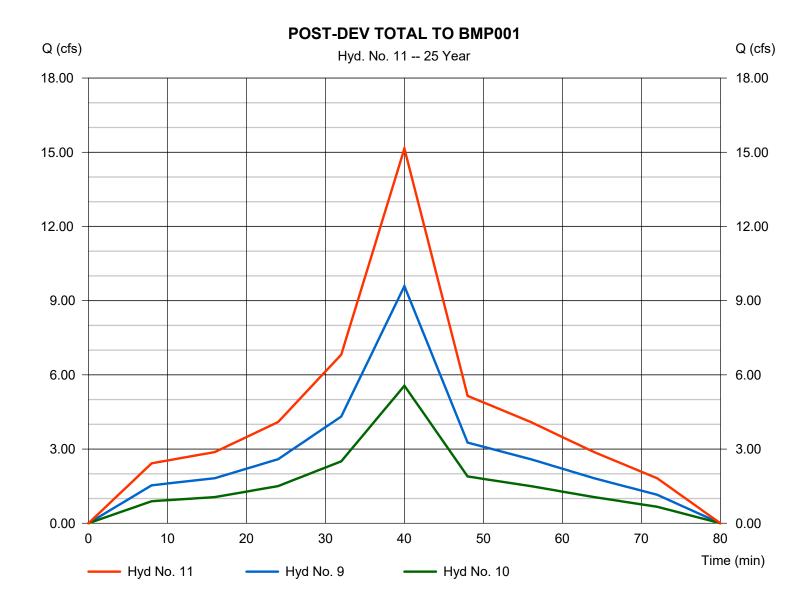
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 11

POST-DEV TOTAL TO BMP001

Hydrograph type = Combine Peak discharge = 15.15 cfsTime to peak Storm frequency = 25 yrs= 40 min Time interval = 1 min Hyd. volume = 21,743 cuft Inflow hyds. = 9, 10 Contrib. drain. area = 4.530 ac



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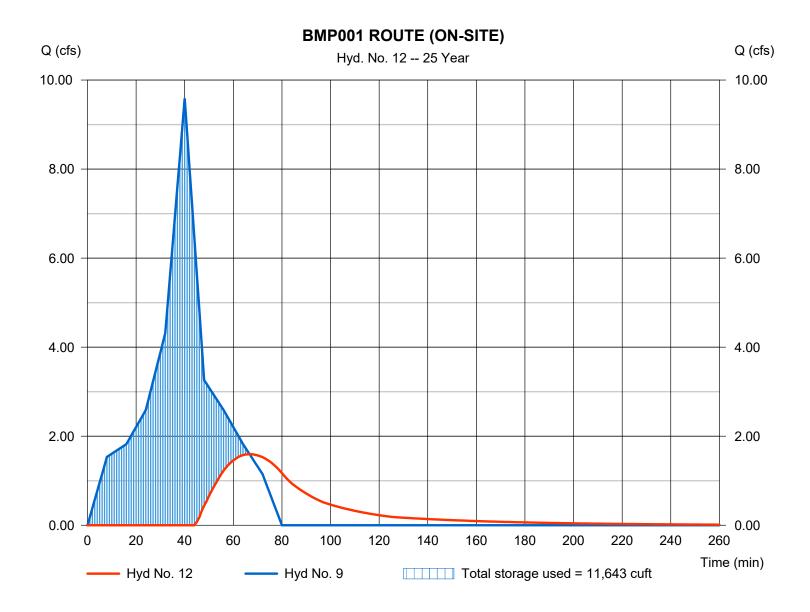
Wednesday, 09 / 13 / 2023

Hyd. No. 12

BMP001 ROUTE (ON-SITE)

Hydrograph type = Reservoir Peak discharge = 1.595 cfsStorm frequency = 25 yrsTime to peak = 67 min Time interval = 1 min Hyd. volume = 4,485 cuftInflow hyd. No. = 9 - POST-DEV TO BMP001 (O'Massi Teme) vation = 134.42 ftReservoir name = BMP 001 Max. Storage = 11,643 cuft

Storage Indication method used.



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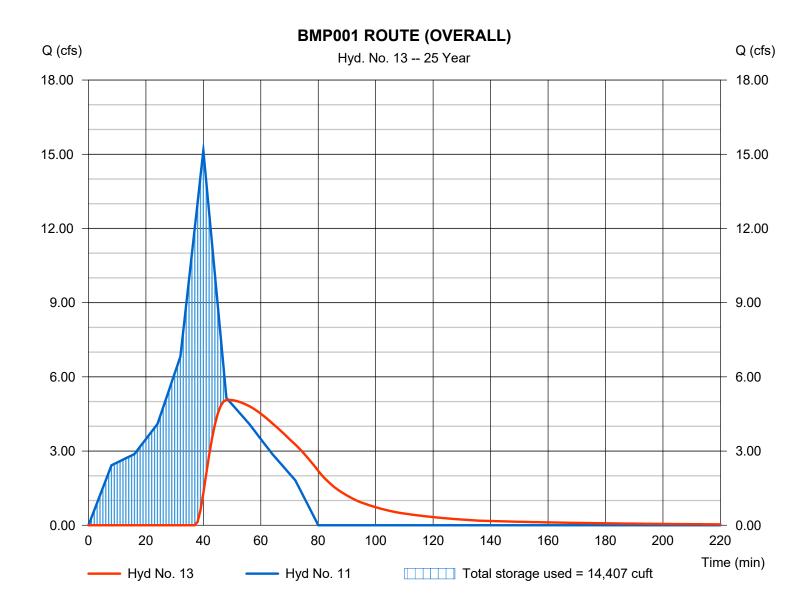
Wednesday, 09 / 13 / 2023

Hyd. No. 13

BMP001 ROUTE (OVERALL)

Hydrograph type = Reservoir Peak discharge = 5.070 cfsStorm frequency = 25 yrsTime to peak = 49 min Time interval = 1 min Hyd. volume = 12,467 cuft = 11 - POST-DEV TOTAL TO BINNPOXO1Elevation Inflow hyd. No. $= 134.91 \, \text{ft}$ Reservoir name = BMP 001 Max. Storage = 14,407 cuft

Storage Indication method used.



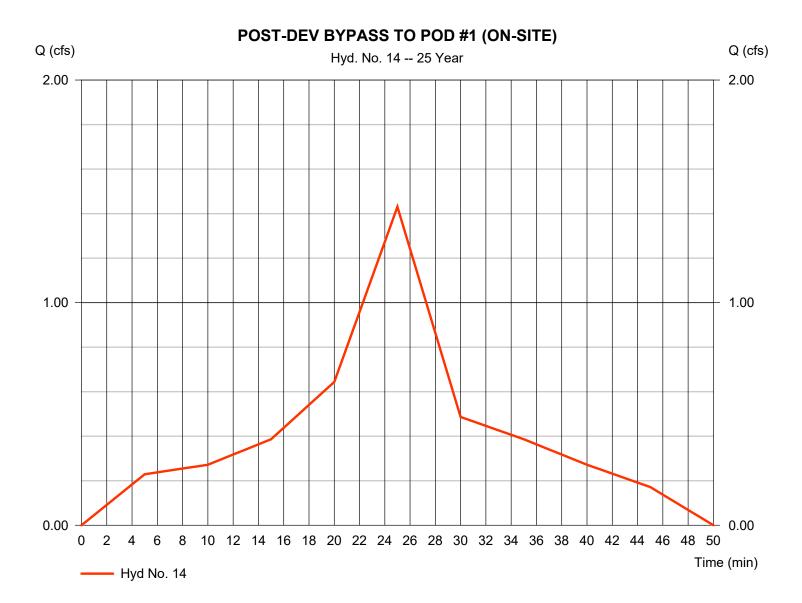
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Wednesday, 09 / 13 / 2023

Hyd. No. 14

POST-DEV BYPASS TO POD #1 (ON-SITE)

= 1.431 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 25 yrsTime to peak = 25 min Time interval = 1 min Hyd. volume = 1,283 cuftRunoff coeff. Drainage area = 0.460 ac= 0.45Tc by User $= 5.00 \, \text{min}$ Intensity = 6.912 in/hrIDF Curve = 2154-10_NOAA Intensities_HyAlsat/liRve/d DMhb fact = n/a



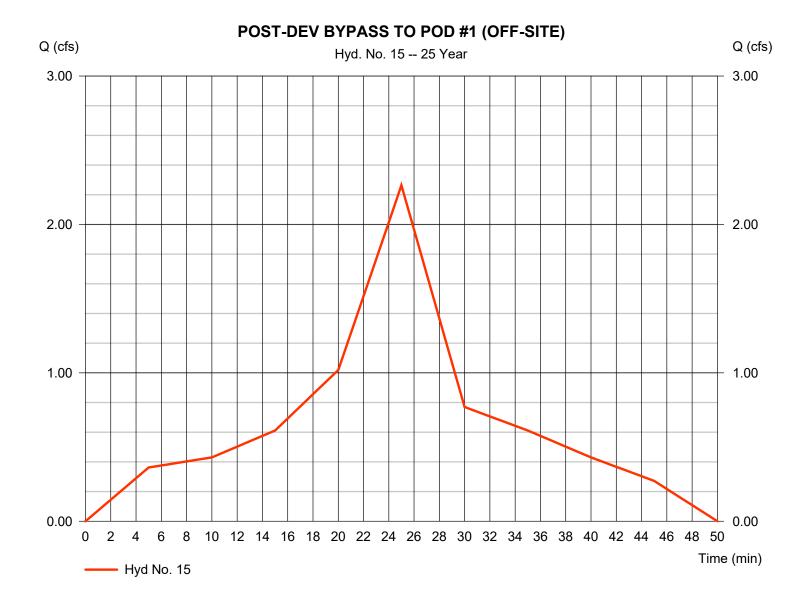
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Wednesday, 09 / 13 / 2023

Hyd. No. 15

POST-DEV BYPASS TO POD #1 (OFF-SITE)

= 2.264 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 25 yrsTime to peak = 25 min Time interval = 1 min Hyd. volume = 2,031 cuftRunoff coeff. Drainage area = 0.910 ac= 0.36Tc by User $= 5.00 \, \text{min}$ Intensity = 6.912 in/hrIDF Curve = 2154-10_NOAA Intensities_HyAlsat/liRved Dyfn fact = n/a



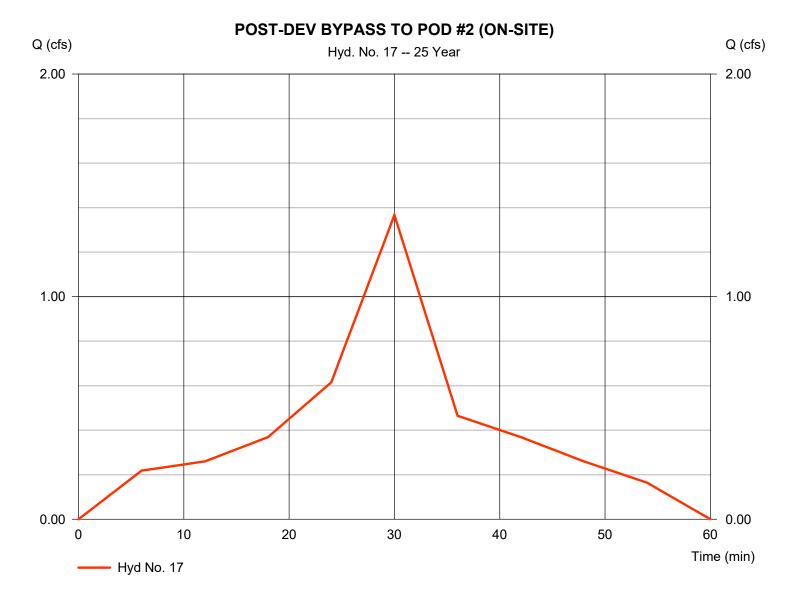
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Wednesday, 09 / 13 / 2023

Hyd. No. 17

POST-DEV BYPASS TO POD #2 (ON-SITE)

= 1.367 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 25 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 1,471 cuft Runoff coeff. Drainage area = 0.440 ac= 0.47Tc by User $= 6.00 \, \text{min}$ Intensity = 6.609 in/hr**IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



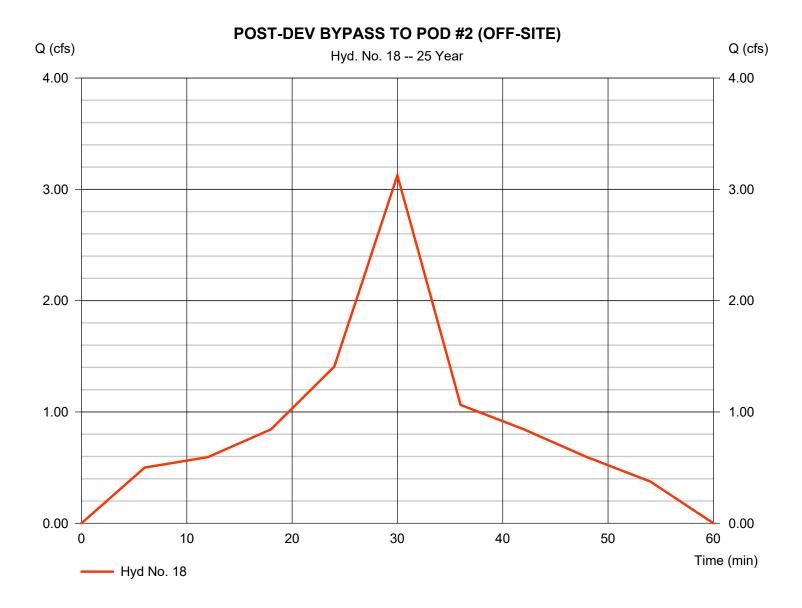
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 18

POST-DEV BYPASS TO POD #2 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 3.126 cfsStorm frequency = 25 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 3,365 cuftRunoff coeff. Drainage area = 1.100 ac= 0.43Tc by User Intensity = 6.609 in/hr $= 6.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



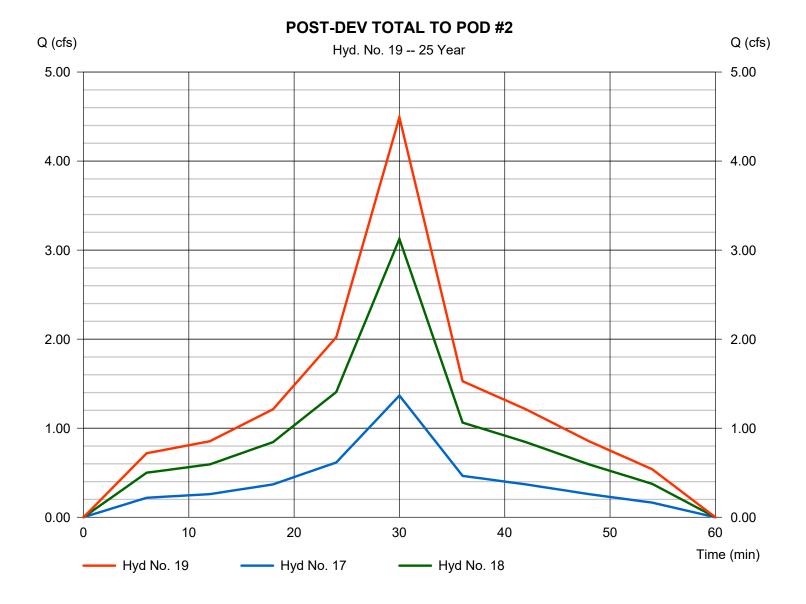
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Wednesday, 09 / 13 / 2023

Hyd. No. 19

POST-DEV TOTAL TO POD #2

Hydrograph type = Combine Peak discharge = 4.493 cfsTime to peak Storm frequency = 25 yrs= 30 min Time interval = 1 min Hyd. volume = 4,836 cuft Inflow hyds. = 17, 18 Contrib. drain. area = 1.540 ac



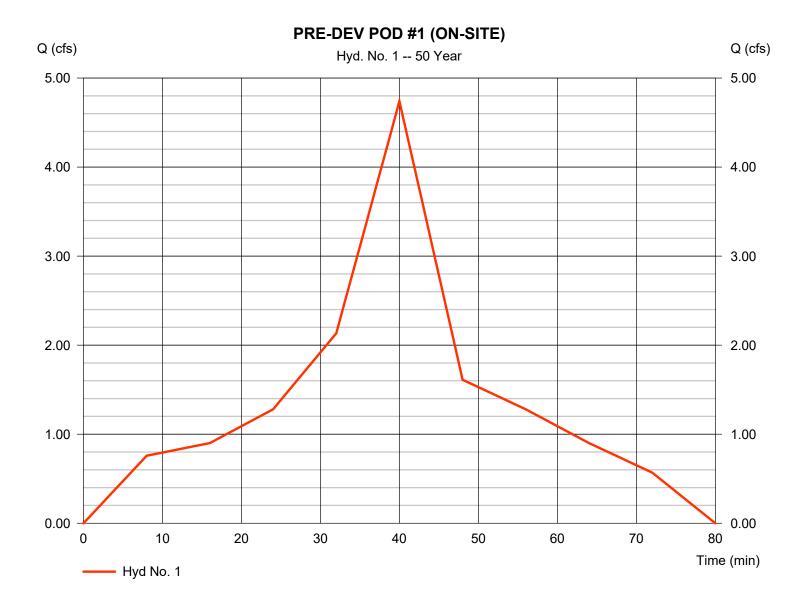
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Wednesday, 09 / 13 / 2023

Hyd. No. 1

PRE-DEV POD #1 (ON-SITE)

= 4.739 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 50 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 6,802 cuftRunoff coeff. Drainage area = 2.350 ac= 0.31Tc by User = 8.00 min Intensity = 6.505 in/hrIDF Curve = 2154-10_NOAA Intensities_HyAlsan/Revol Diffi b fact = n/a



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Wednesday, 09 / 13 / 2023

= n/a

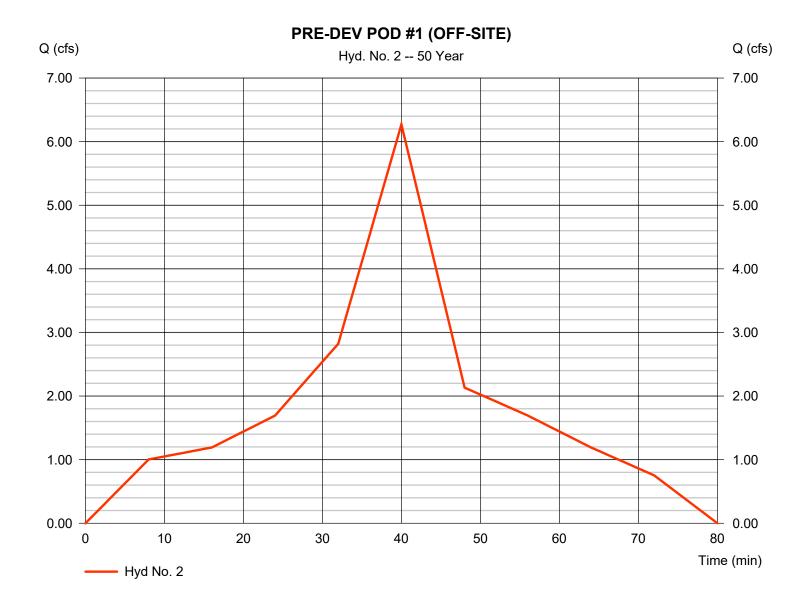
Hyd. No. 2

IDF Curve

PRE-DEV POD #1 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 6.271 cfsStorm frequency = 50 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 9,000 cuftRunoff coeff. Drainage area = 2.410 ac= 0.4Tc by User Intensity = 6.505 in/hr $= 8.00 \, \text{min}$

= 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact



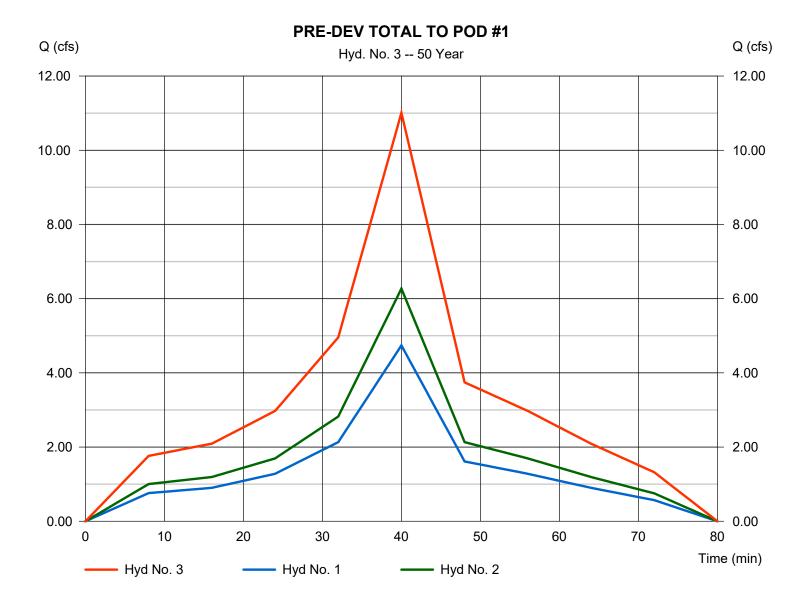
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Wednesday, 09 / 13 / 2023

Hyd. No. 3

PRE-DEV TOTAL TO POD #1

Hydrograph type = Combine Peak discharge = 11.01 cfsTime to peak Storm frequency = 50 yrs= 40 min Time interval = 1 min Hyd. volume = 15,802 cuft Inflow hyds. = 1, 2 Contrib. drain. area = 4.760 ac



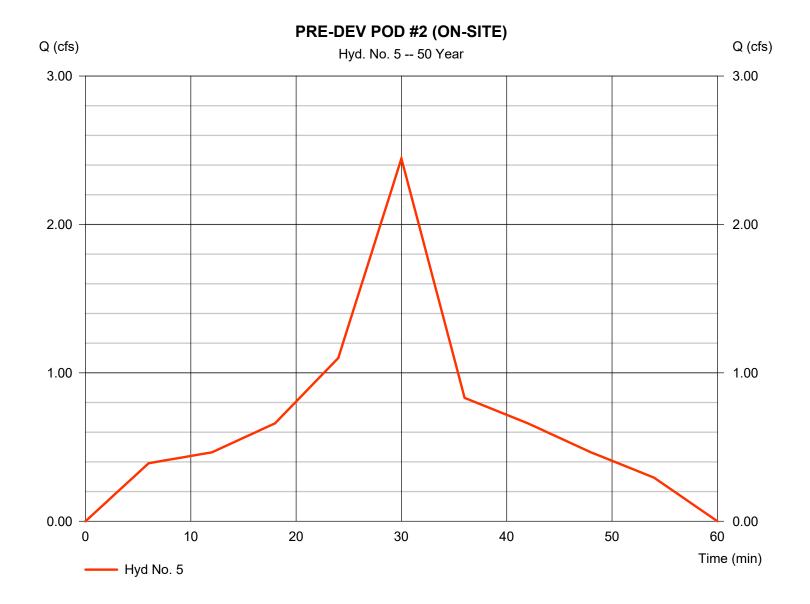
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Wednesday, 09 / 13 / 2023

Hyd. No. 5

PRE-DEV POD #2 (ON-SITE)

= 2.444 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 50 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 2,631 cuft Runoff coeff. Drainage area = 1.050 ac= 0.33Tc by User $= 6.00 \, \text{min}$ Intensity = 7.054 in/hr**IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



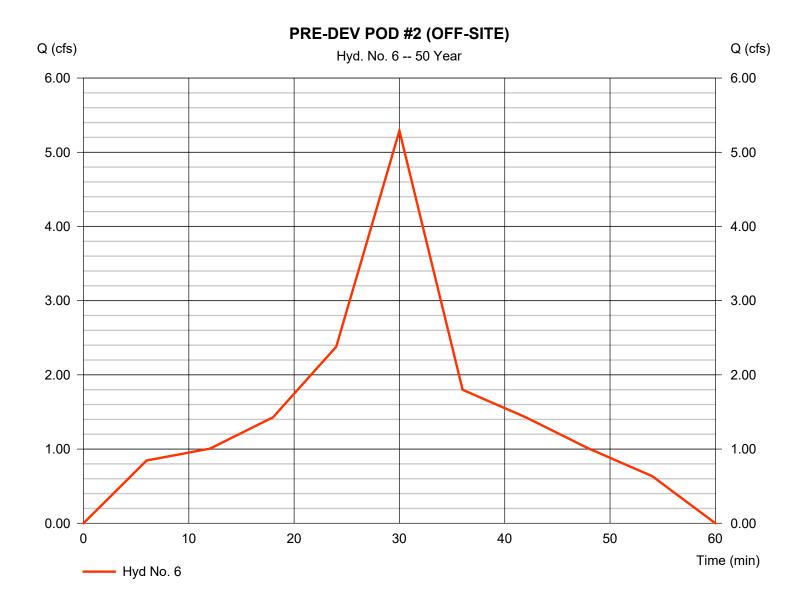
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Wednesday, 09 / 13 / 2023

Hyd. No. 6

PRE-DEV POD #2 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 5.289 cfsStorm frequency = 50 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 5,693 cuftRunoff coeff. Drainage area = 1.630 ac= 0.46= 7.054 in/hrTc by User Intensity $= 6.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



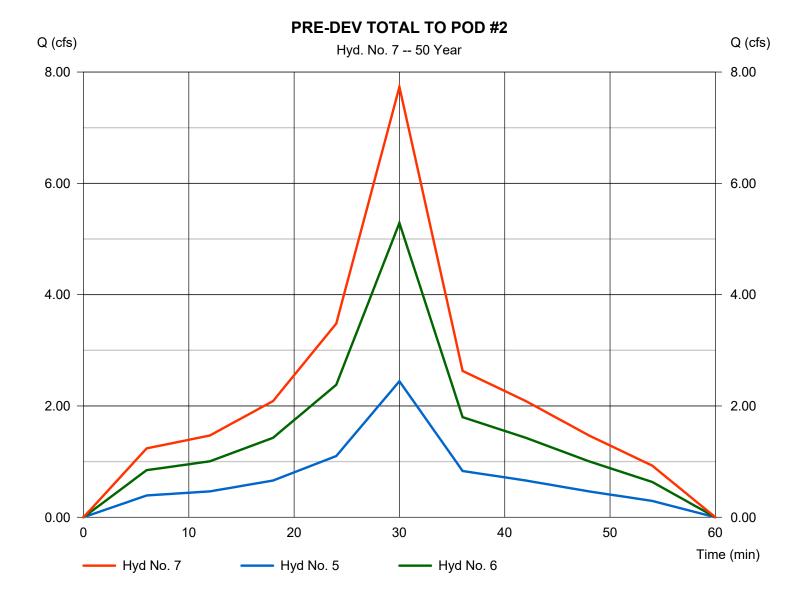
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Wednesday, 09 / 13 / 2023

Hyd. No. 7

PRE-DEV TOTAL TO POD #2

Hydrograph type = Combine Peak discharge = 7.733 cfsStorm frequency Time to peak = 50 yrs= 30 min Time interval = 1 min Hyd. volume = 8,324 cuft Inflow hyds. Contrib. drain. area = 2.680 ac= 5, 6



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Wednesday, 09 / 13 / 2023

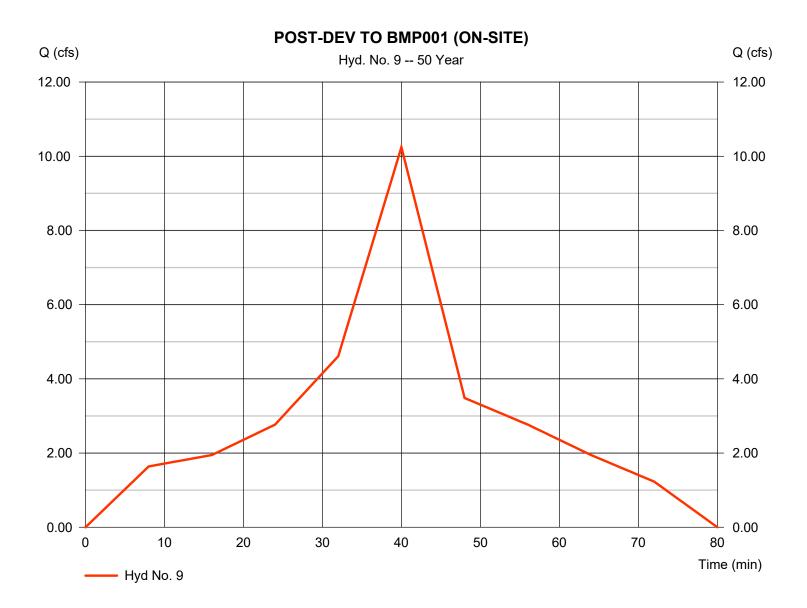
= n/a

Hyd. No. 9

IDF Curve

POST-DEV TO BMP001 (ON-SITE)

= 10.25 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 50 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 14,705 cuftRunoff coeff. Drainage area = 2.500 ac= 0.63Tc by User $= 8.00 \, \text{min}$ Intensity = 6.505 in/hr= 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact



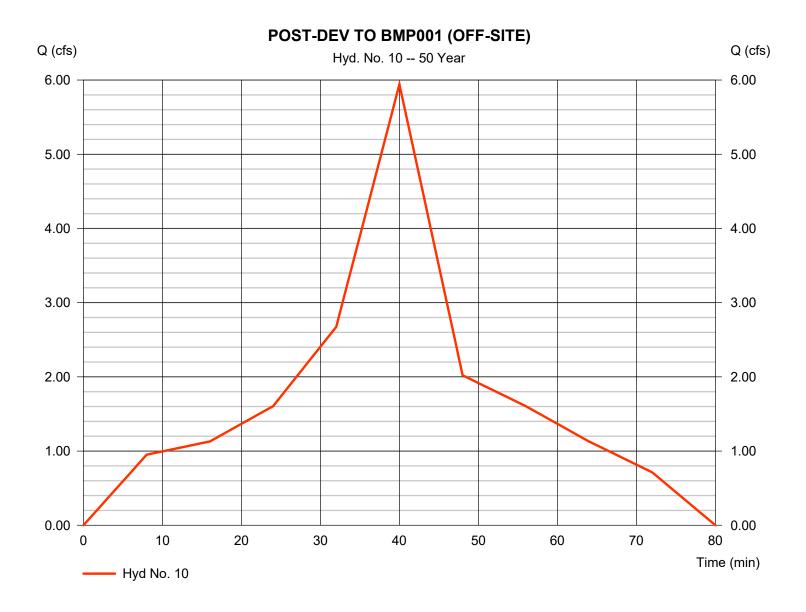
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 10

POST-DEV TO BMP001 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 5.943 cfsStorm frequency = 50 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 8,529 cuftRunoff coeff. Drainage area = 2.030 ac= 0.45Tc by User Intensity = 6.505 in/hr $= 8.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



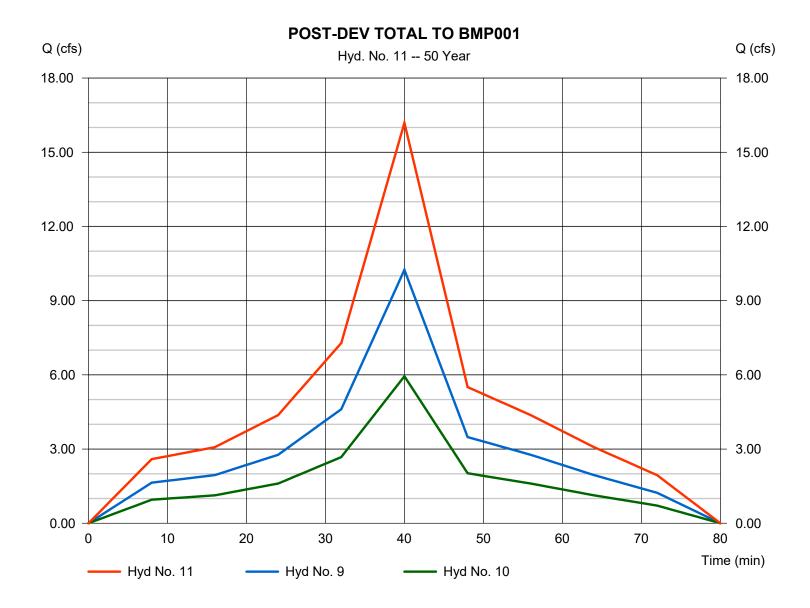
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Wednesday, 09 / 13 / 2023

Hyd. No. 11

POST-DEV TOTAL TO BMP001

Hydrograph type = Combine Peak discharge = 16.19 cfsTime to peak Storm frequency = 50 yrs= 40 min Time interval = 1 min Hyd. volume = 23,234 cuft Inflow hyds. = 9, 10 Contrib. drain. area = 4.530 ac



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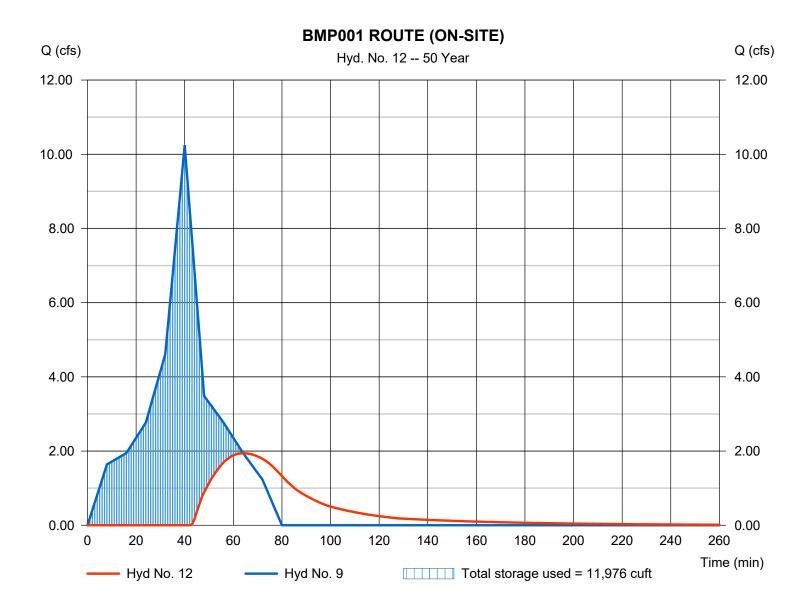
Wednesday, 09 / 13 / 2023

Hyd. No. 12

BMP001 ROUTE (ON-SITE)

Hydrograph type = Reservoir Peak discharge = 1.941 cfsStorm frequency = 50 yrsTime to peak = 64 min Time interval = 1 min Hyd. volume = 5,429 cuftInflow hyd. No. = 9 - POST-DEV TO BMP001 (OMas) Temp vation = 134.48 ftReservoir name = BMP 001 Max. Storage = 11,976 cuft

Storage Indication method used.



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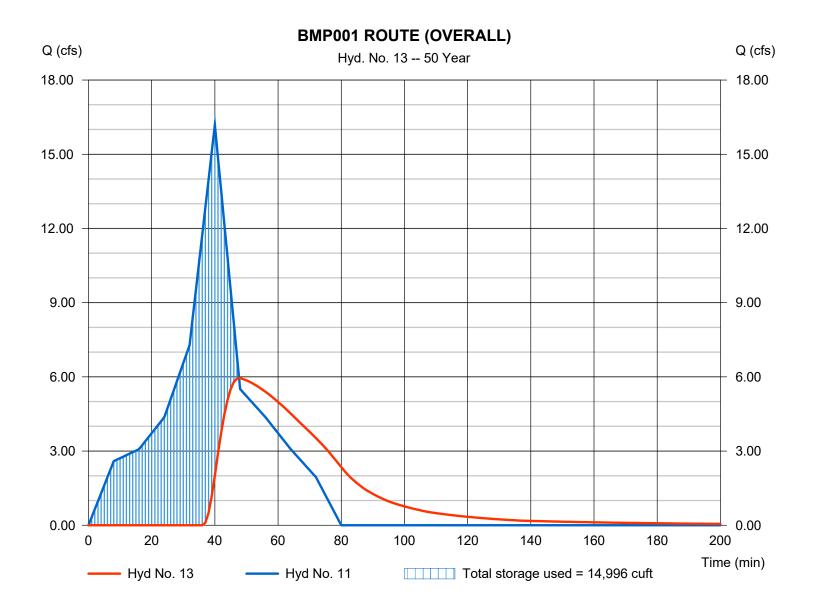
Wednesday, 09 / 13 / 2023

Hyd. No. 13

BMP001 ROUTE (OVERALL)

Hydrograph type = Reservoir Peak discharge = 5.947 cfsStorm frequency = 50 yrsTime to peak = 48 min Time interval = 1 min Hyd. volume = 13,957 cuft= 11 - POST-DEV TOTAL TO BNWP2001 Elevation Inflow hyd. No. $= 135.01 \, \text{ft}$ Reservoir name = BMP 001 Max. Storage = 14,996 cuft

Storage Indication method used.



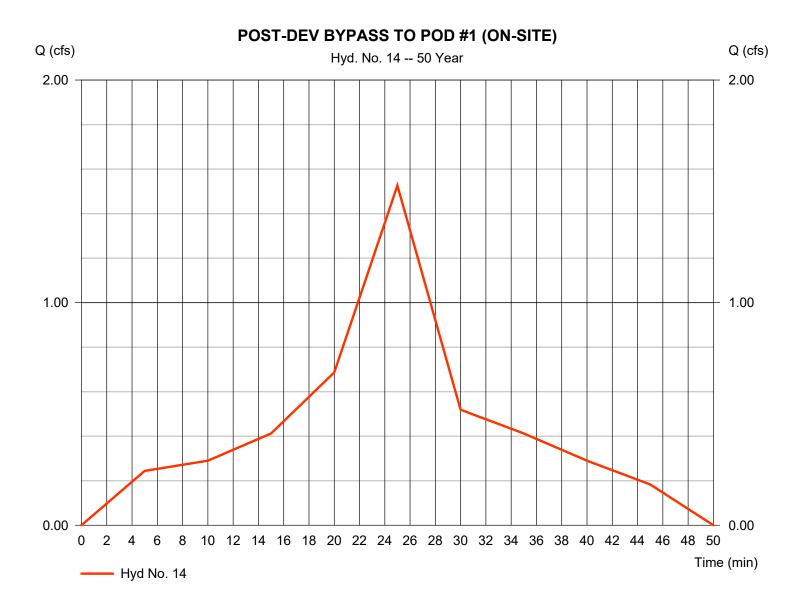
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Wednesday, 09 / 13 / 2023

Hyd. No. 14

POST-DEV BYPASS TO POD #1 (ON-SITE)

Hydrograph type = Dekalb Peak discharge = 1.526 cfsStorm frequency = 50 yrsTime to peak = 25 min Time interval = 1 min Hyd. volume = 1,369 cuftRunoff coeff. Drainage area = 0.460 ac= 0.45Tc by User $= 5.00 \, \text{min}$ Intensity = 7.373 in/hrIDF Curve = 2154-10_NOAA Intensities_HyAlsadianediane fact = n/a



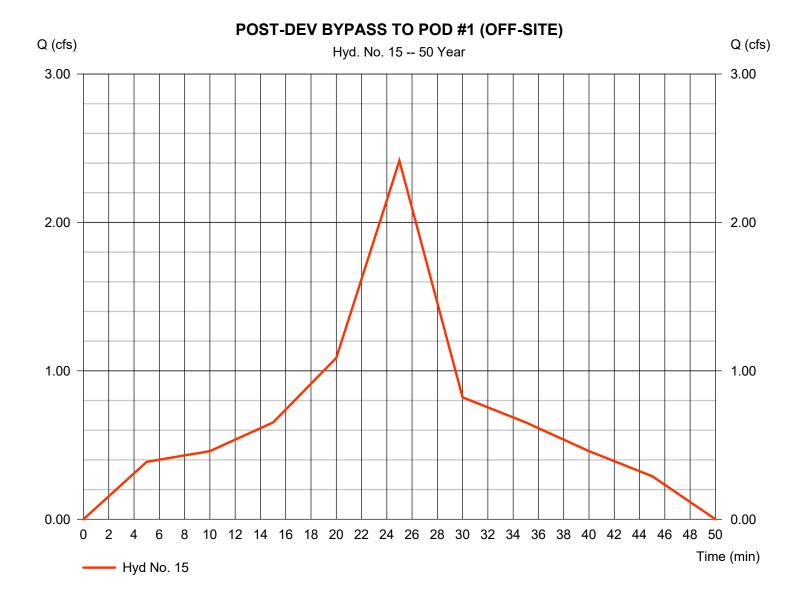
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Wednesday, 09 / 13 / 2023

Hyd. No. 15

POST-DEV BYPASS TO POD #1 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 2.416 cfsStorm frequency = 50 yrsTime to peak = 25 min Time interval = 1 min Hyd. volume = 2,167 cuftRunoff coeff. Drainage area = 0.910 ac= 0.36Tc by User $= 5.00 \, \text{min}$ Intensity = 7.373 in/hrIDF Curve = 2154-10_NOAA Intensities_HyAlsadianediane fact = n/a



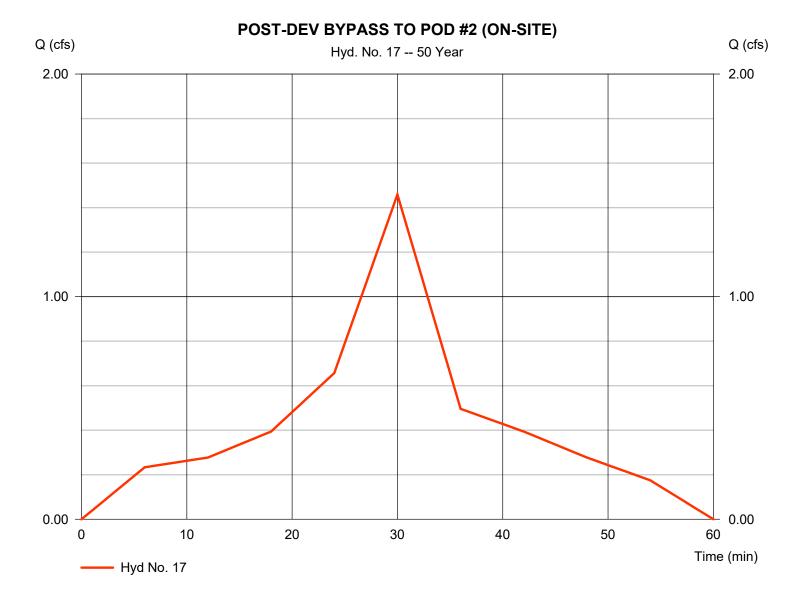
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Wednesday, 09 / 13 / 2023

Hyd. No. 17

POST-DEV BYPASS TO POD #2 (ON-SITE)

= 1.459 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 50 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 1,570 cuftRunoff coeff. Drainage area = 0.440 ac= 0.47Tc by User = 6.00 min Intensity = 7.054 in/hr**IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



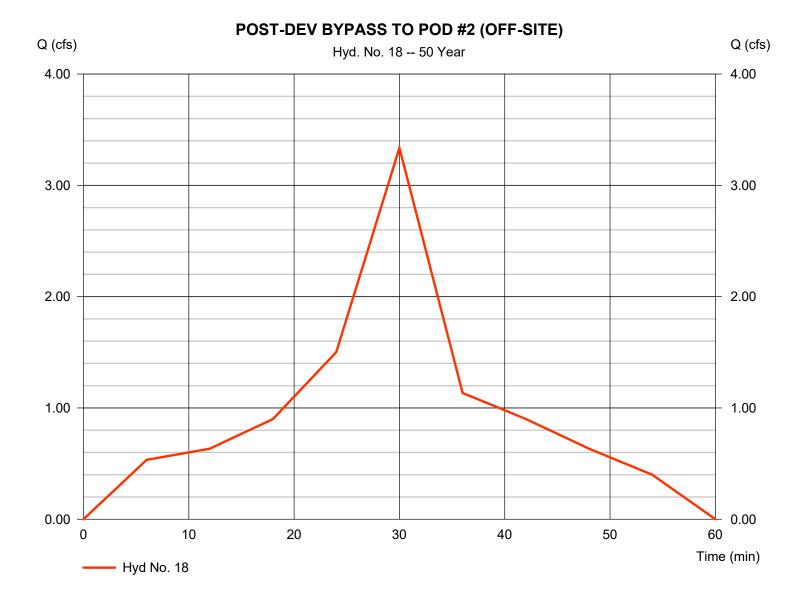
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Wednesday, 09 / 13 / 2023

Hyd. No. 18

POST-DEV BYPASS TO POD #2 (OFF-SITE)

= 3.337 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 50 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 3,591 cuftRunoff coeff. Drainage area = 1.100 ac= 0.43Tc by User Intensity = 7.054 in/hr $= 6.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



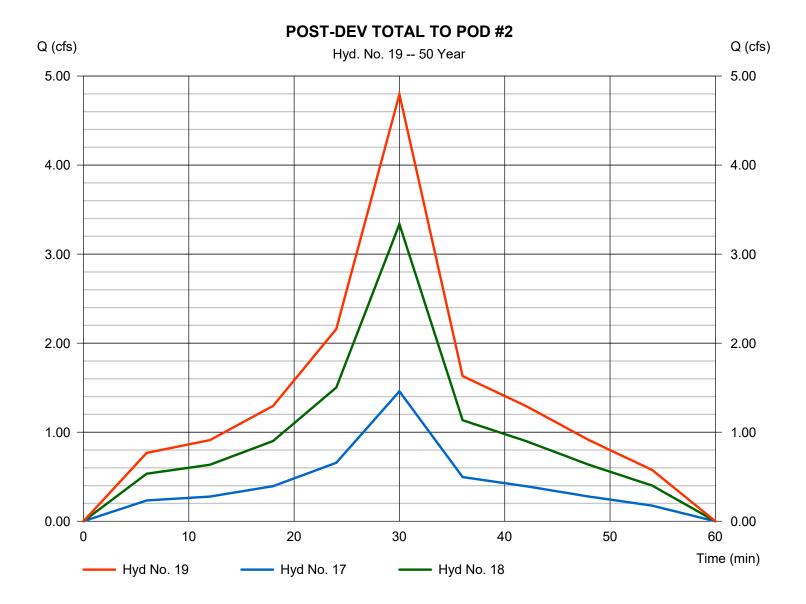
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Wednesday, 09 / 13 / 2023

Hyd. No. 19

POST-DEV TOTAL TO POD #2

Hydrograph type = Combine = 4.795 cfsPeak discharge Time to peak Storm frequency = 50 yrs= 30 min Time interval = 1 min Hyd. volume = 5,162 cuftInflow hyds. = 17, 18 Contrib. drain. area = 1.540 ac



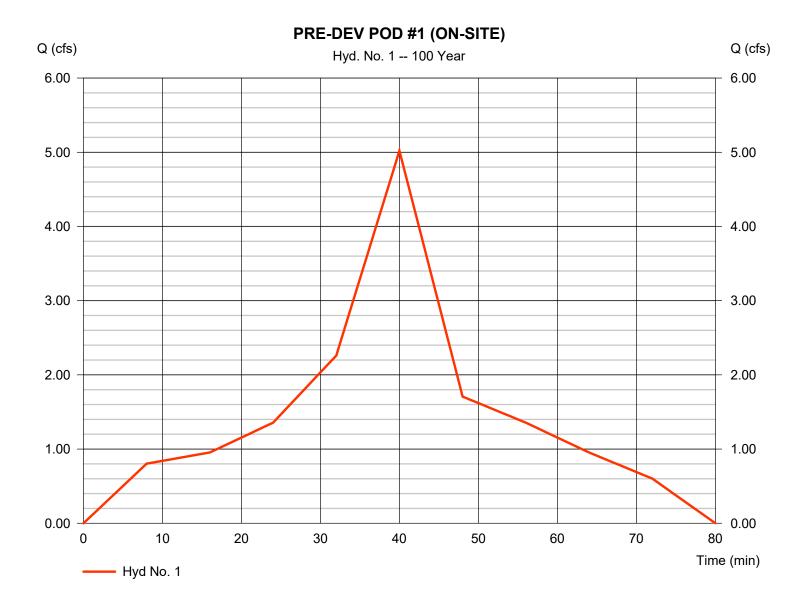
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Wednesday, 09 / 13 / 2023

Hyd. No. 1

PRE-DEV POD #1 (ON-SITE)

Hydrograph type = Dekalb Peak discharge = 5.020 cfsStorm frequency = 100 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 7,205 cuftRunoff coeff. Drainage area = 2.350 ac= 0.31Tc by User Intensity = 6.891 in/hr $= 8.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



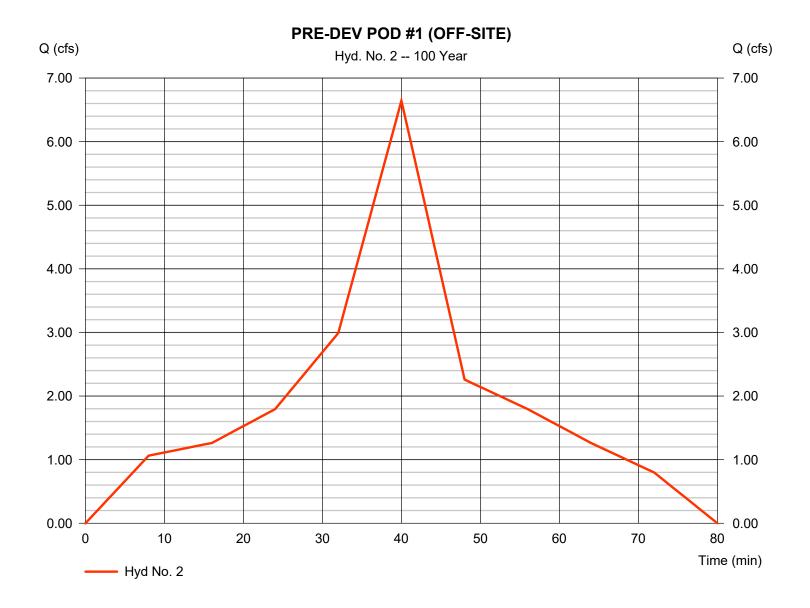
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Wednesday, 09 / 13 / 2023

Hyd. No. 2

PRE-DEV POD #1 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 6.643 cfsStorm frequency = 100 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 9,534 cuftRunoff coeff. Drainage area = 2.410 ac= 0.4Tc by User Intensity = 6.891 in/hr $= 8.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



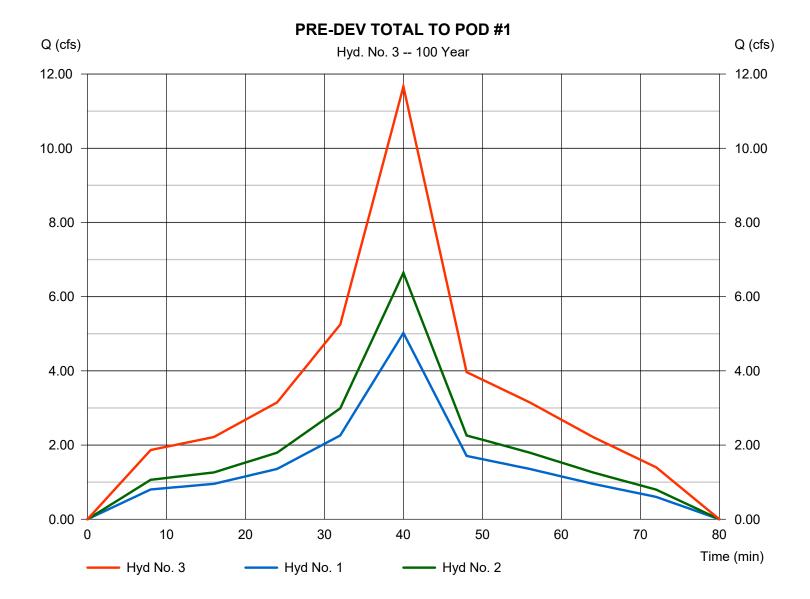
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Wednesday, 09 / 13 / 2023

Hyd. No. 3

PRE-DEV TOTAL TO POD #1

Hydrograph type = Combine Peak discharge = 11.66 cfsTime to peak Storm frequency = 100 yrs= 40 min Time interval = 1 min Hyd. volume = 16,739 cuftInflow hyds. = 1, 2 Contrib. drain. area = 4.760 ac



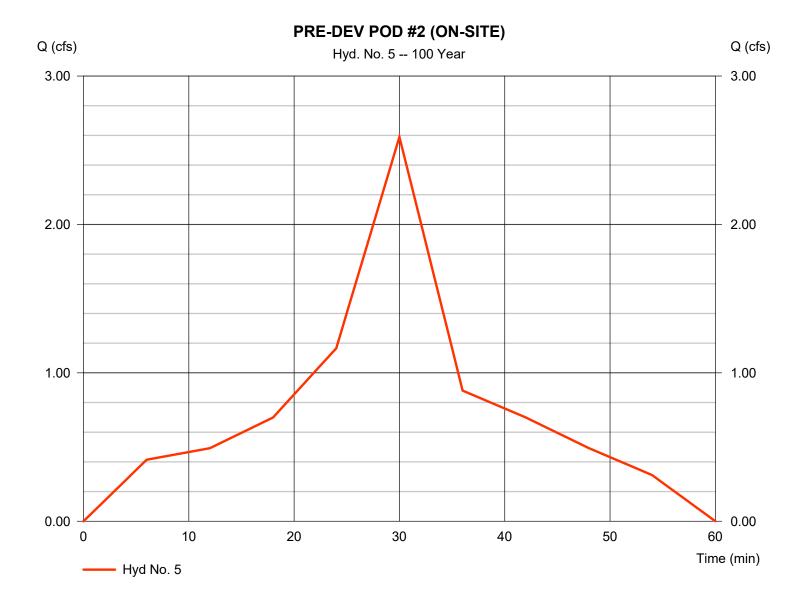
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Wednesday, 09 / 13 / 2023

Hyd. No. 5

PRE-DEV POD #2 (ON-SITE)

Hydrograph type = Dekalb Peak discharge = 2.590 cfsStorm frequency = 100 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 2,788 cuftRunoff coeff. Drainage area = 1.050 ac= 0.33Tc by User $= 6.00 \, \text{min}$ Intensity = 7.475 in/hr**IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



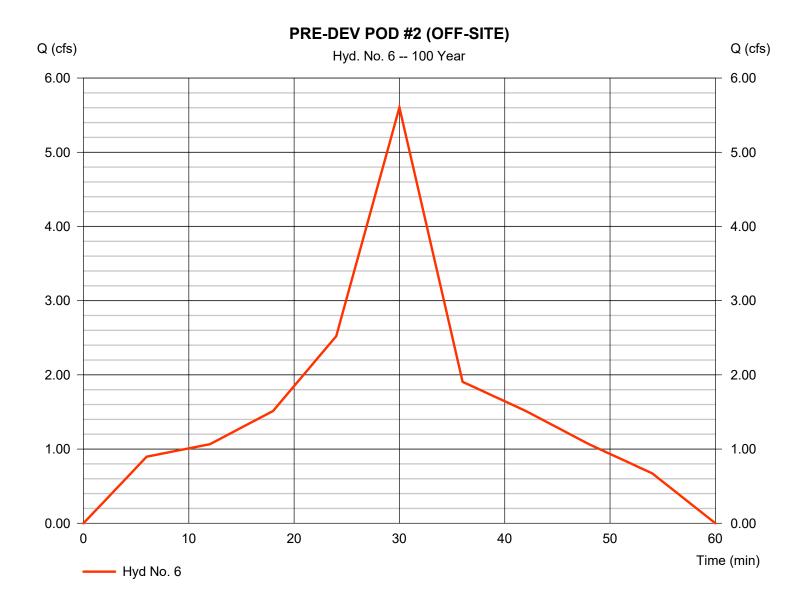
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Wednesday, 09 / 13 / 2023

Hyd. No. 6

PRE-DEV POD #2 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 5.604 cfsStorm frequency = 100 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 6,033 cuftRunoff coeff. Drainage area = 1.630 ac= 0.46Tc by User Intensity = 7.475 in/hr $= 6.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



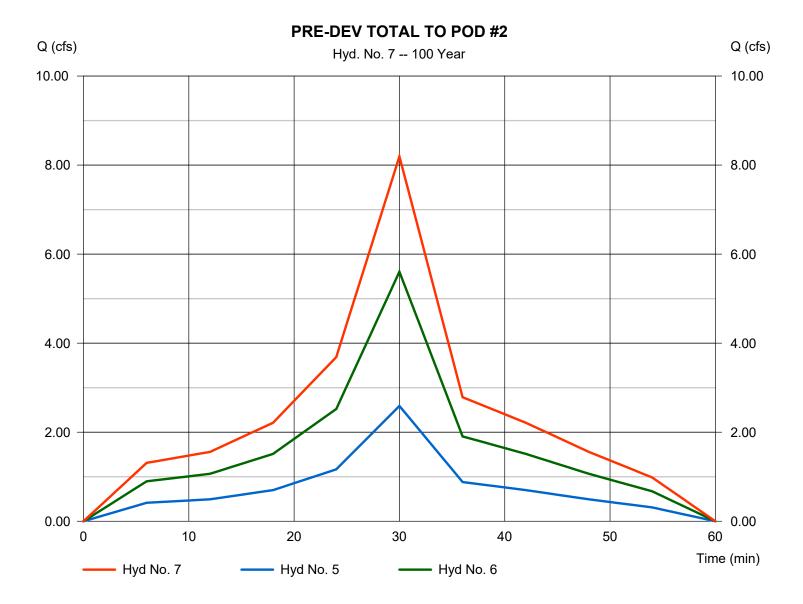
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Wednesday, 09 / 13 / 2023

Hyd. No. 7

PRE-DEV TOTAL TO POD #2

Hydrograph type = Combine Peak discharge = 8.194 cfsTime to peak Storm frequency = 100 yrs= 30 min Time interval = 1 min Hyd. volume = 8,820 cuft Inflow hyds. = 5, 6 Contrib. drain. area = 2.680 ac



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Wednesday, 09 / 13 / 2023

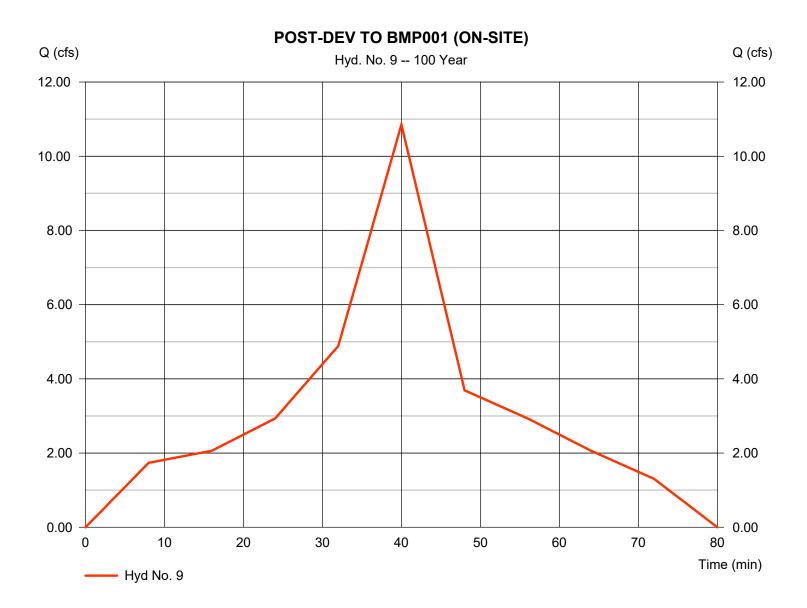
Hyd. No. 9

POST-DEV TO BMP001 (ON-SITE)

Hydrograph type= DekalbPeak discharge= 10.85 cfsStorm frequency= 100 yrsTime to peak= 40 minTime interval= 1 minHyd. volume= 15,577 cuftDrainage area= 2.500 acRunoff coeff.= 0.63

Drainage area = 2.500 ac Runoff coeff. = 0.63
Intensity = 6.891 in/hr Tc by User = 8.00 min

IDF Curve = 2154-10_NOAA Intensities_Hy&lseofl@ned Donab fact = n/a



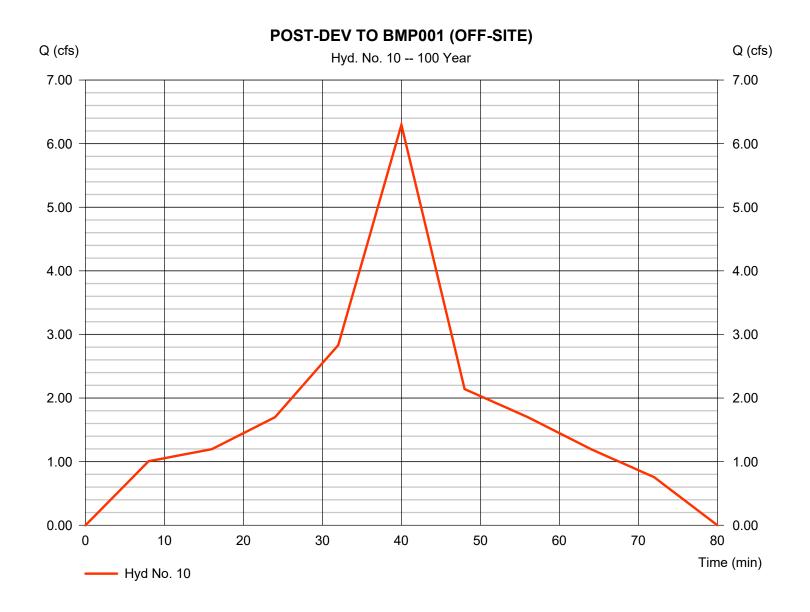
Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

Wednesday, 09 / 13 / 2023

Hyd. No. 10

POST-DEV TO BMP001 (OFF-SITE)

= 6.295 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 100 yrsTime to peak = 40 min Time interval = 1 min Hyd. volume = 9,035 cuftRunoff coeff. Drainage area = 2.030 ac= 0.45Tc by User Intensity = 6.891 in/hr $= 8.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



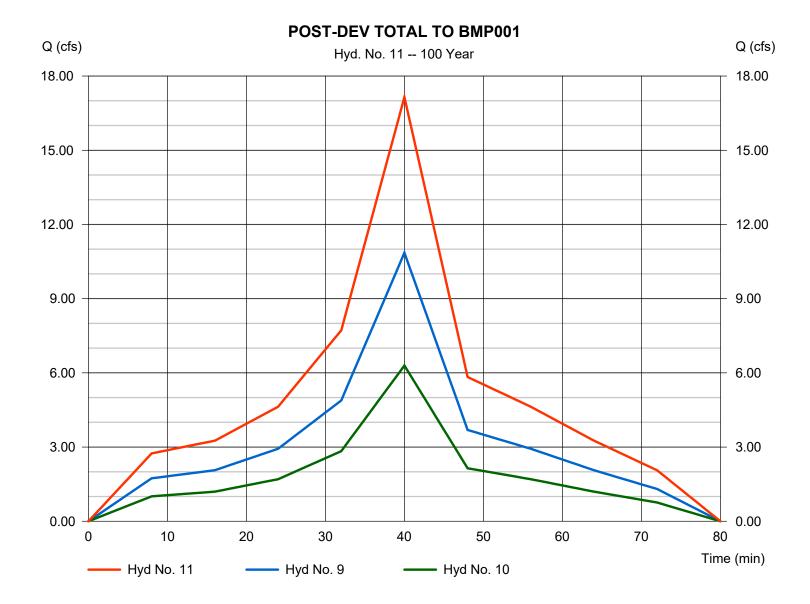
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Wednesday, 09 / 13 / 2023

Hyd. No. 11

POST-DEV TOTAL TO BMP001

Hydrograph type = Combine Peak discharge = 17.15 cfsTime to peak Storm frequency = 100 yrs= 40 min Time interval = 1 min Hyd. volume = 24,612 cuft Inflow hyds. = 9, 10 Contrib. drain. area = 4.530 ac



Hydraflow Hydrographs Extension for Autodesk® Civil 3D® by Autodesk, Inc. v2023

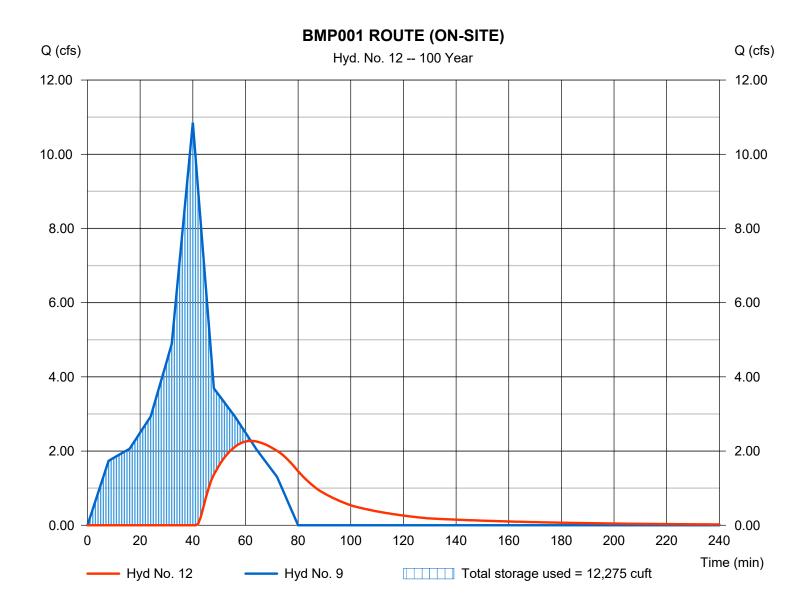
Wednesday, 09 / 13 / 2023

Hyd. No. 12

BMP001 ROUTE (ON-SITE)

Hydrograph type = Reservoir Peak discharge = 2.273 cfsStorm frequency Time to peak = 62 min = 100 yrsTime interval = 1 min Hyd. volume = 6,301 cuftInflow hyd. No. = 9 - POST-DEV TO BMP001 (OMas) Temp vation = 134.53 ftReservoir name = BMP 001 Max. Storage = 12,275 cuft

Storage Indication method used.



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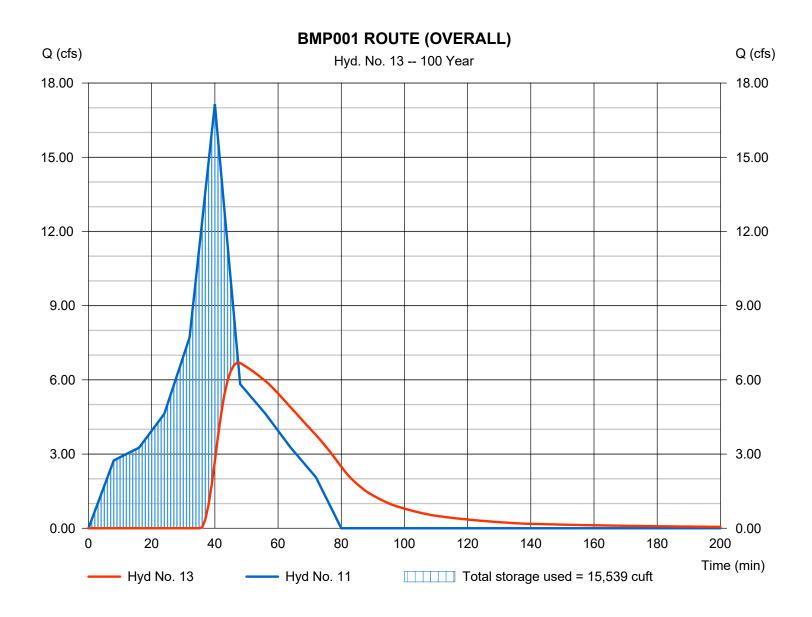
Wednesday, 09 / 13 / 2023

Hyd. No. 13

BMP001 ROUTE (OVERALL)

Hydrograph type = Reservoir Peak discharge = 6.691 cfsStorm frequency = 100 yrsTime to peak = 47 min Time interval = 1 min Hyd. volume = 15,336 cuft= 11 - POST-DEV TOTAL TO BNWP2001 Elevation Inflow hyd. No. = 135.10 ftReservoir name = BMP 001 Max. Storage = 15,539 cuft

Storage Indication method used.



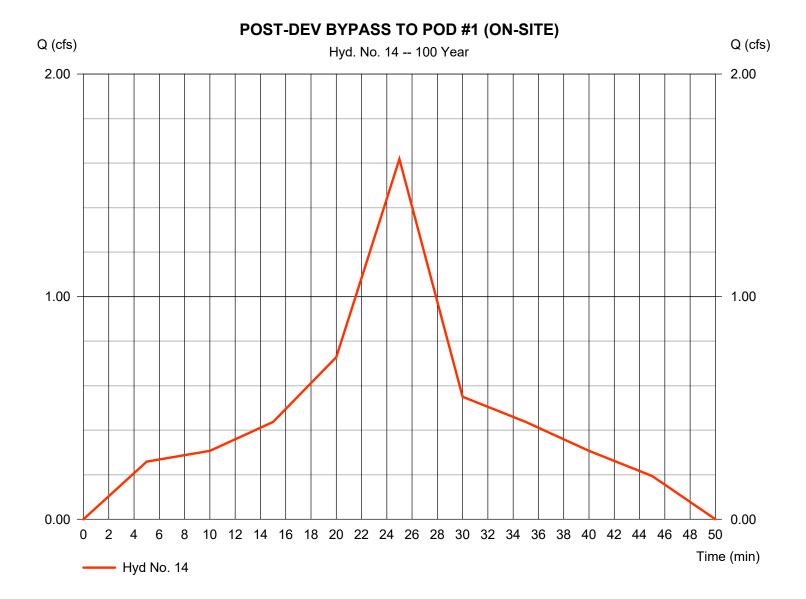
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Wednesday, 09 / 13 / 2023

Hyd. No. 14

POST-DEV BYPASS TO POD #1 (ON-SITE)

= 1.618 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 100 yrsTime to peak = 25 min Time interval = 1 min Hyd. volume = 1,451 cuftRunoff coeff. Drainage area = 0.460 ac= 0.45Tc by User $= 5.00 \, \text{min}$ Intensity = 7.817 in/hrIDF Curve = 2154-10_NOAA Intensities_HyAlsadiliRevol Diffi b fact = n/a



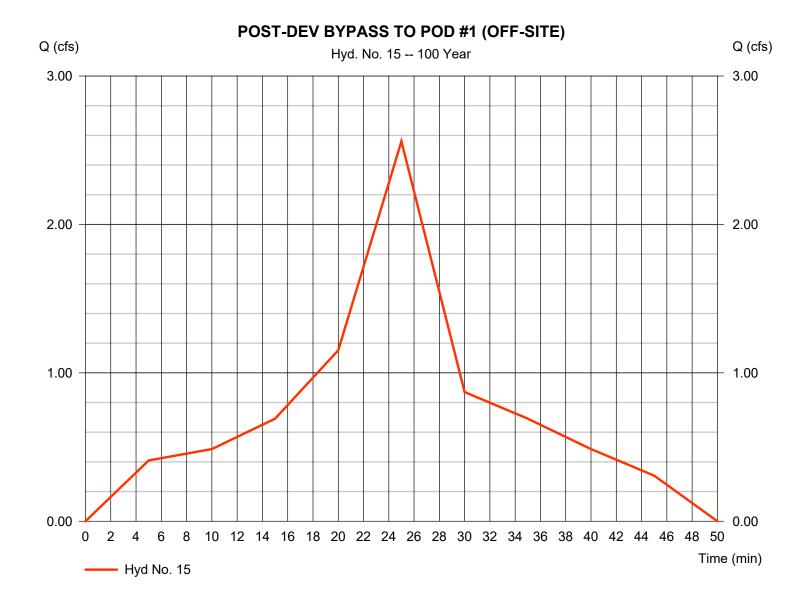
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Wednesday, 09 / 13 / 2023

Hyd. No. 15

POST-DEV BYPASS TO POD #1 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 2.561 cfsStorm frequency = 100 yrsTime to peak = 25 min Time interval = 1 min Hyd. volume = 2,297 cuftRunoff coeff. Drainage area = 0.910 ac= 0.36Tc by User Intensity = 7.817 in/hr $= 5.00 \, \text{min}$ IDF Curve = 2154-10_NOAA Intensities_HyAlsadianediane fact = n/a



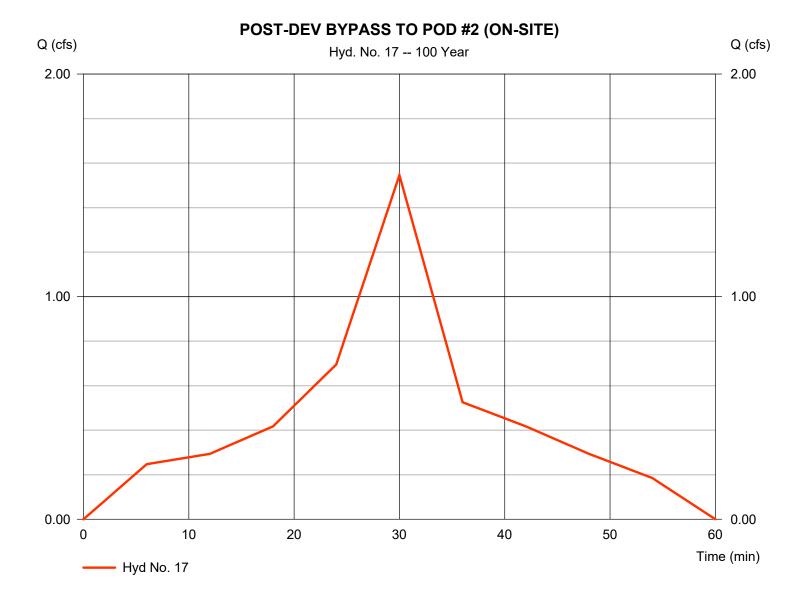
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Wednesday, 09 / 13 / 2023

Hyd. No. 17

POST-DEV BYPASS TO POD #2 (ON-SITE)

= 1.546 cfsHydrograph type = Dekalb Peak discharge Storm frequency = 100 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 1,664 cuft Runoff coeff. Drainage area = 0.440 ac= 0.47Tc by User $= 6.00 \, \text{min}$ Intensity = 7.475 in/hr**IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



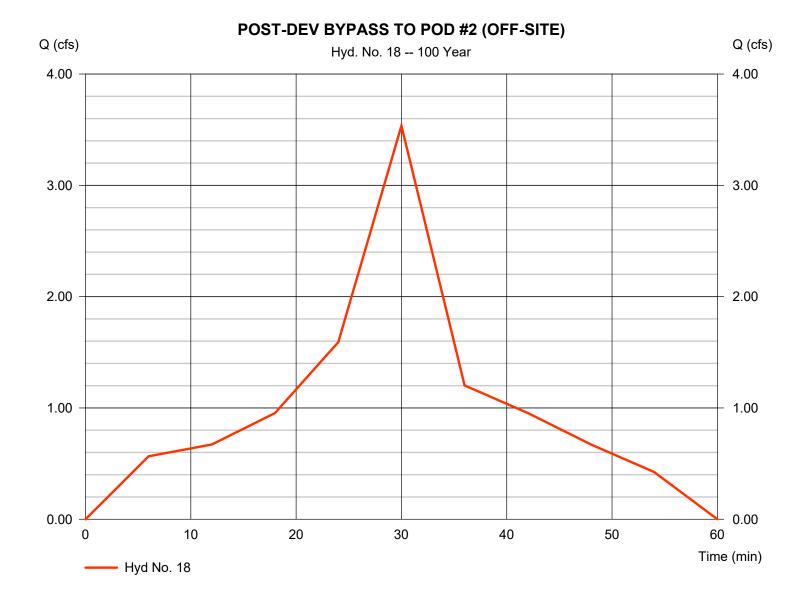
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Wednesday, 09 / 13 / 2023

Hyd. No. 18

POST-DEV BYPASS TO POD #2 (OFF-SITE)

Hydrograph type = Dekalb Peak discharge = 3.535 cfsStorm frequency = 100 yrsTime to peak = 30 min Time interval = 1 min Hyd. volume = 3,806 cuftRunoff coeff. Drainage area = 1.100 ac= 0.43Tc by User Intensity = 7.475 in/hr $= 6.00 \, \text{min}$ **IDF** Curve = 2154-10_NOAA Intensities_Hy&lsat/likevol Dnn b fact = n/a



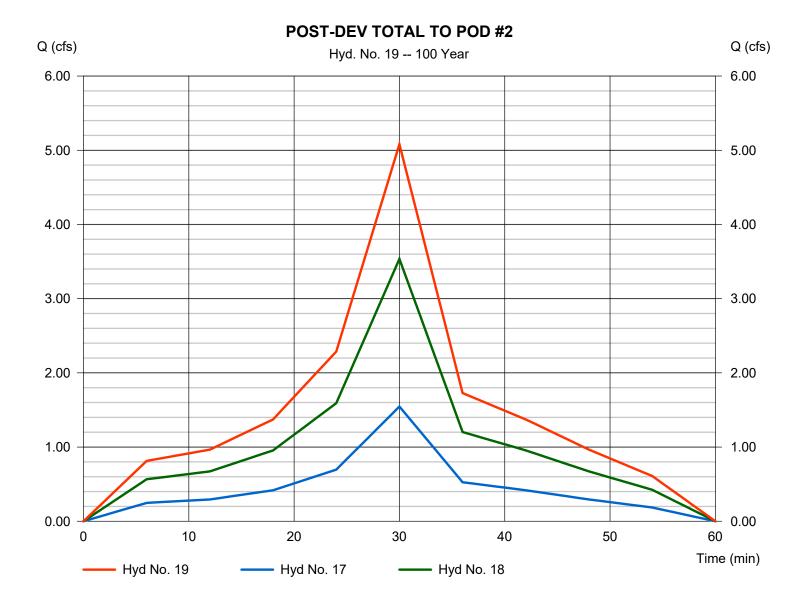
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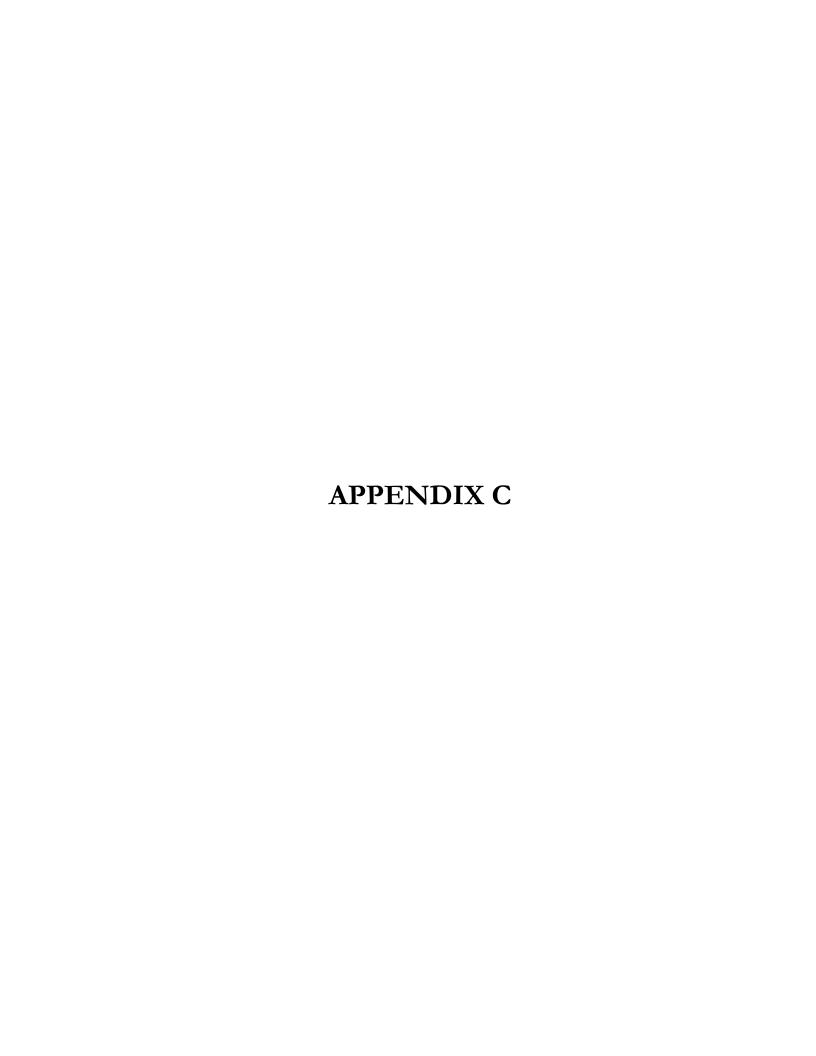
Wednesday, 09 / 13 / 2023

Hyd. No. 19

POST-DEV TOTAL TO POD #2

Hydrograph type = Combine Peak discharge = 5.081 cfsTime to peak Storm frequency = 100 yrs= 30 min Time interval = 1 min Hyd. volume = 5,469 cuftInflow hyds. = 17, 18 Contrib. drain. area = 1.540 ac







NOAA Atlas 14, Volume 2, Version 3 Location name: Elkins Park, Pennsylvania, USA* Latitude: 40.0697°, Longitude: -75.1172° Elevation: 147.23 ft**

* source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M.Yekta, and D. Riley NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

PDS	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) ¹									
Duration				Avera	ge recurren	ce interval (years)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.346 (0.316-0.380)	0.413 (0.376-0.453)	0.487 (0.443-0.534)	0.541 (0.491-0.593)	0.606 (0.548-0.664)	0.652 (0.586-0.715)	0.698 (0.624-0.767)	0.739 (0.657-0.815)	0.789 (0.695-0.875)	0.827 (0.722-0.922)
10-min	0.553 (0.505-0.607)	0.660 (0.602-0.724)	0.780 (0.710-0.855)	0.865 (0.786-0.948)	0.966 (0.873-1.06)	1.04 (0.933-1.14)	1.11 (0.992-1.22)	1.17 (1.04-1.29)	1.25 (1.10-1.38)	1.30 (1.14-1.45)
15-min	0.691 (0.631-0.758)	0.830 (0.756-0.910)	0.987 (0.898-1.08)	1.09 (0.994-1.20)	1.23 (1.11-1.34)	1.32 (1.18-1.44)	1.40 (1.25-1.54)	1.48 (1.31-1.63)	1.57 (1.38-1.74)	1.63 (1.43-1.82)
30-min	0.947 (0.865-1.04)	1.15 (1.05-1.26)	1.40 (1.27-1.54)	1.59 (1.44-1.74)	1.81 (1.64-1.99)	1.98 (1.78-2.17)	2.15 (1.92-2.36)	2.30 (2.05-2.54)	2.50 (2.20-2.77)	2.65 (2.31-2.95)
60-min	1.18 (1.08-1.30)	1.44 (1.31-1.58)	1.80 (1.64-1.97)	2.07 (1.88-2.26)	2.42 (2.18-2.65)	2.68 (2.41-2.94)	2.96 (2.65-3.25)	3.23 (2.87-3.56)	3.59 (3.16-3.98)	3.86 (3.38-4.31)
2-hr	1.42 (1.29-1.57)	1.73 (1.57-1.90)	2.17 (1.97-2.39)	2.51 (2.27-2.75)	2.96 (2.66-3.25)	3.33 (2.97-3.65)	3.69 (3.27-4.06)	4.06 (3.58-4.48)	4.57 (3.97-5.07)	4.97 (4.28-5.54)
3-hr	1.56 (1.41-1.72)	1.89 (1.72-2.09)	2.38 (2.15-2.62)	2.76 (2.49-3.04)	3.28 (2.94-3.61)	3.69 (3.29-4.06)	4.12 (3.65-4.55)	4.55 (4.00-5.04)	5.16 (4.46-5.74)	5.64 (4.82-6.30)
6-hr	1.95 (1.77-2.16)	2.36 (2.15-2.61)	2.96 (2.68-3.27)	3.44 (3.11-3.79)	4.13 (3.70-4.56)	4.70 (4.18-5.18)	5.30 (4.67-5.86)	5.95 (5.18-6.58)	6.86 (5.87-7.65)	7.61 (6.41-8.53)
12-hr	2.37 (2.17-2.63)	2.87 (2.62-3.17)	3.62 (3.30-4.00)	4.25 (3.86-4.69)	5.18 (4.65-5.71)	5.97 (5.31-6.58)	6.84 (6.00-7.56)	7.79 (6.73-8.65)	9.20 (7.76-10.3)	10.4 (8.61-11.7)
24-hr	2.74 (2.53-2.97)	3.30 (3.05-3.59)	4.18 (3.86-4.53)	4.91 (4.52-5.32)	5.98 (5.48-6.47)	6.90 (6.27-7.45)	7.90 (7.13-8.53)	8.99 (8.04-9.70)	10.6 (9.35-11.5)	12.0 (10.4-13.0)
2-day	3.15 (2.90-3.43)	3.81 (3.51-4.14)	4.82 (4.43-5.24)	5.66 (5.19-6.14)	6.86 (6.26-7.43)	7.87 (7.15-8.53)	8.96 (8.08-9.70)	10.1 (9.06-11.0)	11.8 (10.5-12.9)	13.3 (11.6-14.4)
3-day	3.33 (3.08-3.62)	4.02 (3.72-4.37)	5.07 (4.68-5.50)	5.92 (5.46-6.42)	7.15 (6.56-7.73)	8.18 (7.46-8.84)	9.27 (8.41-10.0)	10.4 (9.41-11.3)	12.1 (10.8-13.2)	13.6 (12.0-14.7)
4-day	3.51 (3.26-3.81)	4.24 (3.93-4.59)	5.31 (4.92-5.75)	6.19 (5.73-6.69)	7.44 (6.85-8.04)	8.48 (7.78-9.15)	9.59 (8.74-10.3)	10.8 (9.76-11.6)	12.5 (11.2-13.5)	13.8 (12.3-15.0)
7-day	4.10 (3.82-4.43)	4.92 (4.59-5.31)	6.10 (5.68-6.59)	7.07 (6.57-7.62)	8.47 (7.83-9.12)	9.62 (8.86-10.4)	10.9 (9.94-11.7)	12.2 (11.1-13.1)	14.1 (12.7-15.1)	15.6 (13.9-16.8)
10-day	4.67 (4.37-5.00)	5.58 (5.22-5.98)	6.82 (6.37-7.31)	7.82 (7.29-8.38)	9.22 (8.57-9.87)	10.3 (9.58-11.1)	11.5 (10.6-12.3)	12.8 (11.7-13.7)	14.5 (13.2-15.5)	15.9 (14.4-17.1)
20-day	6.31 (5.96-6.69)	7.49 (7.08-7.95)	8.95 (8.46-9.50)	10.1 (9.53-10.7)	11.7 (11.0-12.4)	12.9 (12.1-13.6)	14.1 (13.2-15.0)	15.4 (14.3-16.3)	17.1 (15.8-18.1)	18.4 (16.9-19.6)
30-day	7.86 (7.46-8.27)	9.27 (8.79-9.75)	10.8 (10.3-11.4)	12.0 (11.4-12.7)	13.6 (12.9-14.4)	14.9 (14.0-15.6)	16.1 (15.1-16.9)	17.3 (16.2-18.2)	18.8 (17.6-19.9)	20.0 (18.6-21.1)
45-day	10.0 (9.53-10.5)	11.8 (11.2-12.3)	13.5 (12.9-14.2)	14.9 (14.2-15.6)	16.6 (15.8-17.4)	17.9 (17.0-18.7)	19.1 (18.1-20.0)	20.2 (19.1-21.2)	21.7 (20.4-22.8)	22.7 (21.3-23.9)
60-day	12.0 (11.4-12.6)	14.0 (13.4-14.7)	16.0 (15.3-16.8)	17.5 (16.7-18.4)	19.4 (18.5-20.3)	20.8 (19.8-21.7)	22.0 (20.9-23.1)	23.2 (22.0-24.3)	24.7 (23.4-25.9)	25.7 (24.3-27.0)

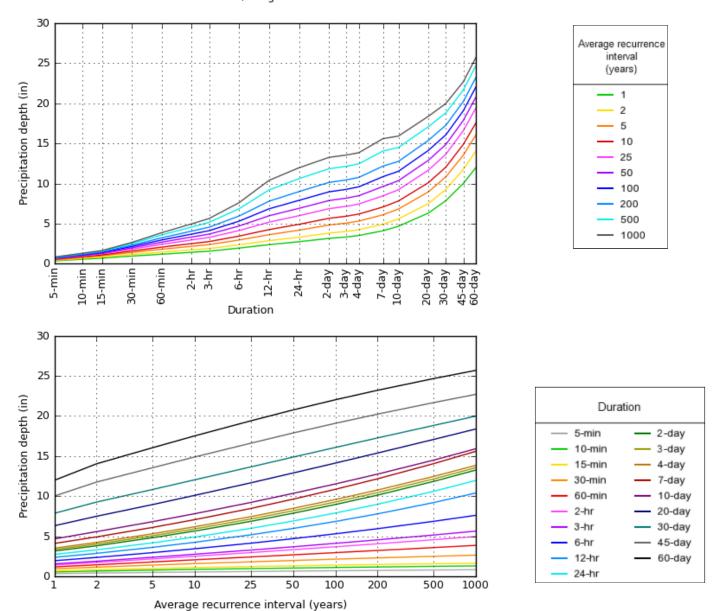
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

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PDS-based depth-duration-frequency (DDF) curves Latitude: 40.0697°, Longitude: -75.1172°



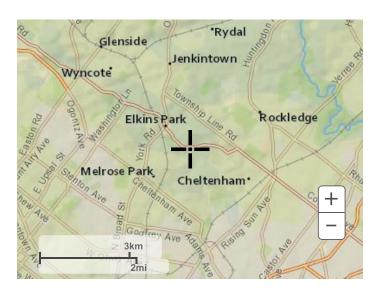
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Silver Spring, MD 20910 Questions?: <u>HDSC.Questions@noaa.gov</u>

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NOAA Atlas 14, Volume 2, Version 3 Location name: Elkins Park, Pennsylvania, USA* Latitude: 40.0697°, Longitude: -75.1172° Elevation: 147.23 ft**

* source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

G.M. Bonnin, D. Martin, B. Lin, T. Parzybok, M.Yekta, and D. Riley NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

PDS-b	PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour) ¹									
Duration				Avera	ge recurren	ce interval (years)			
Buration	1	2	5	10	25	50	100	200	500	1000
5-min	4.15 (3.79-4.56)	4.96 (4.51-5.44)	5.84 (5.32-6.41)	6.49 (5.89-7.12)	7.27 (6.58-7.97)	7.82 (7.03-8.58)	8.38 (7.49-9.20)	8.87 (7.88-9.78)	9.47 (8.34-10.5)	9.92 (8.66-11.1)
10-min	3.32 (3.03-3.64)	3.96 (3.61-4.34)	4.68 (4.26-5.13)	5.19 (4.72-5.69)	5.80 (5.24-6.35)	6.23 (5.60-6.83)	6.65 (5.95-7.31)	7.03 (6.25-7.75)	7.49 (6.59-8.30)	7.81 (6.83-8.71)
15-min	2.76 (2.52-3.03)	3.32 (3.02-3.64)	3.95 (3.59-4.33)	4.38 (3.98-4.80)	4.90 (4.42-5.36)	5.26 (4.73-5.77)	5.60 (5.02-6.16)	5.91 (5.26-6.52)	6.28 (5.54-6.97)	6.54 (5.71-7.29)
30-min	1.89 (1.73-2.08)	2.29 (2.09-2.51)	2.80 (2.55-3.07)	3.17 (2.88-3.48)	3.63 (3.28-3.97)	3.96 (3.56-4.35)	4.29 (3.84-4.72)	4.60 (4.09-5.08)	5.00 (4.40-5.55)	5.29 (4.63-5.90)
60-min	1.18 (1.08-1.30)	1.44 (1.31-1.58)	1.80 (1.64-1.97)	2.07 (1.88-2.26)	2.42 (2.18-2.65)	2.68 (2.41-2.94)	2.96 (2.65-3.25)	3.23 (2.87-3.56)	3.59 (3.16-3.98)	3.86 (3.38-4.31)
2-hr	0.710 (0.644-0.782)	0.864 (0.784-0.951)	1.09 (0.984-1.19)	1.25 (1.13-1.38)	1.48 (1.33-1.63)	1.66 (1.48-1.83)	1.84 (1.64-2.03)	2.03 (1.79-2.24)	2.29 (1.99-2.53)	2.48 (2.14-2.77)
3-hr	0.518 (0.470-0.572)	0.629 (0.571-0.695)	0.793 (0.717-0.874)	0.918 (0.829-1.01)	1.09 (0.979-1.20)	1.23 (1.10-1.35)	1.37 (1.22-1.51)	1.52 (1.33-1.68)	1.72 (1.49-1.91)	1.88 (1.61-2.10)
6-hr	0.326 (0.296-0.360)	0.394 (0.359-0.436)	0.494 (0.448-0.545)	0.575 (0.519-0.634)	0.690 (0.618-0.761)	0.785 (0.698-0.865)	0.886 (0.780-0.978)	0.993 (0.865-1.10)	1.15 (0.979-1.28)	1.27 (1.07-1.43)
12-hr	0.197 (0.180-0.218)	0.238 (0.217-0.263)	0.300 (0.274-0.332)	0.353 (0.320-0.389)	0.430 (0.386-0.474)	0.496 (0.441-0.546)	0.568 (0.498-0.627)	0.647 (0.559-0.718)	0.764 (0.644-0.853)	0.863 (0.715-0.970)
24-hr	0.114 (0.105-0.124)	0.138 (0.127-0.150)	0.174 (0.161-0.189)	0.205 (0.188-0.222)	0.249 (0.228-0.270)	0.288 (0.261-0.311)	0.329 (0.297-0.355)	0.375 (0.335-0.404)	0.442 (0.390-0.477)	0.498 (0.434-0.540)
2-day	0.066 (0.060-0.071)	0.079 (0.073-0.086)	0.100 (0.092-0.109)	0.118 (0.108-0.128)	0.143 (0.130-0.155)	0.164 (0.149-0.178)	0.187 (0.168-0.202)	0.211 (0.189-0.229)	0.247 (0.218-0.268)	0.276 (0.242-0.301)
3-day	0.046 (0.043-0.050)	0.056 (0.052-0.061)	0.070 (0.065-0.076)	0.082 (0.076-0.089)	0.099 (0.091-0.107)	0.114 (0.104-0.123)	0.129 (0.117-0.139)	0.145 (0.131-0.157)	0.169 (0.150-0.183)	0.188 (0.166-0.204)
4-day	0.037 (0.034-0.040)	0.044 (0.041-0.048)	0.055 (0.051-0.060)	0.064 (0.060-0.070)	0.078 (0.071-0.084)	0.088 (0.081-0.095)	0.100 (0.091-0.108)	0.112 (0.102-0.121)	0.130 (0.116-0.140)	0.144 (0.128-0.156)
7-day	0.024 (0.023-0.026)	0.029 (0.027-0.032)	0.036 (0.034-0.039)	0.042 (0.039-0.045)	0.050 (0.047-0.054)	0.057 (0.053-0.062)	0.065 (0.059-0.069)	0.072 (0.066-0.078)	0.084 (0.075-0.090)	0.093 (0.083-0.100)
10-day	0.019 (0.018-0.021)	0.023 (0.022-0.025)	0.028 (0.027-0.030)	0.033 (0.030-0.035)	0.038 (0.036-0.041)	0.043 (0.040-0.046)	0.048 (0.044-0.051)	0.053 (0.049-0.057)	0.060 (0.055-0.065)	0.066 (0.060-0.071)
20-day	0.013 (0.012-0.014)	0.016 (0.015-0.017)	0.019 (0.018-0.020)	0.021 (0.020-0.022)	0.024 (0.023-0.026)	0.027 (0.025-0.028)	0.029 (0.028-0.031)	0.032 (0.030-0.034)	0.036 (0.033-0.038)	0.038 (0.035-0.041)
30-day	0.011 (0.010-0.011)	0.013 (0.012-0.014)	0.015 (0.014-0.016)	0.017 (0.016-0.018)	0.019 (0.018-0.020)	0.021 (0.019-0.022)	0.022 (0.021-0.023)	0.024 (0.022-0.025)	0.026 (0.024-0.028)	0.028 (0.026-0.029)
45-day	0.009 (0.009-0.010)	0.011 (0.010-0.011)	0.013 (0.012-0.013)	0.014 (0.013-0.014)	0.015 (0.015-0.016)	0.017 (0.016-0.017)	0.018 (0.017-0.019)	0.019 (0.018-0.020)	0.020 (0.019-0.021)	0.021 (0.020-0.022)
60-day	0.008 (0.008-0.009)	0.010 (0.009-0.010)	0.011 (0.011-0.012)	0.012 (0.012-0.013)	0.013 (0.013-0.014)	0.014 (0.014-0.015)	0.015 (0.015-0.016)	0.016 (0.015-0.017)	0.017 (0.016-0.018)	0.018 (0.017-0.019)

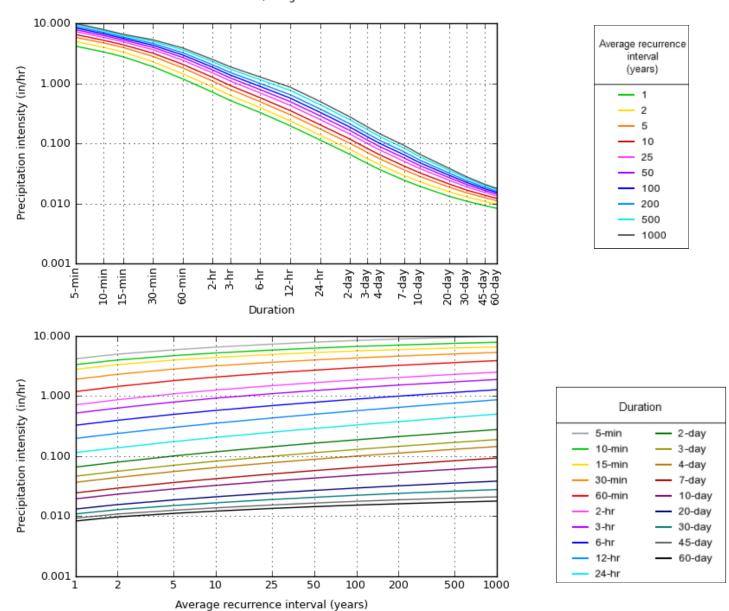
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

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PDS-based intensity-duration-frequency (IDF) curves Latitude: 40.0697°, Longitude: -75.1172°



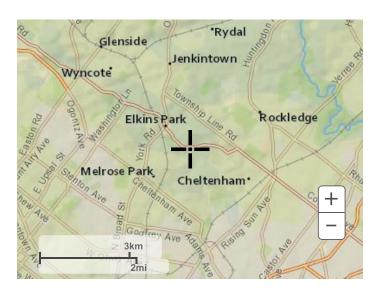
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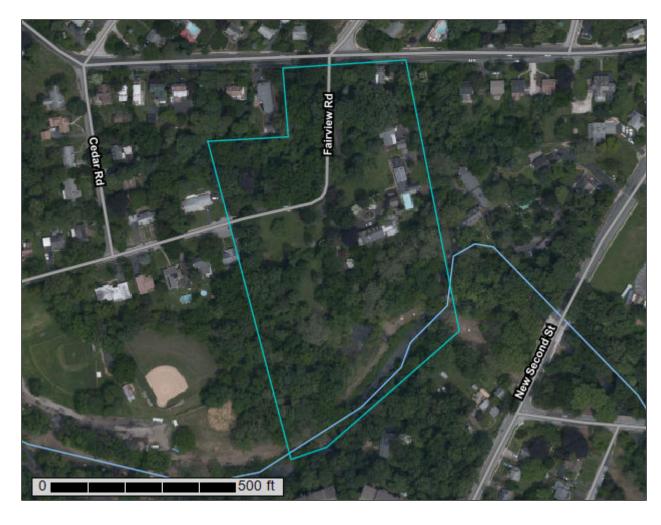
Natural Resources Conservation

Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Montgomery County, Pennsylvania

222 Church Road



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/?cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

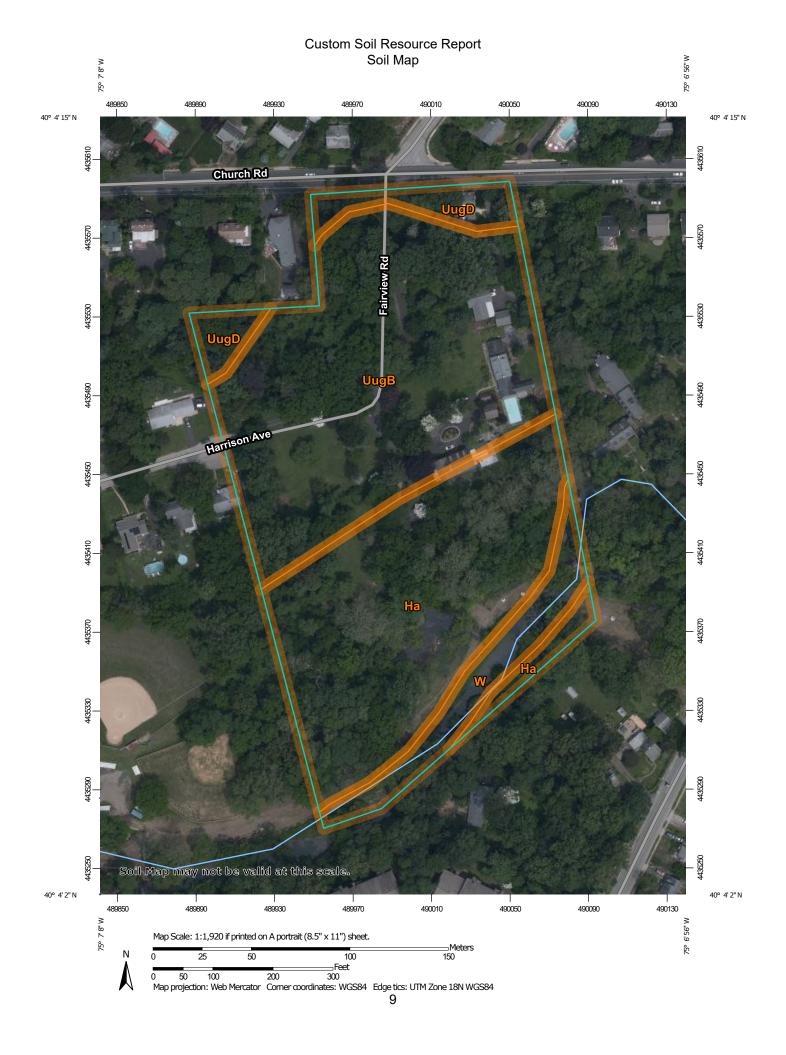
Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Map Unit Polygons

-

Soil Map Unit Lines

Soil Map Unit Points

Special Point Features

(0)

Blowout

 \boxtimes

Borrow Pit

Ж

Clay Spot

 \wedge

Closed Depression

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Gravel Pit

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Gravelly Spot

0

Landfill Lava Flow

٨.

Marsh or swamp

@

Mine or Quarry

0

Miscellaneous Water
Perennial Water

0

Rock Outcrop

4

Saline Spot

. .

Sandy Spot

_

Severely Eroded Spot

_

Sinkhole

30

Slide or Slip Sodic Spot 8

Spoil Area



Stony Spot

Δħ

Very Stony Spot

87

Wet Spot Other

Δ

Special Line Features

Water Features

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Streams and Canals

Transportation

ransp

Rails

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Interstate Highways

~

US Routes

~

Major Roads

~

Local Roads

Background

1

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:12.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Montgomery County, Pennsylvania Survey Area Data: Version 15, Jun 5, 2020

Soil map units are labeled (as space allows) for map scales 1:50.000 or larger.

Date(s) aerial images were photographed: Jun 1, 2019—Aug 4, 2019

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
На	Hatboro silt loam	4.1	38.6%
UugB	Urban land-Udorthents, schist and gneiss complex, 0 to 8 percent slopes	5.1	47.9%
UugD	Urban land-Udorthents, schist and gneiss complex, 8 to 25 percent slopes	0.6	5.8%
W	Water	0.8	7.8%
Totals for Area of Interest	,	10.7	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Montgomery County, Pennsylvania

Ha—Hatboro silt loam

Map Unit Setting

National map unit symbol: 154h Elevation: 200 to 800 feet

Mean annual precipitation: 36 to 50 inches Mean annual air temperature: 48 to 57 degrees F

Frost-free period: 140 to 200 days

Farmland classification: Not prime farmland

Map Unit Composition

Hatboro and similar soils: 95 percent Minor components: 5 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hatboro

Setting

Landform: Flood plains

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread

Down-slope shape: Concave, linear Across-slope shape: Concave, linear

Parent material: Alluvium derived from metamorphic and sedimentary rock

Typical profile

Ap - 0 to 9 inches: silt loam Bg - 9 to 44 inches: silt loam

Cg - 44 to 56 inches: sandy clay loam

C - 56 to 70 inches: stratified gravelly sand to clay

Properties and qualities

Slope: 0 to 3 percent

Depth to restrictive feature: 60 to 99 inches to lithic bedrock

Drainage class: Poorly drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high

(0.60 to 2.00 in/hr)

Depth to water table: About 0 to 6 inches Frequency of flooding: FrequentNone

Frequency of ponding: None

Available water capacity: High (about 9.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: B/D Hydric soil rating: Yes

Minor Components

Glenville

Percent of map unit: 5 percent

Landform: Hillslopes

Landform position (two-dimensional): Footslope, backslope Landform position (three-dimensional): Side slope, head slope

Down-slope shape: Linear, concave Across-slope shape: Concave, linear

Hydric soil rating: No

UugB—Urban land-Udorthents, schist and gneiss complex, 0 to 8 percent slopes

Map Unit Setting

National map unit symbol: 2dtz7 Elevation: 200 to 2,000 feet

Mean annual precipitation: 35 to 55 inches Mean annual air temperature: 45 to 61 degrees F

Frost-free period: 110 to 235 days

Farmland classification: Not prime farmland

Map Unit Composition

Urban land: 80 percent

Udorthents, schist and gneiss, and similar soils: 15 percent

Minor components: 5 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Urban Land

Setting

Landform: Hills

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Interfluve, side slope, nose slope

Down-slope shape: Linear, convex Across-slope shape: Convex, linear

Parent material: Pavement, buildings and other artifically covered areas

Typical profile

C - 0 to 6 inches: variable

Properties and qualities

Slope: 0 to 8 percent

Depth to restrictive feature: 10 to 99 inches to lithic bedrock Available water capacity: Very low (about 0.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8s

Hydric soil rating: No

Description of Udorthents, Schist And Gneiss

Setting

Landform: Hills

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Interfluve, side slope, nose slope

Down-slope shape: Linear, convex Across-slope shape: Convex, linear

Parent material: Graded areas of schist and/or gneiss

Typical profile

Ap - 0 to 6 inches: loam

C - 6 to 40 inches: silty clay loam R - 40 to 60 inches: bedrock

Properties and qualities

Slope: 0 to 8 percent

Depth to restrictive feature: 20 to 70 inches to paralithic bedrock

Drainage class: Well drained Runoff class: Medium

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.06 to 0.20 in/hr) Depth to water table: About 60 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Moderate (about 6.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7s

Hydrologic Soil Group: C Hydric soil rating: No

Minor Components

Glenelg

Percent of map unit: 1 percent

Landform: Hillslopes

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Interfluve, side slope, nose slope

Down-slope shape: Linear, convex Across-slope shape: Convex, linear

Hydric soil rating: No

Edgemont

Percent of map unit: 1 percent

Landform: Ridges

Landform position (two-dimensional): Summit Landform position (three-dimensional): Mountaintop

Down-slope shape: Convex, linear Across-slope shape: Linear, convex

Hydric soil rating: No

Glenville

Percent of map unit: 1 percent

Landform: Hillslopes

Landform position (two-dimensional): Footslope, backslope Landform position (three-dimensional): Side slope, head slope

Down-slope shape: Linear, concave Across-slope shape: Concave, linear

Hydric soil rating: No

Baile

Percent of map unit: 1 percent

Landform: Depressions

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Linear, concave Across-slope shape: Concave, linear

Hydric soil rating: Yes

Gladstone

Percent of map unit: 1 percent

Landform: Hillslopes

Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Nose slope, side slope

Down-slope shape: Linear, convex Across-slope shape: Linear, convex

Hydric soil rating: No

UugD—Urban land-Udorthents, schist and gneiss complex, 8 to 25 percent slopes

Map Unit Setting

National map unit symbol: 2dtz8 Elevation: 200 to 2,000 feet

Mean annual precipitation: 35 to 55 inches Mean annual air temperature: 45 to 61 degrees F

Frost-free period: 110 to 235 days

Farmland classification: Not prime farmland

Map Unit Composition

Urban land: 80 percent

Udorthents, schist and gneiss, and similar soils: 15 percent

Minor components: 5 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Urban Land

Setting

Landform: Hills

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Interfluve, side slope, nose slope

Down-slope shape: Linear, convex Across-slope shape: Convex, linear

Parent material: Pavement, buildings and other artifically covered areas

Typical profile

C - 0 to 6 inches: variable

Properties and qualities

Slope: 8 to 25 percent

Depth to restrictive feature: 10 to 99 inches to lithic bedrock Available water capacity: Very low (about 0.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 8s

Hydric soil rating: No

Description of Udorthents, Schist And Gneiss

Setting

Landform: Hills

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Interfluve, side slope, nose slope

Down-slope shape: Linear, convex Across-slope shape: Convex, linear

Parent material: Graded areas of schist and/or gneiss

Typical profile

Ap - 0 to 6 inches: loam

C - 6 to 40 inches: silty clay loam R - 40 to 60 inches: bedrock

Properties and qualities

Slope: 8 to 25 percent

Depth to restrictive feature: 20 to 70 inches to paralithic bedrock

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to

moderately high (0.06 to 0.20 in/hr) Depth to water table: About 60 inches

Frequency of flooding: None Frequency of ponding: None

Available water capacity: Moderate (about 6.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 7e

Hydrologic Soil Group: C Hydric soil rating: No

Minor Components

Glenville

Percent of map unit: 1 percent

Landform: Hillslopes

Landform position (two-dimensional): Footslope, backslope Landform position (three-dimensional): Side slope, head slope

Down-slope shape: Linear, concave Across-slope shape: Concave, linear

Hydric soil rating: No

Baile

Percent of map unit: 1 percent Landform: Depressions

Landform position (two-dimensional): Footslope Landform position (three-dimensional): Base slope

Down-slope shape: Concave, linear Across-slope shape: Concave, linear

Hydric soil rating: Yes

Edgemont

Percent of map unit: 1 percent

Landform: Ridges

Landform position (two-dimensional): Summit Landform position (three-dimensional): Mountaintop

Down-slope shape: Convex, linear Across-slope shape: Linear, convex

Hydric soil rating: No

Gladstone

Percent of map unit: 1 percent

Landform: Hillslopes

Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Nose slope, side slope

Down-slope shape: Linear, convex Across-slope shape: Linear, convex

Hydric soil rating: No

Glenelg

Percent of map unit: 1 percent

Landform: Hillslopes

Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Interfluve, side slope, nose slope

Down-slope shape: Linear, convex Across-slope shape: Convex, linear

Hydric soil rating: No

W-Water

Map Unit Setting

National map unit symbol: 1nnv3

Mean annual precipitation: 36 to 50 inches
Mean annual air temperature: 46 to 59 degrees F

Frost-free period: 120 to 214 days

Farmland classification: Not prime farmland

Map Unit Composition

Water: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Water

Settina

Parent material: Rivers streams ponds

Properties and qualities

Runoff class: Negligible

Frequency of ponding: Frequent

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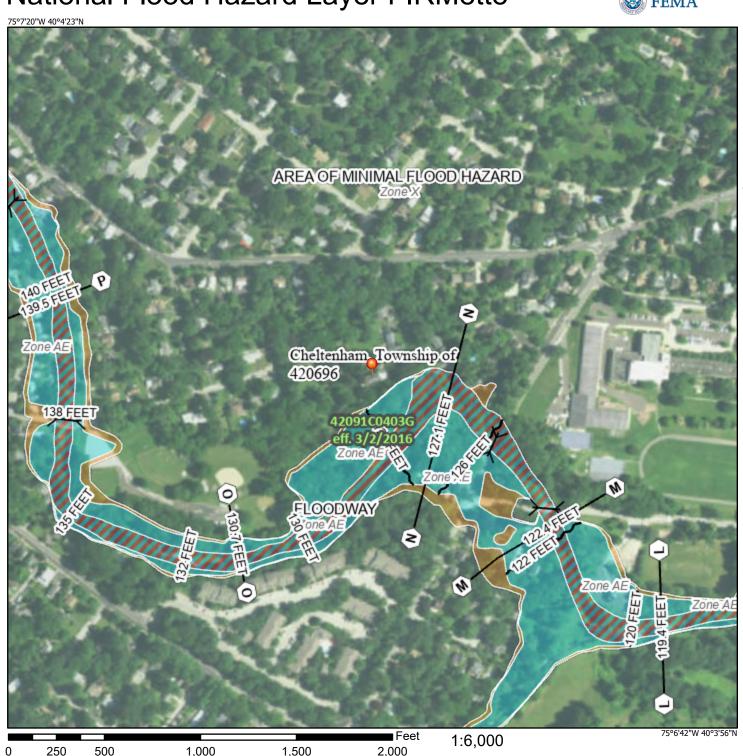
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United States Department of Agriculture, Soil Conservation Service. 1961. Land capability classification. U.S. Department of Agriculture Handbook 210. http://www.nrcs.usda.gov/Internet/FSE_DOCUMENTS/nrcs142p2_052290.pdf

National Flood Hazard Layer FIRMette

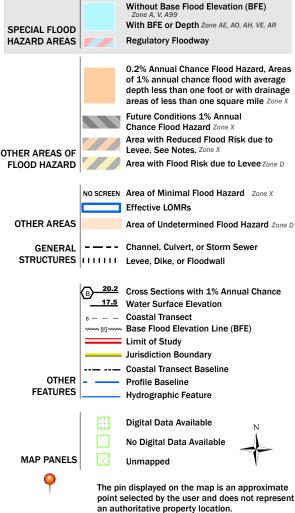


Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020



Legend

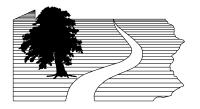
SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 6/3/2021 at 11:13 AM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.



Penn's Trail Environmental, LLC

21 E. Lincoln Ave – Suite 160 Hatfield, PA 19440 Phone: (215) 362-4610

e-mail: staff@pennstrail.com

Robert E. Blue Consulting Engineers, P.C. 1149 Skippack Pike Blue Bell, PA 19422 February 2, 2022

RE: Stormwater Infiltration Study & Report 222 Church Road Tract Cheltenham Twp., Montgomery Co., PA PTE #5303

Dear Mr. Pawlowski;

Penn's Trail Environmental, LLC has performed a subsurface soil and permeability investigation on the referenced parcel. The intent of this investigation was to evaluate the subsurface soil profile and determine the permeability characteristics of the areas indicated for proposed stormwater disposal via infiltration. Test excavations were developed with a backhoe and described in accordance with United States Department of Agriculture-Natural Resource Conservation Service (USDA-NRCS) methodology. In-situ permeability testing was conducted using the Double Ring Infiltrometer (DRI) method as described by ASTM-D3385-09 standards.

Current regulation requires that stormwater control be designed for this proposed new land development project. Permeability testing is required to determine if infiltrative capacity of the subsoil is present. Test locations were positioned throughout this site at the direction of the project engineer. Depth of testing was determined by final constructed grade of the stormwater facilities or adjusted for shallow bedrock or groundwater encountered in test excavations. A backhoe was required for excavation of the test probes and establishment of the double rings.

Soil profile descriptions were developed at each test point and include information such as texture, structure, soil depth, and indication (or lack thereof) of a seasonal high-water table or restricted drainage as would be indicated by redoximorphic features.

Redox features often occur when infiltrating water encounters a slowly permeable layer as it moves downward through the soil profile. These features do not indicate a true water table or zone that is saturated for prolonged periods by regional groundwater at this site. Regional groundwater was not encountered at this site, and redox features observed are an indicator of infiltration issues which are addressed by permeability testing and should not be considered a limiting design factor unless permeability rates reveal that to be the case.

Pre-development USDA-NRCS soil mapping at this site, or more specifically the test locations, was the Hatboro and Urban Land – Udorthents, schist and gneiss soil series. The Hatboro series consists of very deep and poorly drained soils formed in alluvium derived from metamorphic and crystalline rock. They are on flood plains. Saturated hydraulic conductivity is moderately high to high. Solum thickness ranges from 20 to 60 inches. Depth to bedrock ranges from 5 to 10 feet or more. Diagnostic horizons and features recognized in this pedon are an ochric epipedon from 0 to 9 inches (Ap horizon) and a cambic horizon from 9 to 44 inches (Bg1 and Bg2 horizons).

Udorthents are a complex collection of soils that consist of moderately well drained to excessively drained soils that have been disturbed by cutting or filling, and areas that are covered by buildings and pavement. Udorthents consist of gently sloping to moderately

sloping areas where the original soil has been cut away or covered with a loamy fill material. Permeability is moderate to slow throughout. Depth to bedrock is typically more than 60 inches. Seasonal high-water table depth is variable. Layers that restrict permeability, and buried objects may hinder deep excavations. The soil characteristics are variable, requiring on-site investigation before suitability for specific land uses can be evaluated.

The soils at the testing locations were found to be derived primarily from schist as mapped. This investigation was not conducted for the purpose of disputing current mapping or as a remapping effort. Loess material was found to overtop schist derived soils at certain test locations. Soil series designations are provided on the attached soil profile data sheets.

Soil profiles of backhoe excavated test pits were developed to depths at or near final constructed grade of proposed stormwater control facilities. The most restrictive barriers from the point of infiltration to contacting the base flow groundwater table were determined. The most common of these barriers in our region include restrictive soil horizons, varying lithology, fracturing of the bedrock or insufficient fracturing of the bedrock, and encountering groundwater among other factors. Our field observations, as reported on the attached soil profile data sheets, indicate that slowly diggable conditions were not encountered in the test pits. Redoximorphic features were noted in test pits 3, 4 and 6 throughout the lower argillic horizon (Bt2). Subsequent detailed testing more accurately predicts the ability of the soil to efficiently infiltrate stormwater and has been attached.

Testing sought to identify zones that would potentially allow the infiltration of stormwater. The testing protocol used considers regional construction practices, the likelihood of "silting in" during and following construction and the subsurface characteristics of the soil and geology. The determination at this site was that no restrictive condition was encountered to the established installation depth for infiltration of stormwater. The double rings were established at a level with sufficient residual subsoil above groundwater and bedrock to seat and seal the rings permitting unsaturated flow through the soil to the water table.

The recommended acceptable range for subsurface disposal of stormwater is 0.10 inches per hour to 10.0 inches per hour according to current BMP guidance. Surface basins where additional storage is economical can have much slower rates and still provide some infiltration. Our office recommends that the design engineer assume zero infiltration for any stormwater area which achieves less than 0.10 inches per hour.

There are various means to arrive at an infiltrative rate for the substratum following testing. Our method is to average the last four stabilized readings as established in the PA BMP Manual. Another is to use the "last" reading as is common for percolation testing for wastewater disposal. Averaging more accurately reflects what would likely occur during a rain (soil saturation) event.

Testing was conducted at discreet locations selected by the project engineer using double ring infiltrometers. Data sheets containing the information recorded for the soil profile descriptions and double ring infiltrometers have been included as attachments to this report. A table summarizing the field data can be found below:

Stormwater Testing Summary										
Test Location	Depth of Test Pit	Depth to Water	Depth to Rock	Depth of Testing	Infiltration Rate					
Location	Inches	Inches	Inches	Inches	Inches per hour					
1	100			72	2.59					
2	101			72	0.12					

3	99	 	72	0.00
4	99	 	72	0.15
5	101	 	70*	0.43
6	101	 	77*	4.11

*Infiltration testing was conducted deeper than proposed due to the sandy texture of a deeper horizon that would promote better infiltration.

The soil encountered demonstrated varied infiltration rates. Subsurface conditions may change following construction and resultant redirection of surface water following development. Results suggest that the average infiltration rates at tested locations 1, 5 and 6 are within the recommended guidelines even after a safety factor of two is applied. Results suggest that the average infiltration rates tested locations 2, 3, and 4 are below the recommended guidelines of 0.10 inches per hour either before or after a safety factor of two is applied.

At test locations 1, 5, and 6, stormwater control devices can include surface and subsurface facilities that allow the design engineer flexibility in reducing velocity containing and disposing of stormwater on this site in select areas due to the channery composition of the soil at this site. Surface features such as vegetated swales and berms can be employed to reduce overland flow and retain water in-situ thus extending contact time and providing for additional infiltration.

At test locations, 2, 3, and 4, stormwater control devices that allow the design engineer flexibility in reducing velocity containing and disposing of stormwater on this site should be limited to surface facilities due to the clayey composition and slow drainage of the soil at this location. Surface features such as vegetated swales and berms can be employed to reduce overland flow and retain water in-situ thus extending contact time and providing for additional infiltration.

Our findings are a result of testing conducted in specific locations and conditions. Should evidence contrary to the findings in this report be discovered prior to, during, or after construction of the stormwater control devices, our office must be notified immediately so our recommendations can be reviewed and revised if necessary.

Penn's Trail Environmental, LLC expresses no guarantee that the soil conditions following excavation will be identical to those encountered during this investigation. We recommend that caution is exercised during construction to minimize compaction, or other disturbance in those areas intended for use as infiltration areas.

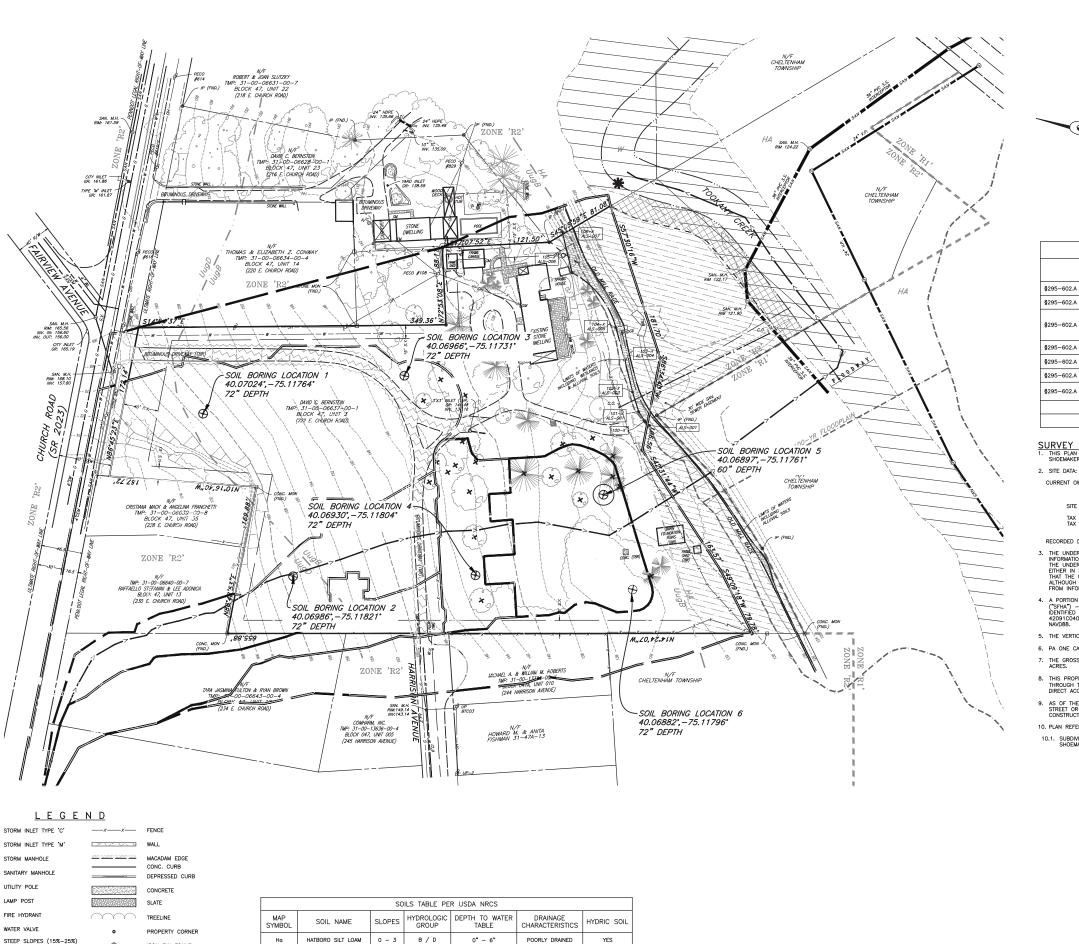
Please review the enclosed information and if any questions arise do not hesitate to contact our office.

Sincerely,

Penn's Trail Environmental, LLC

Paul A. Golrick/JH

Soil Scientist



IRON PIN FOUND

TO BE DEMOLISHED

FLOODPLAIN

RIPARIAN CORRIDOR - ZONE RIPARIAN CORRIDOR - ZONE 2 UugB

UugD

0 - 8

8 - 25

URBAN LAND -UDORTHENTS

WATER

> 60"

> 60"

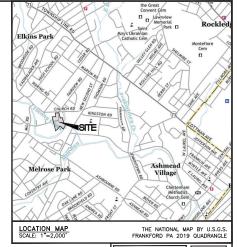
WELL DRAINED

WELL DRAINED

NO

NO





REQUIREMENTS	EXISTING (222 E. CHURCH)
10,000 S.F.	6.2497 ACRES (272,238 S.F.)
70 FT.	172.14 FT.
FRONT YARD = 40 FT. SIDE YARD (AGG.) = 30 FT. SIDE YARD (MIN.) = 10 FT. REAR YARD = 25 FT.	FRONT YARD = 40 FT. SIDE YARD (AGG.) = 30 FT. SIDE YARD (MIN.) = 15 FT. REAR YARD = 25 FT.
20%	1.4% (3,788 S.F.)
40%	8.0% (21,590 S.F.)
<40 FT.	<40 FT.
10 FT. FROM FRONT FACADE	N/A
	10,000 S.F. 70 FT. FRONT YARD = 40 FT. SIDE YARD (AGC.) = 30 FT. SIDE YARD (MIN.) = 10 FT. REAR YARD = 25 FT. 20% 40% <40 FT. 10 FT. FROM FRONT

SURVEY NOTES:

1. THIS PLAN REPRESENTS AN ACTUAL FIELD SURVEY PERFORMED BY CHARLES E. SHOEMARER, INC. COMPLETED IN FEBRUARY, 2021.

CURRENT OWNER: DAVID C. BERNSTEIN 222 E. CHURCH ROAD ELKINS PARK, PA 19027

SITE ADDRESS: 222 E. CHURCH ROAD
ELKINS PARK, PA 19027
TAX MAP: BLOCK 47 - UNIT 3
TAX NUMBER: PARCEL 31-00-06637-001
DB 6206 PG 272

RECORDED DATA: CHELTENHAM TOWNSHIP, MONTGOMERY COUNTY, PENNSYLVANIA

- THE UNDERGROUND UTILITIES SHOWN HAVE BEEN LOCATED FROM FIELD SURVEY INFORMATION AND EXISTING DRAWINGS. THE SURVEYOR MAKES NO GUARANTEES THAT THE UNDERGROUND UTILITIES SHOWN COMPRISE ALL SUCH UTILITIES IN THE AREA, EITHER IN SERVICE OR ABANDONED. THE SURVEYOR FURTHER DOES NOT WARRANT THAT THE UNDERGROUND UTILITIES SHOWN ARE IN THE EXACT LOCATION INDICATED ALTHOUGH HE DOES CONFIRM THAT THEY ARE LOCATED AS ACCURATELY AS POSSIBLE FROM INFORMATION AVAILABLE.
- 4. A PORTION OF THE PROJECT SITE SHOWN LIES WITHIN A SPECIAL FLOOD HAZARD AREA ("SFHA") ZONE AE, AS DOCUMENTED ON THE FLOOD INSURANCE RATE MAP IDENTIFIED AS PANEL 403 OF 451, COMMUNITY NUMBER 420696, MAP NUMBER 42091C0403G; EFFECTIVE DATE: MARCH 2, 2016. THE DATUM FOR THIS MAP IS NAVDBB.
- 5. THE VERTICAL DATUM FOR THIS SITE IS NAVD 1988 BASED ON GPS OBSERVATIONS.
- 6. PA ONE CALL SERIAL NUMBER: SERIAL #20212303507, DATED AUGUST 21, 2021
- THE GROSS AND NET AREA OF 222 E. CHURCH ROAD IS 272,238 S.F. OR 6.2497 ACRES.
- THIS PROPERTY HAS DIRECT ACCESS TO CHURCH ROAD (SR 2023), A PUBLIC STREET, THROUGH TWO (2) TWO-WAY MACADAM DRIVEWAYS. ADDITIONAL THIS PROPERTY HAS DIRECT ACCESS TO HARRISON AVENUE, A PUBLIC STREET.

10. PLAN REFERENCES:

10.1. SUBDIVISION PLA FOR 216 & 222 E. CHURCH ROAD, PREPARED BY CHARLES E. SHOEMAKER, INC., DATED MARCH 1, 2021, LAST REVISED MARCH 31, 2021.

lue ineer Blue Br fax: email: Φ Consulting consulting 1149 Skippack Fel: (610)-277-9 www.robertblue.c.

(DATE)

Penn's Trail Environmental, LLC



21 East Lincoln Ave - Suite 160 Hatfield, PA 19440 ph. (215) 362-4610 Date: 2/2/22 Pit # 1 PTE # 5303
Project: 222 Church Road

Location: 222 Church Road

Cheltenham Twp., Montgomery Co., PA

Soil Series Glenelg

Horizon	Depth (in.)	Color	Redox Features	Texture	Structure	Consistence	Boundary
A	0-6	10YR 3/4		silt loam	strong coarse gr	very friable	clear wavy
Bt	6-42	10YR 5/6		channery sandy loam	weak fine sbk	friable	clear wavy
С	42-100	10YR 5/4		very channery loamy sand	weak very fine sbk	very friable	

Soil Scientist: Terry Harris

Notes

EPIPEDON

Ochric

SUBSURFACE HORIZON(S)

Argillic

SOIL ORDER

Ultisol

DRAINAGE CLASS

Well Drained

LANDFORM

Upland

POSITION

Backslope

PARENT MATERIAL

Colluvium Residuum

BEDROCK LITHOLOGY

Schist

REDOX FEATURES

Abundance

Few <2%
Common .. 2-20%
Many>20%

Contrast faint

hue & chroma of matrix and redox are closely related.

distinct

matrix & redox features vary 1-2 units of hue and several units of chroma & value.

prominent

Matrix & redox features vary several units in hue, value & chroma.

STRUCTURE

Grade

Structureless - No observable aggregation or arrangement of lines of weakness.

Weak - Poorly formed, indistinct peds barely observable in place.

 $\label{eq:moderate} \begin{aligned} &\textit{Moderate} \, - \, \text{Well-formed, distinct} \\ &\textit{peds moderately durable \&} \end{aligned}$

evident in place.

Strong - Durable peds evident in undisturbed soil & become separated when disturbed.

COURSE FRAGMENTS (% of profile)

35-65% >65% 15-35% extremely gravelly gravelly very gravelly very channery extremely channery channery cobbly very cobbly extremely cobbly extremely flaggy flaggy very flaggy stony very stony extremely stony

BOUNDARY

Distinctness

abrupt...<1" (thick) gradual...2.5-5" clear.....1-2.5" diffuse......>5"

Topography

smooth - boundary is nearly level
 wavy - pockets with width greater than depth
 irregular - pockets with depth greater than width
 broken - boundary is discontinuous
 and interrupted

Type

pl - platy

pr - prismatic

cpr - columnar

gr - granular

abk - angular blocky

sbk - subangular blocky

Penn's Trail Environmental, LLC



21 East Lincoln Ave - Suite 160 Hatfield, PA 19440 ph. (215) 362-4610 Date: 2/2/22 Pit # 2 PTE # 5303

Project: 222 Church Road
Location: 222 Church Road

Cheltenham Twp., Montgomery Co., PA

Soil Series Glenelg

Horizon	Depth (in.)	Color	Redox Features	Texture	Structure	Consistence	Boundary
A1	0-4	10YR 3/4		silt loam	strong coarse gr	very friable	clear wavy
A2	4-10	10YR 5/3		silt loam	moderate medium gr	friable	clear wavy
Bt	10-90	10YR 5/6		channery sandy loam	weak fine sbk	friable	clear wavy
С	90-101	10YR 5/4		very channery loamy sand	weak very fine sbk	very friable	

Soil Scientist: Terry Harris

Notes

EPIPEDON

Ochric

SUBSURFACE HORIZON(S)

Argillic

SOIL ORDER

Ultisol

DRAINAGE CLASS

Well Drained

LANDFORM

Upland

POSITION

Backslope

PARENT MATERIAL

Colluvium Residuum

BEDROCK LITHOLOGY

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21 East Lincoln Ave - Suite 160 Hatfield, PA 19440 ph. (215) 362-4610 Date: 2/2/22 Pit # 3 PTE # 5303 Project: 222 Church Road

Location: 222 Church Road

Cheltenham Twp., Montgomery Co., PA

Soil Series Duncannon

Horizon	Depth (in.)	Color	Redox Features	Texture	Structure	Consistence	Boundary
Ap	0-14	10YR 4/4		silt loam	moderate medium gr	very friable	clear wavy
Bt1	14-67	10YR 7/6		silt loam	moderate medium sbk	friable	clear wavy
Bt2	67-99	10YR 7/6	common distinct	silt loam	moderate medium sbk	friable	

Soil Scientist: Terry Harris

Notes

EPIPEDON

Ochric

SUBSURFACE HORIZON(S)

Argillic

SOIL ORDER

Alfisol

DRAINAGE CLASS

Well Drained

LANDFORM

Upland

POSITION

Backslope

PARENT MATERIAL

Loess

BEDROCK LITHOLOGY

Schist

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cpr - columnar

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abk - angular blocky



21 East Lincoln Ave - Suite 160 Hatfield, PA 19440 ph. (215) 362-4610 Date: 2/2/22 Pit # 4 PTE # 5303
Project: 222 Church Road

Project: 222 Church Road Location: 222 Church Road

Cheltenham Twp., Montgomery Co., PA

Soil Series Duncannon

Horizon	Depth (in.)	Color	Redox Features	Texture	Structure	Consistence	Boundary
Ap	0-10	10YR 4/4		silt loam	moderate medium gr	very friable	clear wavy
Bt1	10-55	10YR 7/6		silt loam	moderate medium sbk	friable	clear wavy
Bt2	55-99	10YR 7/6	common distinct	silt loam	moderate medium sbk	friable	

Soil Scientist: Terry Harris

Notes

<u>EPIPEDON</u>

Ochric

SUBSURFACE HORIZON(S)

Argillic

SOIL ORDER

Alfisol

DRAINAGE CLASS

Well Drained

LANDFORM

Upland

POSITION

Backslope

PARENT MATERIAL

Loess

BEDROCK LITHOLOGY

Schist

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21 East Lincoln Ave - Suite 160 Hatfield, PA 19440 ph. (215) 362-4610 Date: 2/2/22 Pit # 5 PTE # 5303

Project: 222 Church Road
Location: 222 Church Road

Cheltenham Twp., Montgomery Co., PA

Soil Series Duncannon taxadjunct

Horizon	Depth (in.)	Color	Redox Features	Texture	Structure	Consistence	Boundary
Ap	0-15	10YR 4/4		silt loam	strong medium gr	very friable	gradual wavy
Bt/2C	15-65	10YR 7/6 10YR 5/3		silt loam loamy sand	moderate medium sbk	friable	clear wavy
2C	65-101	10YR 5/3		channery loamy sand	weak very fine sbk	very friable	

Soil Scientist: Terry Harris

Notes

EPIPEDON

Ochric

SUBSURFACE HORIZON(S)

Argillic

SOIL ORDER

Alfisol

DRAINAGE CLASS

Well Drained

LANDFORM

Upland

POSITION

Backslope

PARENT MATERIAL

Loess Residuum

BEDROCK LITHOLOGY

Schist

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21 East Lincoln Ave - Suite 160 Hatfield, PA 19440 ph. (215) 362-4610 Date: 2/2/22 Pit # 6 PTE # 5303

Project: 222 Church Road
Location: 222 Church Road

Cheltenham Twp., Montgomery Co., PA

Soil Series Lawrenceville taxadjunct

Horizon	Depth (in.)	Color	Redox Features	Texture	Structure	Consistence	Boundary
Ap	0-13	10YR 4/4		silt loam	strong medium gr	very friable	gradual wavy
Bt1	13-31	10YR 7/6		silt loam	moderate medium sbk	friable	clear wavy
Bt2	31-62	10YR 7/6	common distinct	silt loam	moderate medium sbk	friable	gradual wavy
2C	62-101	10YR 5/3		channery loamy sand	weak very fine sbk	very friable	

Soil Scientist: Terry Harris

Notes

EPIPEDON

Ochric

SUBSURFACE HORIZON(S)

Argillic

SOIL ORDER

Alfisol

DRAINAGE CLASS

Moderately Well Drained

LANDFORM

Upland

POSITION

Backslope

PARENT MATERIAL

Loess Residuum

BEDROCK LITHOLOGY

Schist

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222 Church Road	Job #
222 Church Road	Date:
Cheltenham	Ring #:
Montgomery	Technician:
	Tax Parcel:
50's °F	Weather:
72 inches	pH:

F 909
5303
2/2/2022
1
Cody Kline
31-00-06637-00-1
cloudy 30's °F
6.9

Time	Interval	Inner Ring Drop	Inner Ring Volume change	Outer Ring Drop	Outer Ring Volume Change	Rate	Infiltration rate
(hr:min)	(min.)	(in.)	(ml)	(in.)	(ml)	(ml/min)	(in/hr)
8:35 AM	$>\!\!<$		fill		fill	$>\!\!<$	\searrow
9:05 AM	30	2 1/8	1,000	2 1/8	1,750	33.33	4.32
9:35 AM	30	2	900	1	800	30.00	3.88
9:45 AM	10	3/8	200	2/8	250	20.00	2.59
9:55 AM	10	4/8	210	2/8	250	21.00	2.72
10:05 AM	10	3/8	190	2/8	240	19.00	2.46
10:15 AM	10	3/8	200	2/8	250	20.00	2.59
Average	><		200.00		247.50	20.00	2.59

222 Church Road	Job #
222 Church Road	Date:
Cheltenham	Ring #:
Montgomery	Technician:
	Tax Parcel:
50's °F	Weather:
72 inches	pH:

5303
2/2/2022
2
Cody Kline
31-00-06637-00-1
cloudy 30's °F
6.9

Time	Interval	Inner Ring Drop	Inner Ring Volume change	Outer Ring Drop	Outer Ring Volume Change	Rate	Infiltration rate
(hr:min)	(min.)	(in.)	(ml)	(in.)	(ml)	(ml/min)	(in/hr)
9:00 AM	>><		fill		fill	\mathbf{X}	\searrow
9:30 AM	30	2 1/8	1,000	1 2/8	1,000	33.33	4.32
10:00 AM	30	2/8	90	1/8	100	3.00	0.39
10:30 AM	30	< 1/8	20	< 1/8	30	0.67	0.09
11:00 AM	30	1/8	30	< 1/8	30	1.00	0.13
11:30 AM	30	1/8	30	< 1/8	30	1.00	0.13
12:00 PM	30	1/8	30	< 1/8	30	1.00	0.13
				·			
Average	\searrow		27.50		30.00	0.92	0.12

222 Church Road	Job #
222 Church Road	Date:
Cheltenham	Ring #:
Montgomery	Technician:
	Tax Parcel:
50's °F	Weather:
72 inches	pH:

5303
2/2/2022
3
Cody Kline
31-00-06637-00-1
cloudy 30's °F
6.9

Time	Interval	Inner Ring Drop	Inner Ring Volume change	Outer Ring Drop	Outer Ring Volume Change	Rate	Infiltration rate
(hr:min)	(min.)	(in.)	(ml)	(in.)	(ml)	(ml/min)	(in/hr)
8:45 AM	>><		fill		fill	>>	$>\!\!<$
9:15 AM	30	1/8	70	1/8	75	2.33	0.30
9:45 AM	30	< 1/8	20	< 1/8	50	0.67	0.09
10:15 AM	30	0	0	< 1/8	10	0.00	0.00
10:45 AM	30	0	0	0	0	0.00	0.00
11:15 AM	30	0	0	0	0	0.00	0.00
11:45 AM	30	0	0	0	0	0.00	0.00
Average	$\geq \leq$		0.00		2.50	0.00	0.00



22 Church Road	Job #
22 Church Road	Date:
heltenham	Ring #:
Iontgomery	Technician:
	Tax Parcel:
o's °F	Weather:
2 inches	pH:

5303
2/2/2022
4
Terry Harris
31-00-06637-00-1
cloudy 30's °F
6.9

Time	Interval	Inner Ring Drop	Inner Ring Volume change	Outer Ring Drop	Outer Ring Volume Change	Rate	Infiltration rate
(hr:min)	(min.)	(in.)	(ml)	(in.)	(ml)	(ml/min)	(in/hr)
9:16 AM	$>\!\!<$		fill		fill	$>\!\!<$	\searrow
9:46 AM	30	1/8	70	4/8	400	2.33	0.30
10:16 AM	30	1/8	30	< 1/8	30	1.00	0.13
10:46 AM	30	1/8	50	1/8	60	1.67	0.22
11:16 AM	30	< 1/8	20	< 1/8	30	0.67	0.09
11:46 AM	30	1/8	40	< 1/8	30	1.33	0.17
12:16 PM	30	1/8	30	< 1/8	30	1.00	0.13
Average	\searrow		35.00		37.50	1.17	0.15

222 Church Road	Job #
222 Church Road	Date:
Cheltenham	Ring #:
Montgomery	Technician:
	Tax Parcel:
50's °F	Weather:
70 inches	pH:

5303
2/2/2022
5
Terry Harris
31-00-06637-00-1
cloudy 30's °F
6.9

Time	Interval	Inner Ring Drop	Inner Ring Volume change	Outer Ring Drop	Outer Ring Volume Change	Rate	Infiltration rate
(hr:min)	(min.)	(in.)	(ml)	(in.)	(ml)	(ml/min)	(in/hr)
9:49 AM	$>\!\!<$		fill		fill	\mathbf{X}	\searrow
10:19 AM	30	1/8	70	3/8	330	2.33	0.30
10:49 AM	30	2/8	100	3/8	340	3.33	0.43
11:19 AM	30	2/8	100	2/8	210	3.33	0.43
11:49 AM	30	2/8	110	3/8	310	3.67	0.47
12:19 PM	30	2/8	100	3/8	270	3.33	0.43
12:49 PM	30	2/8	90	2/8	250	3.00	0.39
Average	><		100.00		260.00	3.33	0.43

222 Church Road	Job #
222 Church Road	Date:
Cheltenham	Ring #:
Montgomery	Technician:
	Tax Parcel:
50's °F	Weather:
77 inches	pH:

5303
2/2/2022
6
Terry Harris
31-00-06637-00-1
cloudy 30's °F
6.9

Time	Interval	Inner Ring Drop	Inner Ring Volume change	Outer Ring Drop	Outer Ring Volume Change	Rate	Infiltration rate
(hr:min)	(min.)	(in.)	(ml)	(in.)	(ml)	(ml/min)	(in/hr)
9:31 AM	>>		fill		fill	\mathbb{X}	\bigvee
10:01 AM	30	2 4/8	1,160	2 6/8	2,260	38.67	5.01
10:31 AM	30	2 2/8	1,040	2 1/8	1,750	34.67	4.49
10:41 AM	10	6/8	360	1 1/8	890	36.00	4.66
10:51 AM	10	5/8	300	3/8	350	30.00	3.88
11:01 AM	10	5/8	290	3/8	320	29.00	3.75
11:11 AM	10	6/8	320	4/8	410	32.00	4.14
Average	><		317.50		492.50	31.75	4.11



April 21, 2023

Steven N. Kline, AIA Regan/Kline/Cross 7670 Queen Street, Suite 200 Wyndmoor, PA 19038

via email: s_kline@reganklinecrossllc.com

Re: Wetland/Waters Investigation

TM# 31-00-06637-001

222 Church Road Elkins Park, PA 19027 Cheltenham Township, Montgomery County

Dear Mr. Kline,

VW Consultants, LLC (VW) is pleased to present this letter summarizing findings of a wetland evaluation completed on March 22, 2023 at the above referenced property. The purpose of the routine investigation was to identify and delineate wetlands and waters of the US and Commonwealth for a proposed residential land development project. This evaluation area was completed throughout the ± 5.05 acres property. The property has frontage Church Road and Harrison Ave with paved driveways from each. The property currently contains a stone dwelling and associated outbuildings. The majority of the property is well maintained lawn with scattered mature trees. Site surface drainage is generally toward the south in the direction of Tookany Creek which traverses neighboring lots.

Methodology

The site was evaluated per routine procedures established by <u>Corps of Engineers Wetland Delineation Manual</u> (1987) and <u>Regional Supplement to the Corps of Engineers Wetland Manual: Eastern Mountains and Piedmont Region, (Version 2.0) (2012)</u>. To qualify as a wetland the manuals require the area to exhibit hydric soils, dominance of hydrophytic vegetation, and wetland hydrology.

VW traversed the project site to identify plant communities and wetland hydrology indicators. Samples points were located in and along low-lying sections of the site most likely to contain wetlands. The project site and delineated wetlands are depicted on the attached *Existing Features* plan, dated July 23, 2021, last revised April 10, 2023, prepared by Robert E. Blue Consulting Engineers, p.c. Locations of the sample points documented on the attached forms are also indicated on the site plan.

Desktop Resource Review and Setting

A review the U.S. Fish and Wildlife Services National Wetlands Inventory (NWI) Map revealed presence of riverine habitat associated with Tookany Creek and a forested wetland within the creeks floodway. Both mapped features are off site and down gradient of the project area.

The current Soil Survey of Montgomery County, Version 6, Sept. 17, 2019, published by the National Resource Conservation Service and accessed via Web Soil Survey indicates soils on the subject site are expected to be Hatboro silt loam (Ha) and Urban land-Udorthents of schist and gneiss (UugB & UugD). The Hatboro soil series is recognized as very deep and poorly drained Inceptisols formed in alluvium from metamorphic and crystalline rock. The Urban land-Udorthents mapping units indicate a combination of manmade impervious coverages and cut/fill lands. Given the site bedrock formation of Wissahickon schist and hillslope position the author would

expect to encountered well drained Glenelg type soil and moderately well Glenville type soil, with an urban component based on the developed condition. Evidence of significant and filling activity was not readily apparent in the upland portion of the project site based on our above grade observations.

Findings

The project site contains a manmade water conveyance structure reported to have been a mill raceway. This raceway is disconnected from the source of surface water as control structures have deteriorated and berms eroded allowing the outlet of water to Tookany Creek upgradient of the project site. A small on-site masonry structure is labelled as Spring House on the Existing Features Plan. During our site visit in late March following a warm wet winter no spring was present at the Spring House. Function of the spring house is likely impacted by changes to the local hydrologic regime as the result of extensive land development or it may have originally functioned as a root cellar.

The raceway currently contains a small area of closed grading where surface water is present in small pools at the lowest points. This area meets the criteria of a wetland and was field delineated as such. It is unclear how much of the wetland's hydrology is the result of shallow groundwater or if the wetland is supported by transmission of infiltrated water transmitted via sediment deposits to this low point. To the east and west of the wetland feature the raceway plant communities become more neutral in their affinity for saturated soil conditions and hydrology and hydric soils become absent. The wettest portion of the wetland was unvegetated at the time of our site visit. Margin species include Eurasian buttercup (*Ficaria verna*), boxelder maple (*Acer negundo*), and Amur honeysuckle (*Lonicera maackii*).

A natural wetland located at the rear of the Tookany Creek floodplain is present along the toe of the raceway berm. This wetland extends off site to the south. A surface connection from the raceway wetland to the flooplain wetland is present in the form of an erosion channel through the berm. The hydrology source of the floodplain wetland is regional groundwater discharge. The connection with the raceway appears to have minimal impacts on the floodplain wetland hydrology and characteristics. Dominant plants include Eurasian butter cup and boxelder maple, along with skunk cabbage (*Symplocarpus foetidus*) in the most lowlying locations.

Conclusion

The project site includes a wetland regulated by the Commonwealth of Pennsylvania and under Federal jurisdiction administered by the Army Corps of Engineers. The wetland exhibits varying characteristic. The upper portion can be characterized as a manmade depressional wetland to vernal pool during wet springs. The remainder is a backswamp floodplain wetland with drainage channel. The abandoned mill raceway does not exhibit fluvial characteristics that support regulation as a water course. Final jurisdictional boundaries are dependent upon Federal and State field determinations. Should you need any assistance with permitting of disturbance of wetlands or waters please feel free to contact me at 267-498-8778 or by email at <a href="maintenanto-minimal-multipleasing-minimal-minimal-multipleasing-minimal-mul

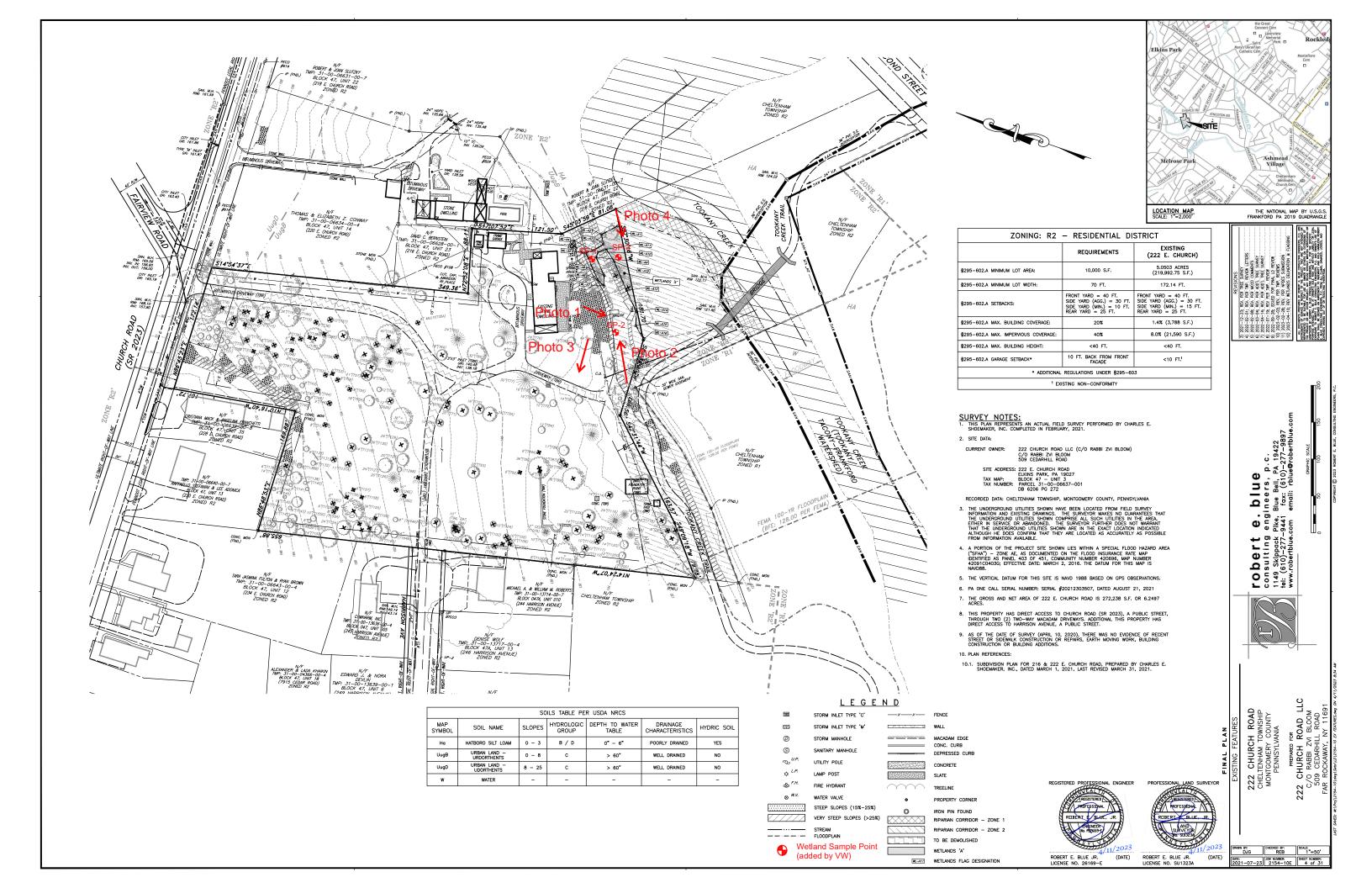
Respectfully submitted,

VW Consultants, LLC Max Russick, CPSS

Soil Scientist

Enclosures: Existing Features Plan (reduced to 11"x17"), NWI Map Figure, Data Forms, NC DWQ Stream Identification Form, Photo Plates

CC: Robert Blue, P.E.- Robert E. Blue Consulting Engineers, P.C. Michael Baginski, E.I.T.- Robert E. Blue Consulting Engineers, P.C.



U.S. Fish and Wildlife Service

National Wetlands Inventory

222 Church Road



April 20, 2023

Wetlands

Estuarine and Marine Deepwater

Estuarine and Marine Wetland

Freshwater Emergent Wetland

Freshwater Forested/Shrub Wetland

Freshwater Pond

Lake

Other

Riverine

This map is for general reference only. The US Fish and Wildlife Service is not responsible for the accuracy or currentness of the base data shown on this map. All wetlands related data should be used in accordance with the layer metadata found on the Wetlands Mapper web site.

U.S. Army Corps of Engineers

WETLAND DETERMINATION DATA SHEET – Eastern Mountains and Piedmont Region

OMB Control #: 0710-0024, Exp:11/30/2024 Requirement Control Symbol EXEMPT: (Authority: AR 335-15, paragraph 5-2a)

See ERDC/EL TR-12-9; the proponent agency is CECW-CO-R

Project/Site: 222 Church Road		City/County: Montgome	ery Co.	Sampling Date: 3/22/23
Applicant/Owner: 222 Church Road LLC			State: PA	Sampling Point: 1
Investigator(s): Max Russick	Se	ction, Township, Range:	Cheltanham Twp.	
Landform (hillside, terrace, etc.): Artificial T	errace Local	relief (concave, convex,	none): Concave	Slope (%):1-2
Subregion (LRR or MLRA): LRR S, MLRA 1	48 Lat: 40.06911	Long: -7	75.11680	Datum: WGS 84
Soil Map Unit Name: Hatboro			NWI classifica	tion: Vernal Pool/PEM
Are climatic / hydrologic conditions on the site	typical for this time of year?	Yes	No (If no, e	explain in Remarks.)
Are Vegetation X , Soil X , or Hydro			ircumstances" present?	
Are Vegetation , Soil , or Hydro			plain any answers in Re	
SUMMARY OF FINDINGS – Attach			-	
Hydrophytic Vegetation Present? Hydric Soil Present? Wetland Hydrology Present?		s the Sampled Area vithin a Wetland?	Yes <u>X</u>	No
Remarks:				
HYDROLOGY				
Wetland Hydrology Indicators:			Socondary Indicators	(minimum of two required)
Primary Indicators (minimum of one is requi	red: check all that apply)		Surface Soil Crac	•
X Surface Water (A1)	True Aquatic Plants (B1	4)		ed Concave Surface (B8)
X High Water Table (A2)	Hydrogen Sulfide Odor	,	Drainage Patterns	, ,
X Saturation (A3)	Oxidized Rhizospheres		Moss Trim Lines (
Water Marks (B1)	Presence of Reduced Ir	on (C4)	Dry-Season Wate	r Table (C2)
Sediment Deposits (B2)	Recent Iron Reduction i	n Tilled Soils (C6)	Crayfish Burrows	(C8)
Drift Deposits (B3)	Thin Muck Surface (C7)		Saturation Visible	on Aerial Imagery (C9)
Algal Mat or Crust (B4)	Other (Explain in Remai	rks)	Stunted or Stress	ed Plants (D1)
Iron Deposits (B5)			Geomorphic Posit	tion (D2)
Inundation Visible on Aerial Imagery (B7	')		Shallow Aquitard	(D3)
Water-Stained Leaves (B9)			Microtopographic	
Aquatic Fauna (B13)			FAC-Neutral Test	(D5)
Field Observations:				
Surface Water Present? Yes X	No Depth (inches):			
Water Table Present? Yes X	No Depth (inches):			
Saturation Present? Yes X	No Depth (inches):	0 Wetland I	Hydrology Present?	YesX_ No
(includes capillary fringe)				
Describe Recorded Data (stream gauge, mo	nitoring well, aerial photos, pi	revious inspections), if av	'allable:	
Remarks: Site Evaluated during seasonally wet conditi	ons at beginning of growing s	eason.		

For a Other trans. (Distriction of Other 1999)	Absolute	Dominant	Indicator	Barrier Tart was desired
Free Stratum (Plot size: 30' Radius)	% Cover	Species?	Status	Dominance Test worksheet:
Acer negundo		Yes	FAC	Number of Dominant Species
2. Fraxinus americana		No	<u>FACU</u>	That Are OBL, FACW, or FAC: 2 (A)
3.				Total Number of Dominant
i. 5.	_			Species Across All Strata: 3 (B)
).).				Percent of Dominant Species That Are OBL, FACW, or FAC: 66.7% (A/B
7.				Prevalence Index worksheet:
•	6	=Total Cover		Total % Cover of: Multiply by:
50% of total cover:		of total cover:	2	OBL species 0 x 1 = 0
Sapling/Shrub Stratum (Plot size: 15' Radius	1 2070	or total cover.		FACW species $0 \times 2 = 0$
. Lonicera maackii	_	Yes	UPL	FAC species 15 x 3 = 45
. Londora madolai			- 01 L	FACU species 1 x 4 = 4
				UPL species 15 x 5 = 75
				Column Totals: 31 (A) 124 (E
·				Prevalence Index = B/A = 4.00
·				Hydrophytic Vegetation Indicators:
· -				1 - Rapid Test for Hydrophytic Vegetation
				X 2 - Dominance Test is >50%
				3 - Prevalence Index is ≤3.0 ¹
·	15			· 1 —— .
		= Lotal Cover		I 4 - Morphological Adaptations (Provide supporting)
50% of total cover:		=Total Cover	3	4 - Morphological Adaptations ¹ (Provide supportine data in Remarks or on a separate sheet)
50% of total cover:		of total cover:	3	data in Remarks or on a separate sheet)
lerb Stratum (Plot size: 5' Radius)	8 20%	of total cover:		data in Remarks or on a separate sheet) Problematic Hydrophytic Vegetation ¹ (Explain)
lerb Stratum (Plot size: 5' Radius) . Ficaria verna			3 FAC	data in Remarks or on a separate sheet)
lerb Stratum (Plot size: 5' Radius) . Ficaria verna	8 20%	of total cover:		data in Remarks or on a separate sheet) Problematic Hydrophytic Vegetation ¹ (Explain) Indicators of hydric soil and wetland hydrology must
Herb Stratum (Plot size: 5' Radius) . Ficaria verna	8 20%	of total cover:		data in Remarks or on a separate sheet) Problematic Hydrophytic Vegetation¹ (Explain) ¹Indicators of hydric soil and wetland hydrology must present, unless disturbed or problematic. Definitions of Four Vegetation Strata: Tree – Woody plants, excluding vines, 3 in. (7.6 cm) more in diameter at breast height (DBH), regardless of the strategy of t
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Herb Stratum (Plot size: 5' Radius) . Ficaria verna	8 20% 10	Yes	FAC	data in Remarks or on a separate sheet) Problematic Hydrophytic Vegetation ¹ (Explain) ¹ Indicators of hydric soil and wetland hydrology must present, unless disturbed or problematic. Definitions of Four Vegetation Strata: Tree – Woody plants, excluding vines, 3 in. (7.6 cm) more in diameter at breast height (DBH), regardless height. Sapling/Shrub – Woody plants, excluding vines, less than 3 in. DBH and greater than or equal to 3.28 ft (1 m) tall. Herb – All herbaceous (non-woody) plants, regardless of size, and woody plants less than 3.28 ft tall.
Herb Stratum (Plot size: 5' Radius) Ficaria verna	8 20% 10 10 10 10 5 20%	Yes	FAC	data in Remarks or on a separate sheet) Problematic Hydrophytic Vegetation¹ (Explain) ¹Indicators of hydric soil and wetland hydrology must present, unless disturbed or problematic. Definitions of Four Vegetation Strata: Tree – Woody plants, excluding vines, 3 in. (7.6 cm) more in diameter at breast height (DBH), regardless theight. Sapling/Shrub – Woody plants, excluding vines, less than 3 in. DBH and greater than or equal to 3.28 ft (1 m) tall. Herb – All herbaceous (non-woody) plants, regardless of size, and woody plants less than 3.28 ft tall. Woody Vine – All woody vines greater than 3.28 ft in
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Herb Stratum (Plot size: 5' Radius) Ficaria verna 500 of total cover: Voody Vine Stratum (Plot size: 30' Radius) Vitis sp. Celastrus sp.	8 20% 10 10 10 5 20%	Yes Yes Total Cover of total cover:	FAC	data in Remarks or on a separate sheet) Problematic Hydrophytic Vegetation¹ (Explain) ¹Indicators of hydric soil and wetland hydrology must present, unless disturbed or problematic. Definitions of Four Vegetation Strata: Tree – Woody plants, excluding vines, 3 in. (7.6 cm) more in diameter at breast height (DBH), regardless theight. Sapling/Shrub – Woody plants, excluding vines, less than 3 in. DBH and greater than or equal to 3.28 ft (1 m) tall. Herb – All herbaceous (non-woody) plants, regardless of size, and woody plants less than 3.28 ft tall. Woody Vine – All woody vines greater than 3.28 ft in
lerb Stratum (Plot size: 5' Radius) Ficaria verna	8 20% 10 10 5 20% 2 2	Yes Yes Total Cover of total cover:	FAC	data in Remarks or on a separate sheet) Problematic Hydrophytic Vegetation¹ (Explain) ¹Indicators of hydric soil and wetland hydrology must present, unless disturbed or problematic. Definitions of Four Vegetation Strata: Tree – Woody plants, excluding vines, 3 in. (7.6 cm) more in diameter at breast height (DBH), regardless theight. Sapling/Shrub – Woody plants, excluding vines, less than 3 in. DBH and greater than or equal to 3.28 ft (1 m) tall. Herb – All herbaceous (non-woody) plants, regardless of size, and woody plants less than 3.28 ft tall. Woody Vine – All woody vines greater than 3.28 ft in
Herb Stratum (Plot size: 5' Radius) Ficaria verna 50% of total cover: Voody Vine Stratum (Plot size: 30' Radius) Vitis sp. Celastrus sp.	8 20% 10 10 5 20% 2 2	Yes Yes Total Cover of total cover:	FAC	data in Remarks or on a separate sheet) Problematic Hydrophytic Vegetation¹ (Explain) ¹Indicators of hydric soil and wetland hydrology must present, unless disturbed or problematic. Definitions of Four Vegetation Strata: Tree – Woody plants, excluding vines, 3 in. (7.6 cm) more in diameter at breast height (DBH), regardless theight. Sapling/Shrub – Woody plants, excluding vines, less than 3 in. DBH and greater than or equal to 3.28 ft (1 m) tall. Herb – All herbaceous (non-woody) plants, regardless of size, and woody plants less than 3.28 ft tall. Woody Vine – All woody vines greater than 3.28 ft in height.
Herb Stratum (Plot size: 5' Radius) Ficaria verna Solution S	8 20% 10 10 5 20% 2 2	Yes Yes Total Cover of total cover:	FAC	data in Remarks or on a separate sheet) Problematic Hydrophytic Vegetation¹ (Explain) ¹Indicators of hydric soil and wetland hydrology must present, unless disturbed or problematic. Definitions of Four Vegetation Strata: Tree – Woody plants, excluding vines, 3 in. (7.6 cm) more in diameter at breast height (DBH), regardless theight. Sapling/Shrub – Woody plants, excluding vines, less than 3 in. DBH and greater than or equal to 3.28 ft (1 m) tall. Herb – All herbaceous (non-woody) plants, regardless of size, and woody plants less than 3.28 ft tall. Woody Vine – All woody vines greater than 3.28 ft in

SOIL Sampling Point: 1

		o the de				itor or co	onfirm the absence of	of indicators.)		
Depth	Matrix			Featur			- .	Б		
(inches)	Color (moist)	<u>%</u>	Color (moist)		Type ¹	Loc ²	Texture	Remarks		
0-3	2.5Y 2.5/1	100					Loamy/Clayey			
3-16	2.5Y 3/1	92	7.5YR 4/6	5	<u>C</u>	PL/M	Loamy/Clayey	Prominent redox concentrations		
			2.5Y 4/2	2	D	M				
1Type: C=Co	oncentration, D=Depl	etion RM	-Reduced Matrix M		—— ked Sand		² l ocation	PL=Pore Lining, M=Matrix.		
Hydric Soil I		elion, ixivi	-Neduced Matrix, W	IO-IVIAS	Keu Sanc	Giailis.		eators for Problematic Hydric Soils ³ :		
Histosol (Polyvalue Be	low Sur	face (S8	(MLRA		2 cm Muck (A10) (MLRA 147)		
	ipedon (A2)		Thin Dark Su				· · · —	Coast Prairie Redox (A16)		
Black His			Loamy Muck							
	n Sulfide (A4)		Loamy Gleye					Piedmont Floodplain Soils (F19)		
	Layers (A5)		Depleted Ma				<u> </u>	(MLRA 136, 147)		
	ck (A10) (LRR N)		X Redox Dark	, ,			F	Red Parent Material (F21)		
	Below Dark Surface	(A11)	Depleted Dar				(outside MLRA 127, 147, 148)			
	rk Surface (A12)	(,,,,	X Redox Depre				\	/ery Shallow Dark Surface (F22)		
	ucky Mineral (S1)				-	2) (LRR N		Other (Explain in Remarks)		
	leyed Matrix (S4)		Iron-Manganese Masses (F12) (LRR N, Other (Explain in Remarks) MLRA 136)							
	edox (S5)			•	3) (MLRA	122, 136	3Indio	cators of hydrophytic vegetation and		
	Matrix (S6)		Umbric Surface (F13) (MLRA 122, 136 Piedmont Floodplain Soils (F19) (MLR							
	face (S7)		Red Parent Material (F21) (MLRA 127,							
	.ayer (if observed):		_		· / ·			'		
Type:	None Obs	served								
Depth (in	iches):						Hydric Soil Prese	nt? Yes X No		
Remarks:							•			

U.S. Army Corps of Engineers

WETLAND DETERMINATION DATA SHEET – Eastern Mountains and Piedmont Region

OMB Control #: 0710-0024, Exp:11/30/2024 Requirement Control Symbol EXEMPT: (Authority: AR 335-15, paragraph 5-2a)

See ERDC/EL TR-12-9; the proponent agency is CECW-CO-R

Project/Site: 222 Church Road		City/County: Montgome	ery Co.	Sampling Date: 3/22/23		
Applicant/Owner: 222 Church Road LLC			State: PA	Sampling Point: 2		
Investigator(s): Max Russick		Section, Township, Range:	Cheltanham Twp.			
Landform (hillside, terrace, etc.): Artificial 1	errace Lo	cal relief (concave, convex,		Slope (%): 0-2		
Subregion (LRR or MLRA): LRR S, MLRA 1	48 Lat: 40.06898	Long: -	75.11710	Datum: WGS 84		
Soil Map Unit Name: Hatboro			NWI classifica	tion: None		
Are climatic / hydrologic conditions on the sit	e typical for this time of ye	ar? Yes	No (If no, e	explain in Remarks.)		
Are Vegetation X , Soil X , or Hydro			circumstances" present?	,		
Are Vegetation , Soil , or Hydro			plain any answers in Re			
SUMMARY OF FINDINGS – Attach			•	•		
			•	·		
Hydrophytic Vegetation Present?	Yes No	Is the Sampled Area	.,			
Hydric Soil Present?	Yes No No	within a Wetland?	Yes	NoX		
Wetland Hydrology Present?	Yes No					
Remarks:						
HYDROLOGY						
Wetland Hydrology Indicators:			Secondary Indicators	(minimum of two required)		
Primary Indicators (minimum of one is requi	red; check all that apply)		Surface Soil Crac	ks (B6)		
Surface Water (A1)	True Aquatic Plants	(B14)		ed Concave Surface (B8)		
High Water Table (A2)	Hydrogen Sulfide Od		Drainage Patterns	_ Drainage Patterns (B10)		
Saturation (A3)		res on Living Roots (C3)	Moss Trim Lines (· · · ·		
Water Marks (B1)	Presence of Reduce		Dry-Season Water Table (C2)			
Sediment Deposits (B2)		on in Tilled Soils (C6)	Crayfish Burrows	· ·		
Drift Deposits (B3)	Thin Muck Surface (Saturation Visible on Aerial Imagery (C9) Stunted or Stressed Plants (D1)			
Algal Mat or Crust (B4)	Other (Explain in Re	marks)		Geomorphic Position (D2)		
Iron Deposits (B5)	7 \		· ·			
Inundation Visible on Aerial Imagery (B	()	Shallow Aquitard (D3) Microtopographic Relief (D4)				
— Water-Stained Leaves (B9) Aquatic Fauna (B13)		FAC-Neutral Test (D5)				
		1	PAC-Neutiai Test	(D3)		
Field Observations: Surface Water Present? Yes	No. Y Donth (inch	00).				
Water Table Present? Yes X	No X Depth (inch	es): 14				
Saturation Present? Yes X	No X Depth (inch No Depth (inch Depth (inch	es): 14 Wetland	Hydrology Present?	Yes No		
(includes capillary fringe)	Boptii (iiioii	00). <u>10</u>	riyarology i resent.	103NO		
Describe Recorded Data (stream gauge, mo	onitoring well, aerial photos	s, previous inspections), if a	vailable:			
(5 5 1						
Remarks:						
Site Evaluated during seasonally wet condit	ions at beginning of growir	ng season. Stream assessm	ent data also collected	at this location.		

Indicator Status	Dominance Test worksheet:
	Dominance rest worksheet.
FAC	
	Number of Dominant Species That Are OBL, FACW, or FAC: 2 (A)
	Total Number of Dominant Species Across All Strata: 4 (B)
	Percent of Dominant Species That Are OBL, FACW, or FAC: 50.0% (A/E
	Prevalence Index worksheet:
	Total % Cover of: Multiply by:
: 2	OBL species 0 $x 1 = 0$
· ——	FACW species 0 x 2 = 0
UPL	FAC species 100 x 3 = 300
UPL	FACU species 0 x 4 = 0
— UFL	UPL species 10 x 5 = 50
	(/(
	Prevalence Index = B/A = 3.18
	Hydrophytic Vegetation Indicators:
	1 - Rapid Test for Hydrophytic Vegetation
	2 - Dominance Test is >50%
	3 - Prevalence Index is ≤3.0 ¹
	4 - Morphological Adaptations ¹ (Provide supporti
:2	data in Remarks or on a separate sheet)
	Problematic Hydrophytic Vegetation ¹ (Explain)
FAC	¹ Indicators of hydric soil and wetland hydrology must
	present, unless disturbed or problematic.
	Definitions of Four Vegetation Strata:
	Tree – Woody plants, excluding vines, 3 in. (7.6 cm)
	more in diameter at breast height (DBH), regardless
	height.
	Sapling/Shrub – Woody plants, excluding vines, les
	than 3 in. DBH and greater than or equal to 3.28 ft
	(1 m) tall.
	Herb – All herbaceous (non-woody) plants, regardles
	of size, and woody plants less than 3.28 ft tall.
	Woody Vine – All woody vines greater than 3.28 ft in
: 18	height.
	Hydrophytic
	Vegetation
:1	Present? Yes No
- er	er: 1

SOIL Sampling Point: 2

	ription: (Describe t	o the de				itor or co	onfirm the absence	of indicat	tors.)	
Depth (inches)	Matrix Color (moist)	%		k Featur %		Loc ²	Toyturo		Dom	orko
(inches)	Color (moist)		Color (moist)		Type ¹	Loc	Texture		Rem	arks
0-14	10YR 2/1	100					Loamy/Clayey			
14-20	2.5Y 3/2	90	7.5YR 5/6	5	<u>C</u>	PL/M	Loamy/Clayey	Prom	inent redox	concentrations
								-		
								-		
								·		
¹ Type: C=Co	ncentration, D=Deple	etion, RM	=Reduced Matrix, N	1S=Mas	ked Sand	l Grains.	² Locatio	n: PL=Po	re Lining, M	1=Matrix.
Hydric Soil I	ndicators:									tic Hydric Soils ³ :
— Histosol (· ·		Polyvalue Be				· · · —		k (A10) (M I	,
	ipedon (A2)		Thin Dark Su	-						(A16)
Black His			Loamy Muck			ILRA 136			147, 148)	
	Sulfide (A4)		Loamy Gleye				Piedmont Floodplain Soils (F19)			
	Layers (A5)		Depleted Ma						136, 147)	(504)
	ck (A10) (LRR N)	(0.44)	Redox Dark		. ,		Red Parent Material (F21)			
	Below Dark Surface rk Surface (A12)	(A11)	Depleted Da		, ,		(outside MLRA 127, 147, 148) Very Shallow Dark Surface (F22)			
	ucky Mineral (S1)				-) /I PP N		-		
	eyed Matrix (S4)			Iron-Manganese Masses (F12) (LRR N, Other (Explain in Remarks) MLRA 136)						
	edox (S5)			Umbric Surface (F13) (MLRA 122, 136				icators of I	hvdrophvtic	vegetation and
	Matrix (S6)		Piedmont Floodplain Soils (F19) (MLR							
Dark Sur			Red Parent I	•	•	, ,				roblematic.
	ayer (if observed):		_		. , ,				<u>.</u>	
Type:	None Obs	served								
Depth (in	ches):						Hydric Soil Pres	ent?	Yes	No
Remarks:										
Soil derived f	rom deposition in mil	l raceway	. No oxidized rhizo	spheres	could be	located	along living roots.			

U.S. Army Corps of Engineers

WETLAND DETERMINATION DATA SHEET – Eastern Mountains and Piedmont Region See ERDC/EL TR-12-9; the proponent agency is CECW-CO-R

OMB Control #: 0710-0024, Exp:11/30/2024 Requirement Control Symbol EXEMPT: (Authority: AR 335-15, paragraph 5-2a)

Sampling Date: 3/22/23 Project/Site: 222 Church Road City/County: Montgomery Co. Applicant/Owner: 222 Church Road LLC State: PA Sampling Point: Investigator(s): Max Russick Section, Township, Range: Cheltanham Twp. Local relief (concave, convex, none): Linear Landform (hillside, terrace, etc.): Floodplain Terrace Long: _-75.1167 Subregion (LRR or MLRA): LRR S, MLRA 148 Lat: 40.069035 Datum: WGS 84 Soil Map Unit Name: Hatboro NWI classification: PFO Are climatic / hydrologic conditions on the site typical for this time of year? Yes X No (If no, explain in Remarks.) Are Vegetation _____, Soil _____, or Hydrology _____ significantly disturbed? Are "Normal Circumstances" present? Yes X No ___ Are Vegetation , Soil , or Hydrology naturally problematic? (If needed, explain any answers in Remarks.) SUMMARY OF FINDINGS – Attach site map showing sampling point locations, transects, important features, etc. Hydrophytic Vegetation Present? Yes X Nο Is the Sampled Area Yes X No_ Hydric Soil Present? within a Wetland? Yes X No ____ Wetland Hydrology Present? Yes X No Remarks: **HYDROLOGY** Wetland Hydrology Indicators: Secondary Indicators (minimum of two required) Primary Indicators (minimum of one is required; check all that apply) Surface Soil Cracks (B6) Surface Water (A1) True Aquatic Plants (B14) Sparsely Vegetated Concave Surface (B8) High Water Table (A2) Hydrogen Sulfide Odor (C1) Drainage Patterns (B10) X Saturation (A3) Oxidized Rhizospheres on Living Roots (C3) Moss Trim Lines (B16) Water Marks (B1) Presence of Reduced Iron (C4) Dry-Season Water Table (C2) Sediment Deposits (B2) Recent Iron Reduction in Tilled Soils (C6) Crayfish Burrows (C8) Drift Deposits (B3) Thin Muck Surface (C7) Saturation Visible on Aerial Imagery (C9) Algal Mat or Crust (B4) Other (Explain in Remarks) Stunted or Stressed Plants (D1) Geomorphic Position (D2) Iron Deposits (B5) Inundation Visible on Aerial Imagery (B7) Shallow Aquitard (D3) Water-Stained Leaves (B9) Microtopographic Relief (D4) FAC-Neutral Test (D5) Aquatic Fauna (B13) Field Observations: Surface Water Present? No X Depth (inches): Depth (inches): Water Table Present? No Depth (inches): 6 Wetland Hydrology Present? Saturation Present? Yes X No (includes capillary fringe) Describe Recorded Data (stream gauge, monitoring well, aerial photos, previous inspections), if available: Remarks: Site Evaluated during seasonally wet conditions at beginning of growing season. Surface water only present in chanel traversing the wetland.

	fic names Absolute	Dominant	Indicator	Sampling Point: 3
Tree Stratum (Plot size:30' Radius)	% Cover	Species?	Status	Dominance Test worksheet:
1. Acer negundo	20	Yes	FAC	Number of Dominant Species
2. Acer platanoides	5	Yes	UPL	That Are OBL, FACW, or FAC:3(A)
i				Total Number of Dominant
·				Species Across All Strata: 5 (B)
·				Percent of Dominant Species That Are OBL, FACW, or FAC: 60.0% (A/B)
·				That Are OBL, FACW, or FAC: 60.0% (A/B) Prevalence Index worksheet:
	25	=Total Cover		Total % Cover of: Multiply by:
50% of total cover:		of total cover:	5	OBL species 5 x 1 = 5
apling/Shrub Stratum (Plot size: 15' Radius)	o. 101a. 0010.1		FACW species 0 x 2 = 0
. Acer negundo	, 5	Yes	FAC	FAC species 117 x 3 = 351
. Viburnum dentatum	2	No	FAC	FACU species 1 x4 = 4
Euonymus alatus	10	Yes	UPL	UPL species 15 x 5 = 75
<u>Luonymus alatus</u>		163		Column Totals: 138 (A) 435 (B)
·				Prevalence Index = B/A = 3.15
				Hydrophytic Vegetation Indicators:
-				1 - Rapid Test for Hydrophytic Vegetation
				X 2 - Dominance Test is >50%
·				3 - Prevalence Index is ≤3.0 ¹
·	17	=Total Cover		4 - Morphological Adaptations ¹ (Provide supporting
50% of total cover:		of total cover:	4	data in Remarks or on a separate sheet)
Herb Stratum (Plot size: 5' Radius)		or total cover.		Problematic Hydrophytic Vegetation ¹ (Explain)
. Ficaria verna	90	Yes	FAC	1 .
Symplocarpus foetidus	5	No	OBL	¹ Indicators of hydric soil and wetland hydrology must b present, unless disturbed or problematic.
Reynoutria japonica	1	No	FACU	Definitions of Four Vegetation Strata:
. Ligustrum sp.	1	No		Tree – Woody plants, excluding vines, 3 in. (7.6 cm) or
	<u> </u>			more in diameter at breast height (DBH), regardless of
				height.
				Sapling/Shrub – Woody plants, excluding vines, less
				than 3 in. DBH and greater than or equal to 3.28 ft
				(1 m) tall.
0				Herb – All herbaceous (non-woody) plants, regardless of size, and woody plants less than 3.28 ft tall.
	97	=Total Cover		Woody Vine – All woody vines greater than 3.28 ft in
50% of total cover:	9 20%	of total cover:	20	height.
Voody Vine Stratum (Plot size: 30' Radius)				
2.				
3.				
2. 3.		=Total Cover		Hydrophytic
2		=Total Cover		Hydrophytic Vegetation Present? Yes X No

SOIL Sampling Point: 3

		to the dep				itor or c	onfirm the absence of	of indicators.)		
Depth	Matrix			x Featur		. 2				
(inches)	Color (moist)	<u>%</u>	Color (moist)		Type ¹	Loc ²	Texture	Remarks		
0-8	10YR 3/2	100					Loamy/Clayey			
8-14	2.5Y 4/1	80	7.5YR 5/6	5	<u> </u>	PL	Loamy/Clayey	Prominent redox concentrations		
			10YR 4/2	5	D	M				
14-20	10YR 4/2	90	7.5YR 5/6	5	C	PL	Loamy/Clayey	Prominent redox concentrations		
			10YR 4/2	5	D	<u>M</u>				
¹Type: C=Co	ncentration, D=Depl	letion, RM	=Reduced Matrix, N	 //S=Mas	ked Sand	Grains.	² Location	: PL=Pore Lining, M=Matrix.		
Hydric Soil In		· · · · · · · · · · · · · · · · · · ·	•					ators for Problematic Hydric Soils ³ :		
Histosol ((A1)		Polyvalue Be	elow Sur	rface (S8	(MLRA	147, 148)	2 cm Muck (A10) (MLRA 147)		
Histic Epi	ipedon (A2)		Thin Dark Su	urface (S	S9) (MLR	A 147, 1	48)	Coast Prairie Redox (A16)		
Black His	stic (A3)		Loamy Muck					(MLRA 147, 148)		
	Sulfide (A4)		Loamy Gley				Piedmont Floodplain Soils (F19)			
Stratified	Layers (A5)		X Depleted Ma	trix (F3))		(MLRA 136, 147)			
2 cm Muc	ck (A10) (LRR N)		Redox Dark Surface (F6) Red Parent Material (F21)							
X Depleted	Below Dark Surface	e (A11)	Depleted Da	rk Surfa	ice (F7)		(outside MLRA 127, 147, 148)			
Thick Dar	rk Surface (A12)		Redox Depressions (F8) Very Shallow Dark Surface (F22)							
Sandy Mu	ucky Mineral (S1)		Iron-Manganese Masses (F12) (LRR N, Other (Explain in Remarks)							
Sandy Gl	eyed Matrix (S4)		MLRA 136)							
Sandy Re			Umbric Surface (F13) (MLRA 122, 136)							
Stripped I	Matrix (S6)		Piedmont Floodplain Soils (F19) (MLR							
Dark Surf	face (S7)		Red Parent I	Material	(F21) (M	LRA 127	7, 147, 148) ι	inless disturbed or problematic.		
Restrictive L	ayer (if observed):									
Type:	None Ob	served								
Depth (in	ches):						Hydric Soil Prese	nt? Yes X No		
Remarks:										

NC Division of Water Quality –Methodology for Identification of Intermittent and Perennial Streams and Their Origins v. 4.11

NC DWQ Stream Identification Form Version 4.11 Project/Site: 222 Charch Rd Date: 3-22-2,23 Latitude: Kussic4 **Evaluator:** Longitude: Max **Total Points:** 4.5 Stream Determination (circle one) Other Stream is at least intermittent **Ephemeral Intermittent Perennial** e.g. Quad Name: if ≥ 19 or perennial if ≥ 30* Abandonded Disconnected Mill Roceway - Not a Water Course Absent Weak Moderate Strong A. Geomorphology (Subtotal = 1 2 3 1a. Continuity of channel bed and bank 0 2. Sinuosity of channel along thalweg 0 2 3 1 3. In-channel structure: ex. riffle-pool, step-pool, 3 (0) 1 2 ripple-pool sequence 0 2 3 4. Particle size of stream substrate 1 5. Active/relict floodplain 0 1 2 3 (6) 1 2 3 6. Depositional bars or benches 0 2 3 7. Recent alluvial deposits 1 8. Headcuts 0 1 2 3 1.5 9. Grade control 0 0.5 1 10. Natural valley 0.5 1 1.5 11. Second or greater order channel No = 0Yes = 3artificial ditches are not rated; see discussions in manual B. Hydrology (Subtotal = 12. Presence of Baseflow (0) 2 1 (0) 1 2 3 13. Iron oxidizing bacteria (0.5) 0 14. Leaf litter 1.5 1 1.5 15. Sediment on plants or debris (0) 0.5 1 1.5 (0) 0.5 1 16. Organic debris lines or piles Yes = 317. Soil-based evidence of high water table? No = 0C. Biology (Subtotal = 0 18. Fibrous roots in streambed 3 2 1 0 3 2 1 19. Rooted upland plants in streambed 3 0 1 2 20. Macrobenthos (note diversity and abundance) 2 3 0 1 21. Aquatic Mollusks 1.5 0 0.5 1 22. Fish 0 0.5 1.5 23. Crayfish 1.5 0 0.5 24. Amphibians 1.5 (0) 0.5 25. Algae FACW = 0.75; OBL = 1.5 Other = 0 26. Wetland plants in streambed *perennial streams may also be identified using other methods. See p. 35 of manual. tes: Sample reach is centered around wetland Sample Point - 2.
Raceway floor is blanketed by Eurosian butter cap, a terrestial Species. Sketch: See Existing features plan by Robert E. Blue Consulting Engineers, P.C.

222 Church Road Cheltenham Twp., Montgomery County March 22, 2023



Photo 1: View of Raceway From Lawn; Facing South



Photo 2: View of Raceway at SP-2, Facing North-northeast



Photo 3: Typical Upland Lawn Condition



Photo 4: Wetland within Floodplain; Facing West